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Witness: Timothy D. Finnell  
Sponsoring Party: Union Electric Company  
Type of Exhibit: Rebuttal Testimony  
Case No.: ER-2011-0028  
Date Testimony Prepared: March 25, 2011

**MISSOURI PUBLIC SERVICE COMMISSION**

**CASE NO. ER-2011-0028**

**REBUTTAL TESTIMONY**

**OF**

**TIMOTHY D. FINNELL**

**ON**

**BEHALF OF**

**UNION ELECTRIC COMPANY  
d/b/a Ameren Missouri**

**St. Louis, Missouri  
March, 2011**

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**REBUTTAL TESTIMONY**

**OF**

**TIMOTHY D. FINNELL**

**CASE NO. ER-2011-0028**

1

**I. INTRODUCTION**

2

**Q. Please state your name and business address.**

3

A. My name is Timothy D. Finnell. My business address is One Ameren Plaza,

4

1901 Chouteau Avenue, St. Louis, MO 63103.

5

**Q. By whom and in what capacity are you employed?**

6

A. I am employed by Ameren Services Company as a Managing Supervisor,

7

Operations Analysis in the Corporate Planning Function.

8

**Q. Are you the same Timothy D. Finnell who filed direct testimony in this**

9

**case?**

10

A. Yes, I am.

11

**Q. What is the purpose of your rebuttal testimony?**

12

A. The purpose of my rebuttal testimony is to: (1) explain why Missouri

13

Industrial Energy Consumer's ("MIEC") witness James Dauphinais' proposed changes to

14

several generating unit capabilities used in the production cost model are incorrect; (2)

15

correct the Sioux coal blend cost calculated by the Staff, and (3) point out problems with the

16

Staff's calculation of normalized hourly power prices used in the production cost model to

17

develop normalized net fuel costs.

18

**II. MIEC REBUTTAL**

19

**Q. What areas of disagreement do you have with MIEC witness Dauphinais?**

1           A.     Mr. Dauphinais' direct testimony states that the Company incorrectly modeled  
2 the Callaway, Sioux, and Osage plant ratings and that the ratings of these plants should be  
3 increased.

4           **Q.     Is Mr. Dauphinais' recommended Callaway rating correct?**

5           A.     No. Mr. Dauphinais used actual unit net generation data from 2009 to  
6 determine his Callaway rating. Mr. Dauphinais calculated a 12-month average rating of  
7 1,229 net megawatts (MW), which is higher than the unit rating prepared by the Callaway  
8 performance engineering group (1,224 net MW). Schedule TDF-ER7 contains the 2009,  
9 2010, and 2011 plant rating information prepared by Brian Pae, Thermal Performance  
10 Engineer at Callaway.

11           **Q.     Why is there a difference between the ratings calculated by Mr. Pae and**  
12 **the 2009 performance?**

13           A.     Callaway's rating is very temperature sensitive. Schedule TDF-ER7 shows  
14 the monthly ratings prepared by Mr. Pae and illustrates how the output changes with  
15 temperature. In January, the coldest month, the rating is 1,234 net MW and in July, the  
16 hottest month, the rating is 1,197 net MW. During 2009 the Callaway plant performed better  
17 than its normal rating due to the cooler than normal circulating water temperatures.

18           The plant rating tables prepared by Mr. Pae are based on five years of temperature  
19 data rather than temperature data from a single year. The use of five years of temperature  
20 data is a better method for calculating normalized unit ratings and prevents significant rating  
21 changes that would occur if temperature data from a single year was used. For the same  
22 reason that billing units in a rate case are determined using normalized weather conditions  
23 (i.e., to eliminate the effects of hotter or cooler than normal weather in the test year) the

1 Callaway rating used by the production cost model should be based upon ratings calculated  
2 using multi-year temperature information. The latest information the Company has is the  
3 2011 Callaway Plant Capability Report, which I have included as the last page of Schedule  
4 TDF-ER7. It reflects an average annual rating of 1,224 net MW. The 1,224 net MW rating,  
5 based upon the latest available information and using multi-year temperature information is  
6 reflective of a normal level of capability for Callaway and this value should be used instead  
7 of the abnormally high value used by Mr. Dauphinais.

8 **Q. Did the Company incorrectly model the Callaway plant outage rates**  
9 **when it combined the full and partial outage rates into a single unplanned outage rate**  
10 **of 3.5%, as Mr. Dauphinais contends?**

11 A. No. The Company did not model the Callaway outage rates incorrectly.  
12 Rather, it simply used one of several PROSYM outage modeling methods. For the Callaway  
13 Plant, the Company chose to model the plant's full and partial outages using the PROSYM  
14 "EFOR" variable rather than to use separate variables for full and partial outages. This  
15 outage modeling method is appropriate because the Callaway partial outage rate is very  
16 small, 0.5%, and the Callaway plant typically runs at full load, which means that whether a  
17 partial outage is modeled as a derate or as a full outage will not result in a significant change  
18 to the production cost model results.

19 **Q. Given the foregoing, should Mr. Dauphinais' adjustments relating to**  
20 **Callaway inputs be made?**

21 A. No. The net fuel costs I have presented in this testimony accurately model the  
22 impact of Callaway generation on net fuel costs.

1           **Q.     Why is Mr. Dauphinais' recommendation regarding the Sioux unit**  
2 **ratings incorrect?**

3           A.     Mr. Dauphinais calculated the normalized Sioux rating (pre-scrubber) based  
4 on historical data from 2009. Had the coal quality used at Sioux in 2009 been normal, his  
5 approach may have produced reasonable results. However, the coal quality in 2009 was not  
6 normal, and it was substantially different in the test year and is expected to remain different.

7           **Q.     How does the coal quality impact the Sioux units' ratings?**

8           A.     For the Sioux Plant, as well as other plants, the generator output is a function  
9 of the amount of fuel, measured in British thermal units (Btus), input into the boiler. The  
10 lower the Btu content of the coal, the lower the generator output.

11           An example of the fuel input and generator output relationship is shown in Schedule  
12 TDF-ER8, which illustrates the impact of coal blending on Sioux unit capability. Sioux is  
13 the only Ameren Missouri coal-fired generating plant that has not been converted to 100%  
14 Powder River Basin ("PRB"), Wyoming coal. Consequently, it must blend PRB coal with  
15 Illinois coal. One method of changing the amount of fuel input to the boiler is to change the  
16 fuel blend or mix of low Btu coal (PRB) and high Btu coal (Illinois coal). Each row in  
17 Schedule TDF-ER8 represents a different Btu value as calculated for a specific coal blend  
18 and the associated unit capability. The first row is a 100% PRB and 0% Illinois coal blend,  
19 which has an average coal quality of 8,810 Btu/lb. and results in a unit capability of 402 net  
20 MW (pre-scrubber) or 394 net MW (post-scrubber). The plant cannot operate for long  
21 periods of time using a 100% PRB / 0% Illinois coal blend without running into operating  
22 issues. In order to avoid operating problems associated with burning 100% PRB coal, the  
23 Company tries to operate the plant at an 80% PRB /20% Illinois coal blend. The row in

1 Schedule TDF-ER8 with an 80% PRB / 20% Illinois coal blend has an average coal quality  
2 of 9,288 Btu/lb., which results in a unit capability of 428 net MW (pre-scrubber) or 419 net  
3 MW (post-scrubber).

4 **Q. What was the coal quality for the Sioux plant during 2009, 2010 and the**  
5 **test year, and what is the plant's estimated rating based upon that coal quality?**

6 A. The coal quality and estimated unit ratings for the periods are provided in the  
7 table below.

8

Period	PRB Coal Quality	ILL Coal Quality	Coal Blend %PRB/%ILL	Average Coal Quality	Rating based on coal Quality	Rating based on coal quality and Scrubber
2009	8830	11506	76.2% / 23.8%	9467	437	429
2010	8800	11114	78.2% /21.8%	9304	429	420
Test Year	8810	11200	80.0% / 20.0%	9288	428	419

9

10 **Q. What values do you recommend for the Sioux ratings?**

11 A. I recommend using 419 net MW based on the normal coal blend and normal  
12 coal quality, as reflected in the test year, adjusted for the impact of adding the scrubbers at  
13 Sioux. I would note that in my direct testimony I assumed that the net MW rating of each  
14 unit would decline by 12 MW due to the addition of the scrubbers. Based upon actual  
15 operations since the scrubbers went into service, the rating has only declined by 9 MW, a  
16 change that I have taken into account in my model results presented with this testimony.

1           **Q.     Why is Mr. Dauphinais' recommendation to change the Osage Plant's**  
2 **rating to 256 net MW incorrect?**

3           A.     Mr. Dauphinais based his rating for the Osage plant on a 2009 PROSYM  
4 "calibration run" that I provided for the purpose of validating the ability of the model to  
5 accurately simulate the Company's system. I have reviewed the Osage rating data used in  
6 my 2009 PROSYM calibration run and found that the value was incorrect. The Osage power  
7 plant never achieved 256 net MW during calendar year 2009. Instead, the highest plant  
8 generation level was 247 net MW and it reached this level for only 3 (out of 8,760) hours  
9 during the year. I have revised the 2009 calibration run rating to 237 net MW based on the  
10 fact that the plant output was equal to or lower than 237 net MW 95% of the hours in the  
11 year.

12           **Q.     Why shouldn't the 247 net MW level be used for the Osage Plant rating?**

13           A.     The 247 net MW output was achieved during high flow periods when the  
14 plant was operating under emergency conditions. During emergency conditions the plant is  
15 allowed (by its FERC license) to release more water, which in turn resulted in a higher than  
16 normal generation level. The 247 net MW level should not be used as a normalized plant  
17 rating, because it overstates the output that the generation the plant can be expected to  
18 achieve.

19           **Q.     What Osage rating do you recommend for use in the production cost**  
20 **model?**

21           A.     I recommend that the Osage rating used for determining normalized annual  
22 net fuel costs be set to the monthly unit rating listed in the Ameren Missouri Unit Capability  
23 Table Year 2011, which is an annual average of 237 net MW.





1 model. Ameren Missouri witness Jaime Haro addresses this “other adjustment” issue in his  
2 rebuttal testimony. Notwithstanding the Staff’s apparent agreement regarding power prices,  
3 so that the record is clear, I will address the problems with Staff’s method, as presented in  
4 their direct case filing, below.

5 **Q. Please continue.**

6 A. There are three major problems with the method that the Staff used as part of  
7 their direct case filing to calculate normalized power prices. The problems are: (1) the Staff  
8 improperly combined Day-Ahead Locational Marginal Prices (“DA-LMP”) applicable to  
9 Ameren Missouri load and Day-Ahead Locational Marginal Prices applicable to Ameren  
10 Missouri Generation, (2) the Staff used a monthly average price based on *all* purchases and  
11 sales, which distorts the power price target used for normalizing power prices, and (3) the  
12 Staff used bilateral purchases and sales, which have LMPs that are different than those  
13 received at Ameren Missouri’s generator nodes. Ameren Missouri witness Jaime Haro also  
14 discusses the third problem in his rebuttal testimony.

15 **Q. What do you mean by a normalized hourly power prices?**

16 A. Power prices have distinct patterns to them similar to customer load shapes.  
17 Schedule TDF-ER9 is a chart of actual power prices for the period May 1, 2010 through  
18 May 7, 2010 which illustrates this pattern.

19 **Q. Why is an hourly price pattern important?**

20 A. The hourly price pattern is important because it is used by the production cost  
21 model to calculate the revenues that can be earned from off-system sales when excess  
22 generation is available and it is used to determine if it is more economical to purchase power  
23 rather than operate generating units. Thus, if the hourly power prices are not developed

1 using a reasonable method that accurately simulates what will happen in the real conditions  
2 of the market, the simulation will be wrong and will predict erroneous levels of off-system  
3 sales or power purchases. This will in turn inject inaccuracy into the rebasing of net base  
4 fuel costs in the case, which will then create larger FAC rate adjustments in the future.

5 **Q. What is the problem with the way that the Staff combined the DA-LMP**  
6 **for Ameren Missouri's load and DA-LMP for Ameren Missouri's generating units?**

7 A. As the name implies, the Locational Marginal Prices ("LMP") means that  
8 each location has a different price. Thus the LMP associated with Ameren Missouri's load is  
9 not representative of the LMP associated with Ameren Missouri's generating units, which are  
10 at another location. Since only the Ameren Missouri generating units are used to make spot  
11 off-system sales, it is not appropriate to use the Ameren Missouri load LMP to develop  
12 normalized power prices, which is what the Staff did when they combined the Ameren  
13 Missouri load LMPs and the Ameren Missouri generation LMPs. In the case of Ameren  
14 Missouri, the LMPs associated with the load are typically higher than the LMPs associated  
15 with the generation. For example, during the month May 2010 the average hourly Ameren  
16 Missouri load LMP was \$29.08/MWh and the average hourly Ameren generator LMP was  
17 \$28.01/MWh, which is a \$1.07/MWh lower. Consequently, the Staff's method exaggerates  
18 normalized power prices. This will cause the model to generate an inaccurate level of fuel  
19 costs (higher fuel costs, because it will suggest Ameren Missouri will generate more MWhs),  
20 off-system sales (higher off-system sales revenues than can reasonably be expected), and  
21 purchased power (less than it should be). These inaccuracies lead to less accuracy in  
22 rebasing net fuel costs – in this case, it would lead to rebased net fuel costs that are too low,  
23 which creates a greater risk of larger fuel adjustment clause increases in the future.

1           **Q.     What is problem with the way that the Staff calculated its average**  
2 **monthly prices?**

3           A.     The Staff calculated the monthly average generator LMP by dividing the total  
4 generation revenues for the month by the total generation MWhs for the month. This  
5 approach produces a “high bias” for the monthly LMP because there is more generation  
6 during hours with higher LMPs and less generation during hours when the LMPs are lower.  
7 In other words, greater weighting was assigned to hours where the LMP was higher. A better  
8 method is to calculate a power price for each hour of the month and then average the hourly  
9 prices to determine the monthly average power price. An even more accurate approach is to  
10 separate the hourly LMPs into “on peak” and an “off peak” period averages for each month.  
11 This method applies the proper weighting to the LMPs.

12           Like the previous issue, the Company has discussed this issue with the Staff and the  
13 Staff has agreed to calculate the normalized hourly prices using hourly values which are  
14 grouped by “on-peak” and “off-peak” periods for each month.

15           **Q.     What are the problems associated with way the Staff handled bilateral**  
16 **sales in its direct case modeling?**

17           A.     There are two problems with the way that the bilateral sales were used. The  
18 first problem is that the Staff assumed that the bilateral sales price is representative of the  
19 price that could be obtained by Ameren Missouri’s generating units. As previously  
20 discussed, all of the pricing is dependent on the location of the power sale and purchase.  
21 Consequently, it is incorrect to use the price of the bilateral sales to represent prices that the  
22 generator could achieve for its excess generation because the generating units are at a  
23 different location from where the bilateral sale transaction occurs. The proper valuation of

1 bilateral sales is to net the revenue from the sale against the cost calculated using the LMP at  
2 the interface (location) where the bilateral sales occurred. The second problem with the  
3 Staff's modeling of bilateral sales is that many of them have fixed prices over consecutive  
4 hours, which distorts the hourly price shape (distortion of the hourly price shape means the  
5 wrong price is applied to the wrong hours). By way of further explanation, the use of fixed  
6 block sales prices will understate power prices during true high price periods and overstate  
7 prices during true low cost time periods. Therefore, bilateral sales must be excluded from the  
8 determination of normalized hourly power prices used in the production cost model.

9 **Q. Does this conclude your rebuttal testimony?**

10 A. Yes, it does.



December 1, 2008

Randall Irwin  
 Gary Blessing  
 Lee Eitel  
 James Warner  
 Dan Trokey  
 Tim Finnell  
 Tom Antweiler  
 Jeff Shelton  
 Regional Regulatory Affairs Supervisor  
 A160.0924

**2009 Callaway Plant Capability Report**

The Main 2009 capabilities are based on the MAIN (Mid-America Interconnected Network) Guide definition of monthly capability. Per the guide, net capability is corrected each month to account for changes in ambient temperature. The correction is based on an average of the warmest circulating water temperature each day averaged over a month (for 5 years). These capabilities represent what Callaway should be able to achieve during the four warmest hours of the day on an average temperature day. They are not intended to represent the worst possible peak load.

The Average 2009 capabilities are based on an average circulating water temperature each month. These capabilities represent what Callaway should be able to average for an entire month.

Due to the removal of the mechanical excitation system in refuel 15, gross capability increased by 2 MWe. An electrical excitation system was added at that time which increased house loads by 2 MWe. Therefore, net capability remained unchanged. The table below reflects this change. There are no generation uprates scheduled in 2009.

Please contact me at extension 68366 for any further information.

	<b>Main</b>	<b>2009</b>	<b>Average</b>	<b>2009</b>
	<b>Gross</b>	<b>Net</b>	<b>Gross</b>	<b>Net</b>
<b>Month</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>
January	1298	1240	1301	1243
February	1294	1236	1298	1240
March	1291	1233	1296	1238
April	1288	1230	1291	1233
May	1268	1210	1274	1216
June	1255	1197	1265	1207
July	1248	1190	1255	1197
August	1252	1194	1257	1199
September	1264	1206	1271	1213
October	1288	1230	1283	1225
November	1294	1236	1295	1237
December	1297	1239	1300	1242
Average	1278	1220	1282	1224



Brian A. Pae  
 Thermal Performance Engineer

December 7, 2009

Randall Irwin  
 Gary Blessing  
 Lee Eitel  
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 Tom Antweiler  
 Jeff Shelton  
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 Regional Regulatory Affairs Supervisor  
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### **2010 Callaway Plant Capability Report**

The Main 2010 capabilities are based on the MAIN (Mid-America Interconnected Network) Guide definition of monthly capability. Per the guide, net capability is corrected each month to account for changes in ambient temperature. The correction is based on an average of the warmest circulating water temperature each day averaged over a month (for 5 years). These capabilities represent what Callaway should be able to achieve during the four warmest hours of the day on an average temperature day. They are not intended to represent the worst possible peak load.

The Average 2010 capabilities are based on an average circulating water temperature each month. These capabilities represent what Callaway should be able to average for an entire month.

There are no changes in the 2010 capability report when compared to the 2009 capability report issued December 1, 2009. There are no generation uprates scheduled in 2010.

Please contact me at extension 68366 for any further information.

	<b>Main</b>	<b>2010</b>	<b>Average</b>	<b>2010</b>
	<b>Gross</b>	<b>Net</b>	<b>Gross</b>	<b>Net</b>
<b>Month</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>
January	1298	1240	1301	1243
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Average	1278	1220	1282	1224

Brian A. Pae  
 Thermal Performance Engineer



August 24, 2010

Randall Irwin  
 Gary Blessing  
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 Steve Finkbiner  
 Ken Stuckmeyer  
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**2011 Callaway Plant Capability Report**

The Main 2011 capabilities are based on the MAIN (Mid-America Interconnected Network) Guide definition of monthly capability. Per the guide, capability is corrected each month to account for changes in ambient temperature. The correction is based on an average of the warmest circulating water temperature each day averaged over a month (for 5 years). These capabilities represent what Callaway should be able to achieve during the four warmest hours of the day on an average temperature day. They are not intended to represent the worst possible peak load.

The Average 2011 capabilities are based on an average circulating water temperature each month. These capabilities represent what Callaway should be able to average for an entire month.

There are no changes in the 2011 capability report when compared to the 2010 capability report issued December 7, 2009. There are no generation uprates scheduled in 2011.

	<b>Main</b>	<b>2011</b>	<b>Average</b>	<b>2011</b>
	<b>Gross</b>	<b>Net</b>	<b>Gross</b>	<b>Net</b>
<b>Month</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>	<b>Capability</b>
January	1298	1240	1301	1243
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Brian A. Pae  
 Thermal Performance Engineer

**SIoux PLANT**  
**SO2 and Predicted Loads for Fuel Blends**

	PRB	8810	Net Load	Net Load
	ILL	11200	95% Fuel	95% Fuel
Actual BLEND % PRB	Actual BLEND % Ill	BTU/LB	No Scubber	With Scrubber
100%	0%	8810	402	394
95%	5%	8930	409	400
90%	10%	9049	415	407
85%	15%	9169	421	413
80%	20%	9288	428	419
75%	25%	9408	434	426
70%	30%	9527	441	432
65%	35%	9647	447	439
60%	40%	9766	454	445
55%	45%	9886	460	451
50%	50%	10005	466	458
45%	55%	10125	473	464
40%	60%	10244	479	471
35%	65%	10364	486	477
30%	70%	10483	492	484
25%	75%	10603	499	490
20%	80%	10722	505	497
15%	85%	10842	509	500
10%	90%	10961	509	500
5%	95%	11081	509	500
0%	100%	11200	509	500

### Generation DA LMP May 1, 2010-May 7, 2011

