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Witness/Type of Exhibit: Oligachlasgar,

Sponsoring Party: Missouri Public Service Commission

Comp.my: Kansas City Power

& Light Company

Case No.: HO-86-139

# MISSOURI PUBLIC SERVICE COMMISSION UTILITY DIVISION

SCHEDULES 1 THROUGH 7

OF

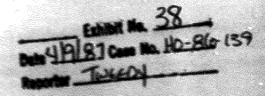
DIRECT TESTIMONY

OF

MARK L. OLIGSCHLAEGER

Jefferson City, Missouri Tebruary, 1987





# KANSAS CITY POWER & LIGHT COMPANY CASE NO. HO-86-139

# INDEX

SCHEDULE	TITLE
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# KANSAS CITY POWER & LIGHT COMPANY

A STUDY OF KCPL'S STEAM HEAT BUSINESS

December 1981

Corporate Planning Department

Corporate Planning & Pinance Division

# A STUDY OF KCPL'S STEAM HEAT BUSINESS

### I. INTRODUCTION

This study of KCPL's Steam Heat operations is in four parts. Following this Introductory Section, Section II addresses the history to add perspective, the physical aspects of the system, the current status of the business, and a discussion relating to allocation of costs, pricing, and financial results. Section II includes a discussion of the financial modeling approach taken and assumptions made to analyze alternative courses of action. A decision tree is developed to illustrate these alternatives.

In Section III an analysis of financial feasibility is performed. This is a graphical analysis consisting of price, rate of return, and cash flow comparisons. Once financial feasibility is evaluated, alternatives to continued operation are addressed in Section IV.

#### II. REVIEW OF THE BUSINESS

### A. Ristory

The distribution of steam for heating purposes was begun by the Kansas City Electric Light Company (a forerunner of KCPL) at its first incandescent light plant at 604 Wall Street. This address is now known as 604 Baltimore. This plant began operation in 1888. The distribution and sale of steam offered an economic outlet for an otherwise waste product by operating engines at an exhaust pressure slightly above atmosphere. The increase in exhaust pressure

did not materially increase the cost of electric energy and it made it practical to transmit the steam for heating purposes. Steam heat sales met with such success that the Kansas City Heating Company was formed in 1905, and the 604 Wall Street Station became Heating Station No. 1.

When the plant was abandoned as a primary source of electrical power due to the advent of condensing type equipment, the original boiler installation was converted to a heating plant so that steam service to customers could continue. Steam service was recognized as an aid in the sale of electric energy to large office buildings, stores, hotels, and others who might have produced their own electricity in an isolated plant, and used the exhaust steam to provide their own heat. The sale of steam made it possible for the Company to offer a complete service to the downtown district.

The increased demand for steam in the downtown area necessitated the construction in 1907 of a more modern heating plant, which was located at 1308-10 Baltimore Avenue. By 1917 the Kansas City Heating Company had ceased to exist and steam heat operations became a department of a predecessor of KCPL. Growing heat and electrical demand necessitated construction of the Wyandotte Station immediately west of the 1308-10 Baltimore location. These plants were connected and operated jointly as Heating Station No. 2.

Prior to 1929 all steam for the heating system was supplied by Heating Station No. 1 and Heating Station No. 2. Station No. 1 was located near the north end of the distribution system and Station No. 2 was near the south end. By 1929 the boilers in Station No. 1 were 40 years old and completely worn out.

In 1927, the Missouri River Power Rouse was purchased from the Ransas City Transit Company. Modernizing the equipment in this plant, later to be

called "Grand Avenue Station," offered the opportunity to produce steam heat in a very economical manner. A high pressure (185 lb.) steam main had to be constructed between Grand Avenue and old Heating Station No. 1 at 6th and Baltimore and pressure reducing equipment was installed in Station No. 1 at this time. These additions were completed in 1929. Grand Avenue virtually eliminated the use of the older heating plant at Heating Station No. 1.

It was also recognized that the equipment located near 13th Street would soon become obsolete, so in 1930 another high pressure main was constructed from 6th and Grand to 10th and McGee. Then in 1954 this main was further extended south to 14th Street to a pressure reducing station (Heating Station No. 3) in the basement of the KCPL Parking Garage. This firmed up the south supply of steam and the adjacent Heating Station No. 2 was continued for peaking purposes only.

In 1958 a second high pressure main was built from Grand Avenue to 6th and Baltimore and ultimately it was extended to 13th and Wyandotte which gave both Stations 1 and 3 two firm main line supplies for steam. Both stations 1 and 3 were subsequently converted to automatic control and in 1958 Heating Station No. 2 was demolished and retired from the plant accounts.

# B. Physical Characteristics

The heat utility plant can be considered in two parts. The steam distribution system and the portion of the electric plant which is used to generate steam for heating.

The steam distribution system consists of desuperheating stations at 604 Baltimore and 1319 Wyandotte, which are used to reduce the pressure of the incoming steam for customer use and the underground conduit, steam mains,

steam services, and meters which are used in distributing steam to our heat utility customers. From 1918 to 1980, the total length of steam mains has increased from 26,292 feet to 61,520 feet. The bulk of this increase occurred in 1930, 1954, and 1958 when mains were added from Grand Avenue to both the north and south ends of the distribution system. Since 1960 only 11,172 feet have been added. This is a 22% increase which means that the mains have been extended by about 1% per year for the past 20 years. There has been very little growth in the number of customers or the addition of steam mains during this period. The downtown service area is outlined in Illustration A. It extends north to 6th Street and south to 14th Street. The east-west boundaries are Oak and Broadway.

As can be seen in Table 1, the steam distribution plant has a dollar weighted average age of about 23 years, the bulk of the investment is in underground conduit and steam mains. The original distribution system, however, was built by the Kansas City Heating Company in 1905 and is, therefore, over 75 years old. The physical age of properties in the Steam Distribution Accounts is apparent from the last column in Table 1, the age of the earliest existing vintages.

The meters which comprise a small-part of the plant investment nevertheless have an important role in the heat utility business since they measure the steam sold to customers. Meters are of two types: condensate meters which measure the amount of steam condensate that exits the customer and flow meters which measure the flow of steam by measuring the drop in pressure across a customer location. The condensate meters are basically mechanical and are considered to be fairly accurate, but if the condensate is extracted

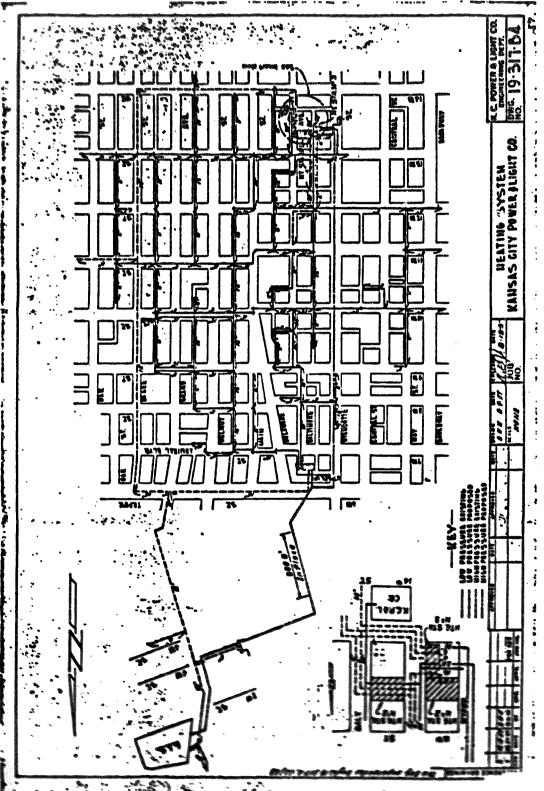


TABLE 1
Steam Distribution Accounts 12/31/80

Account	Plant Balance	Replacement Cost New	Replacement Cost New Less Depre.	Ave. Age	Age of Earliest Vintage
760 Land and Land					
Rights	\$ 60,163	\$ 268,419	\$ 111,434	21.0 yr.	23.0
761 Structures and		-			
Improvements	15,183	-			
762 Station Equip.	193,529	523,527	148,179	23.0	52.0
766 UG Conduit					
Steam Mains	2,994,907	17,999,185	3,422,825	23.0	52.0
769 Services	316,857	1,606,274	423,300	15.0	65.0
770 Meters	81,075	403,937	105,026	31.5	65.0
791 Office Furn.	•	·	•		
Equipment	1,167	4,413	369	53.0	67.0
794 Tools Shop and	•	•			
Garage Equip.	2,778	15,665	1,440	31.0	60.0
798 Misc. Equip.	153	445	79	24.5	24.5
Total	\$3,665,812	\$20,821,865	\$4,212,652	<u>22.5</u> yr.	

# Steam Distribution Plant Totals

	Plant-	Deprec.	
Year	In-Service	Reserve	Net Plant
1960	2,902,311	889,648	2,012,663
1961	2,847,345	847,073	2,000,272
1 <del>96</del> 2	2,881,518	896,150	1,985,368
1963	2,892,252	914,594	1,977,658
1964	2,968,267	962,594	2,005,673
1965	3,068,573	1,024,484	2,044,089
1966	3,257,598	1,051,331	2,206,267
1967	3,307,602	1,093,962	2,213,640
1968	3,381,512	1,168,347	2,213,165
1969	3,437,966	1,230,465	2,207,501
1970	3,500,055	1,294,795	2,205,260
1971	3,536,004	1,370,594	2,165,410
1972	3,586,424	1,433,040	2,153,384
1973	3,465,326	1,498,246	1,967,080
1974	3,473,938	1,573,127	1,900,811
1975	3,513,662	1,695,201	1,818,461
1976	3,578,864	1,786,974	1,791,891
1977	3.582.054	1,911,626	1,670,428
1978	3,618,500	2,040,060	1,578,440
1979	3,618,500	2,175,497	1,442,603
1980	3,665,812	2,334,364	1,361,448

prior to reaching the meters, they can give a low reading indication. The flow meters involve an electro-mechanical conversion to convert a drop in pressure to an electric current which can then be calibrated and measured. This calibration procedure can lead to inaccuracies in measurement. The meter investment is 31.5 years old on a dollar-weighted average basis.

As can be seen in Table 1, the plant balance of the steam distribution system including mains and meters at December 31, 1980, was \$3,665,812.

Replacement cost new was estimated to be \$20,821,865 based on Handy Whitman Indexes and the replacement cost new less depreciation was estimated to be \$4,212,652. Plant in service has only increased from \$2,902,311 to \$3,665,812 over the last 20 years. Net plant has decreased over this period from \$2,012,663 to \$1,361,448, so very little has been added to Distribution Plant.

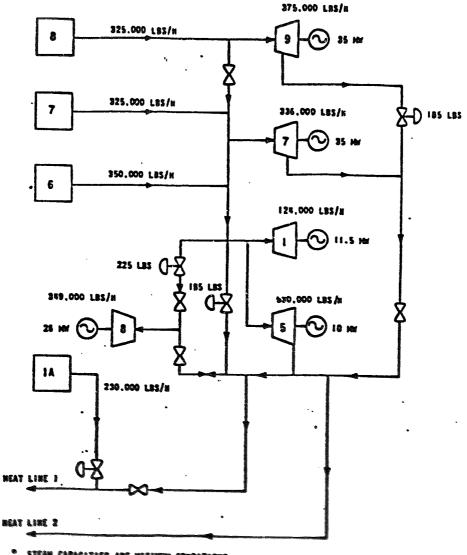
The remaining plant used to generate steam for heating is located at Grand Avenue station. Grand Avenue station is located on the Missouri River near the main business district of Kansas City, Missouri. Steam is produced in boilers at a nominal pressure of 650 PSIG for use in electric generation and at 185 PSIG for delivery to the Steam Department after suitable pressure reduction. The Steam Department then distributes steam at 185 PSIG, 100 PSIG, and 10 PSIG to steam customers. Prior to being purchased by KCPL, Grand Avenue Station had seven 25-cycle turbines with a combined generation of 59,000 kW. Realizing that the 25 cycle demand would be reduced as the electric railways were phased out, KCPL began converting the plant to 60 cycle. RCPL eventually installed 107,500 kW of 60 cycle and 10,000 kW of 25 cycle capacity removing five older turbine units having a capacity of 39,000 kW. The remaining 20,000 kW of older 25 cycle capacity was ultimately retired with the elimination

of the electric transit system, and the newer 10,000 kW, 25 cycle unit was converted to 60 cycle by the addition of a frequency converter. There are currently three coal or gas fired boilers—#6, #7, and #8—and one boiler, #1A, which is fueled by oil or gas. Boiler #1A is currently in a state of disrepair and its future use is questionable. Electricity is produced in high pressure turbines #1, #7, and #9 and topping turbine #5. The low pressure steam from turbine #5 was previously used to serve low pressure turbine #8 and aupply steam to the steam department. In 1977, low pressure turbine #8 was taken out of service. Low pressure steam is now all provided to the steam department either directly from boilers through pressure reducing valves or from topping turbine #5 which exhausts steam at 185 PSIG and, therefore, pressure reduction is not required. A schematic of the Steam Generating System at Grand Avenue is depicted by Illustration B.

Condensed steam from the turbines is returned to boilers, however, condensate for the steam department is not returned to the station and requires complete make-up from the city water supply.

The maximum capacity of Grand Avenue was rated at 99,000 kW peak net generation from 1971 to 1977 although peak net generation of 108,000 kW was achieved as can be seen in Table 2 which gives some operating statistics on the station. From 1977 to present, it has been rated at 70,000 kW. As the related capacity of Grand Avenue has been reduced, so has the annual generation from 156,200 MWh in 1971 to 44,000 MWh in 1980. Future projections, also indicated on Table 2, are even lower reducing to 20,000 MWh and sero generation beyond 1990. The rated capacity at Grand Avenue is scheduled to be derated from 70,000 kW to 40,000 kW in 1982 when turbines #1, #5, and #7 will go on inactive reserve.

# ILLUSTRATION B



- . PLENS CTARCILIES THE MELLINES CONDILION?"
- \*\* TOTAL CAPACITIES ARE RATED.

TABLE 2

Grand Avenue Operating Statistics

Year	(000°s) MWhs Net Genera- tion	Total and Fired MMBtu	Peak kW	Avg. Cents/ MMBtu	Total Fuel
1971	156.2	4,516,998	107,000	30.9	1,395,752
1972	157.6	4,744,884	108,000	33.0	1.565.812
1973	186.9	5,130,633	106,000	36.3	1.862.420
1974	154.5	4,397,835	107,000	42.6	1.873.478
1975	198.2	5,320,909	99,C00	69.24	3.684.416
1976	203.1	5,624,476	99,000	84.2	4,735,802
1977	143.1	4,774,660	70,000*	90.17	4.305.439
1978	120.3	4,526,393	70,000	107.3	4,858,543
1979	127.9	4,776,599	70,000	128.89	6,156,558
1980	44.0	2,933,820	70,000	151.18	4,435,346

\*Retired Boiler #8

# Future Projections

Year	(000's) MWhs Net Genera- tion	MMBtu Excluding Steam	Peak kW	Cents/ MBtu	Fuel Excluding Steam
1981	20.0	748,677	70,000	190.68	1,431,098
1982	20.0	748,677	40,000	226.0	1,692,010
1983	32.0	588,000	40,000	230.0	1,351.000
1984	28.0	525,000	40,000	285.0	1,498,000
1985	15.0	275,000	40,000	313.0	861,000
1986	35.0	640,000	40,000	334.0	2,138,000
1987	22.0	408,000	40,000	328.0	1,340,000
1988	36.0	655,000	40,000	429.0	2,507,000
1989	37.0	692,000	40,000	453.0	3,135,000
1990	20.0	369,000	40,000	591.0	2,182,000
1991	0.0				-,,

Table 3 demonstrates that the weighted average age of steam generating plant is approximately 35 years, but the property dates back to the early 1900s. The total plant in service at the end of 1980 was \$20,959,272. The replacement cost new was estimated to be \$120,408,317 and the depreciated replacement cost new was \$18,666,077. This relates to 117.5 MW of name plate capacity that is currently rated at 70 MW. Of the 320,959,272 electric plant in service, \$3,092,727 has been allocated to the heat utility business.

Electric plant in service at Grand Avenue has only increased from \$18,925,608 to \$20,959,272 over the last 20 years. Net plant has decreased over this period from \$10,863,294 to \$6,232,547. Grand Avenue, like the Steam Heat Distribution System, has had very few additions made in the recent past.

Electrically, Grand Avenue serves mainly as a peaking unit and a central distribution point for providing electrical services to the downtown area. If the steam requirement were eliminated, some generation at Grand Avenue would still be required unless some changes are made in the distribution network. An alternative would be to operate Grand Avenue on a standby status as a gas fired unit. This alternative would necessitate a redesign of the electrical network that supplies downtown Kansas City. It has been estimated that this could reduce the O6M expenses at Grand Avenue by 67%.

# C. Allocation Factors

The allocation of electric expenses to the heat utility operations was originally based on the philosophy that Grand Avenue station is primarily an electric generating peaking source and the steam demand of the steam department is a secondary by-product of electric generation. This philosophy has been followed even though steam service is not interruptible. This early allocation

TABLE 3

	Grand	Avenue P	roduct	ion Acco	unts	12/31/80		
Account	Plant	Balance	•	cement	Cor	lecement st New s Depre.	Ave. Age	Age of Earliest Vintage
310 Land	\$	626,252	\$	-	\$			
311 Structures and								
Improvements	3,	821,027	29	,027,145	1,	,146,938	35.0 yr.	65.0
312 Boiler Plant	9,	133,956.	50,	207,338	7,	,332,643	31.0	65.0
314 Turbo Generato	TB 4.	220,990	28	540,623	6.	202,387	45.0	65.0
315 Accessory Elec	_							
Equipment		911,234	11.	794,968	3.	764.941	30.0	65.0
316 Miscellaneous		245,813		838,243		219,168	24.0	65.0
Total	\$20,	959,272	\$120	408,317	\$18	,666,077	34.5 yr.	
Allocation to Stea	m \$ 3,	092,727		-			,	

# Grand Avenue Station Totals

Year	Plant- In-Service	Deprec. Reserve	Net Plant
1960	18,925,608	8,062,314	10,863,294
1961	18,927,632	8,541,326	10,386,306
1962	18,958,992	8,995,740	9, <del>9</del> 63,252
1963	17,887,993	8,420,525	9,467,468
1964	17,925,099	8,647,892	9,277,207
1965	17,714,273	8,300,544	9,413,729
1966	17,723,214	8,734,810	8,988,404
1967	16,944,205	8,294,288	8,649,917
1968	18,120,128	8,728,749	9,391,379
1969	19,547,037	9,186,727	10,360,310
1970	19,165,511	9,310,581	9,854,930
1971	19,184,556	9,775,393	9,409,163
1972	19,207,834	10,262,524	8,945,310
1973	19,471,180	10,269,261	8,601,919
1974	19,516,503	14,428,956	5,087,547
1975	20,480,645	11,571,054	8,909,591
1976	20,477,190	12,194,754	8,282,436
1977	20,696,698	12,745,856	7,946,842
1978	20,735,710	13,431,567	7,304,143
1979	20,908,829	14,075,392	6,833,437
1980	20,959,272	14,726,725	6,232,547

was based on the steam heat demand that was coincident with one-hour peak electrical demand. Since 1953 the electrical peak has occurred in the summer causing a large part of the station's total costs to be borne by the electricity business. A study on steam allocations was performed by Black & Veatch in 1958 in detail on an item-by-item basis which confirmed this "peak allocation". This allocation method has been challenged several times by commission staff members. Only recently has this methodology been changed to give steam customers a larger percentage of costs to be shared with the electric business.

The largest component of cost for heat utility operations is purchased steam. This expense is basically the fuel and water expenses associated with producing steam for heat. These direct variable costs are determined on the basis of actual pounds of steam transferred to heat utility and pounds of make-up water used by the heat department.

Those expense items associated with operating and maintaining the boilers and other structures, O&M expenses, are allocated to the Steam Heat Department on the basis of the average of the monthly steam requirements supplied by the boiler facilities for use by the Steam Department as compared to the annual peak steam requirement of the Electric Department. Other allocations to the utility heat business are interdepartmental rent and Administration and General (A&G) expenses. The former consists of taxes, depreciation, and return on the electric plant allocated to steam. This allocation is made in the same manner as boiler O&M. The latter, Steam Heat A&G expenses, are a portion of the overall company's A&G expenses. This is also allocated in the same manner as boiler O&M. Further detail on steam allocations is provided in Appendix A which includes sample allocations and extracts of filed testimony from the last Missouri retail and steam filing, Case No. 28-61-42.

# D. Steam Heat Prices

The growth in the steam business has been relatively slow. In 1918 annual sales were 440 million pounds, the price was 68 cents per thousand pounds, producing revenues of \$300,000. The price of steam increased sharply to \$1.50 per thousand pounds in 1921 at which time usage was 450 million pounds annually, producing revenues of about \$700,000. After 1921, the price of steam declined steadily reaching a low of near 85 cents in the early 1930s. In 1960, 39 years later, the price of steam had risen again to \$1.50 per thousand pounds, usage was 878 million pounds, and revenues were \$1,324,539. By 1971, the price of steam was still around \$1.50 per thousand pounds, usage was 1,141 million pounds yielding revenues of \$1,700,000. By 1980, the price had climbed to \$5.80 per thousand pounds, the usage was 633 million pounds, and the revenues were \$3,660,000.

The price of steam heat has increased dramatically in the last few years. The only rate case prior to 1971 was in 1961 and that resulted in a lower steam heat rate being set at an average of \$1.46. Since 1971, we have had six rate increases and the average cost of steam per 1,000 pounds has increased from \$1.50 in 1971 to \$5.80 at the end of 1980. The average revenue per 1,000 pounds for each year is shown in Table 4.

A comparison of other utilities' prices as compiled by The International District Heating Association reveals that in 1980 the price of steam per 1.000 pounds ranged from \$2.50 to \$15.00.

# E. Customers and Financial Results

There were 210 steam customers at the end of 1980. Since 1971, the number of customers has declined from 272 to 210 billed at the end of 1980.

TABLE 4

Year	Avg. Annual Rate ( (\$/1,000 lbs.)	Month of Rate Increase	Steam Customer Dollars Per Unit Of Heat Content (\$/MMBtu)	Gas Customer Dollars Per Unit Of Heat Content (\$/M'Btu)	Gas/Steam (Percent)
1971	1.50		1.29		
1972	1.50		1.29		
1973	1.50	June 73	1.29		
1974	2.00	APE 74	1.72		
1975	2.70		2.32	.75	327
1976	3.30	May 76	2.84	.95	332
1977	3.80	Nov 77	3.27	1.50	462
1978	4.50		3.87	1.75	457
1979	5.20		4.48	2.00	45%
1980	5.80	Mar, Jul 1980	5.00	2.80	562

<u>Year</u>	Bldgo.*	Heat Degree Days	Steam Input Less Co. Use (MM1b.)	Sales (MM1b.)	Losses (MM1b.)	Percent Loss	Lbs. Steam Input/ Bldg/ Day	Lbs. Sales/ Bidg/ • Day	Lbs. Losses/ Bldg/ * Day
1960	307	-	1004.4	878	126.0	12.5	0.0	-	
1961	304	-	977.6	859	119.0	12.2			
1962	299	5019	980.7	872	109.0	11.1	653.5	581.1	99.4
1963	293	4782	967.4	841	126.0	13.0	690.4	600.2	72.6
1964	286	4442	954.4	832	122.0	12.9	751.3	654.9	89.9
1965	284	4528	1004.0	861	143.0	14.2	780.7		96.0
1966	278	4614	1108.7	966	143.0	12.9	864.4	669.5	111.2
1967	279	4623	1100.9	981	120.0	10.9	853.5	753.1	111.5
1968	281	4995	1242.4	1177	60.0	5.3	885.2	760.6	93.0
1969	280	5206	1382.4	1215	167.0	12.1	948.4	838.6	47.0
1970	281	4688	1399.5	1220	179.0	12.5		833.5	114.6
1971	294	4529	1346.5	1141	205.5	15.3	1062.4	926.1	135.9
1972	203	5036	1354.5	1169	176.5	13.0	1047.0	887.1	159.9
1973	286	4514	1218.8	1139	79.8		950.4	820.2	130.2
1974	267	4370	1137.6	882	255.6	6.5	944.1	882.3	61.8
1975	208	4636	1120.1	922	198.1	22.5 17.7	975.0	755.9	219.1
1976	269	4763	1126.6	868	258.6		901.5	742.1	157.4
1977	271	4728	1115.0	908	207.0	23.0	882.6	680.0	202.6
1976	252	5570	1243.5	864	379.5	18.6	870.2	708.7	161.5
1979	244	5264	1195.5	764	431.5	30.5	885.9	615.5	270.4
1980	238	4689	1053.0	634	419.0	36.1 39.8	930.8 943.6	594.8 568.1	336.0 375.5

<sup>\*</sup>For the time period 1960-1970, total customers were used as a proxy for the number of buildings.

This number is slightly misleading since some of this decline in customers involved several customers being combined. A more indicative number is the number of meters or buildings served. The number of meters has declined from 284 in 1971 to 238 in 1980. Table 5 summarizes some of the key sales figures during the last 20 years.

Since 1960 the actual amount of business measured in terms of buildings served has decreased. This is reflected in steam input to the system. Steam input per building per degree day has not trended downward but has remained fairly constant. The annual sales in pounds of steam has declined significantly apparently due to two factors—fewer buildings served and fewer sales per building per degree day. The decrease in sales/building/degree day as compared to a relatively constant steam input/building/degree day indicates that "additional efforts be made to improve customer inspection and metering" as pointed out in a recent report made by System Power Operations. It is assumed in this analysis that if a rigorous effort is undertaken to improve customers' inspections and metering losses, unaccounted steam can be reduced to 17%. This is based on the average loss per building per degree day prior to 1978 divided by the average steam input/building/degree day over the 1971-1980 period.

Table 6 lists key financial results for the last 20 years. These results are rearranged to separate the variable components of purchased steam, O6M, general taxes, and the relatively fixed income tax and other expenses. For the past three years, steam heat revenues have not covered total costs. In 1980 such revenues did not even match variable costs which are essential to continuing operation.

These results indicate we have never earned a "reasonable return" on the steam investment. As the amount of sales in pounds of steam per customer per

		Purchased		General	Net	Income Tax	Operating
Teer	Revenues	Steen	OEM	Taxes	Revenue	& Other	Income
		(Variabla)	(Variable)	(Variable)		(Fixed)	
1960	1,324,539	526,822	78,563	115,377	603,777	376,672	277,105
1961	1,253,243	510,244	90,724	108,104	544,171	380,031	164,140
1962	1,237,428	548,675	78,266	112,369	498,118	354,054	144,064
1963	1,169,674	538,756	85,136	106,516	439,266	318,855	120,411
1964	1,171,119	556,311	104,113	107,365	403,330	305,825	97,505
1965	1,194,047	578,173	131,531	116,662	367,681-	287,951	79,730
1966	1,292,850	618,035	185,852	118,840	370,123	310,708	59,415
1967	1,321,137	600,178	113,319	135,230	472,410	374,501	97, <del>9</del> 09
1966	1,568,595	712.831	115,105	169,864	570,795	422,354	148,441
1969	1,729,432	810,175	162,388	237,743	519,126	372,707	146,419
1970	1,797,983	886,682	174,896	245,947	490,458	345,642	144,816
1971	1.700.064	833,826	265,194	244,296	356,748	256,164	100,584
1972	1,828,730	983.860	193,180	244,472	407,218	338,152	69,066
1973	1.735.586	945,601	202,770	232,853	354,362	335,076	19,286
1974	1,786,694	1.046.916	178,058	208,857	352,863	395,158	(42,295)
1975	2.505.512	1,549,272	234,252	288,272	433,716	423,346	10,370
1976	2.866.684	1,874,548	268,254	314,732	409,150	411,618	(2,468)
1977	3,497,462	2,056,490	299,352	397,568	744.052	638.248	105.804
1976	3,912,840	2,697,831	300,150	426,798	488,061	546,889	(58,828)
1979	3.986.082	3,127,249	327,394	453,602	77.837	359,712	(261,875)
1980	3,660,104	3,356,088	378,649	385,079	(459,712)		(554,442)
1960-1	1980 176	537	382	234	(176)	189*	(300)
	at Change	,,,,	<b>301</b>		(0,0)		(200)
Avg. ( Change Year	Percent 5 9 Per	10	8	6	(5)	5*	(7)

\*Adjusted for \$997,000 tax loss in 1980.

degree day has declined, we have had to produce about the same steam due to increased losses. Purchased steam expense which is related to the steam input to the system has increased at a faster pace than any other costs due to higher fuel costs, and a greater ellocation of fixed costs to steam as electric generation has been reduced. Expenses excluding Distribution OSM, taxes, and purchased steam have increased moderately over the last 20 years. These expenses increased by 189% (5% per year) excluding the income tax loss in 1980. Such costs are more related to investment which has not increased substantially. These cost increases have not been offset by adequate rate increases and, therefore, a "reasonable return" has not been attained.

Assuming that the unaccounted steam problem is at the customer's end, then a continous effort of checking metering and customer inspection should result in higher sales.

#### E. Discussion

The objective of this first phase of the steam business study was to recite the history of the business, document its physical characteristics, and review the history of its financial performance. The objective of the next phase is to analyze the future potential profitability of the steam heat business. This will be addressed in Section III.

The financial profitability of the steam business has continued to decline over the last decade. There are several key factors contributing to its decline. These factors include the lack of growth in the area served by the steam business, increased losses, inflation in energy costs, aging plant and distribution facilities, and inadequate revenue increases to meet costs.

With this background, what is the financial potential of the business?

To analyze this question am accounting model of the steam business was developed

using the Interactive Financial Planning System. This model simulates the cost accounting of the steam heat business and can be used to estimate financial profitability under varying assumptions of key factors. Five factors were determined to be the major considerations in the financial future of the steam business.

- The Grand Avenue Plant is old and could be retired. How will changes in the level of the electric business at Grand Avenue affect the steam business. As allocation to electric drops to zero, what is the impact on financial results?
- The number of customers and the steam sold over the past decade has continually declined. What are the possibilities of reversing this trend?
- 3. The system losses have increased substantially, particularly over the past few years. Can these losses be reduced without a significant increase in operating expenses?
- 4. Rate relief has not kept pace with the costs of operating the business. What levels of rate relief are possible from the MPSC? How high can prices rise and yet remain competitive?
- 5. As new investment is required to replace aging equipment, what is the effect on rate levels?

A decision tree was constructed to analyze the financial impact of warying four of these key factors through a reasonable range of expectations (see Illustration C).

Key Factor Definitions:

#### Hypothesis

# (1) Grand Avenue operation continues?

#### Definition

Yes: Grand Avenue electric operation continues indefinitely at current operating levels.

No: Grand Avenue electric operation retires in 1985 and is used only for steam business thereafter.

(2) Sales can be increased? Yes: Steam sales increase to include a large customer in 1983.

No: Continue trend established over the past decade.

(3) Losses can be reduced? Yes: Losses are reduced to 20%.

No: Losses remain at 402.

(4) What level of rate relief Alt. 1: Prices escalate at the Company's can be obtained? expected fuel inflation rate.

Alt. 2: Prices escalate at projected gas price escalation rates to remain competitive with gas.

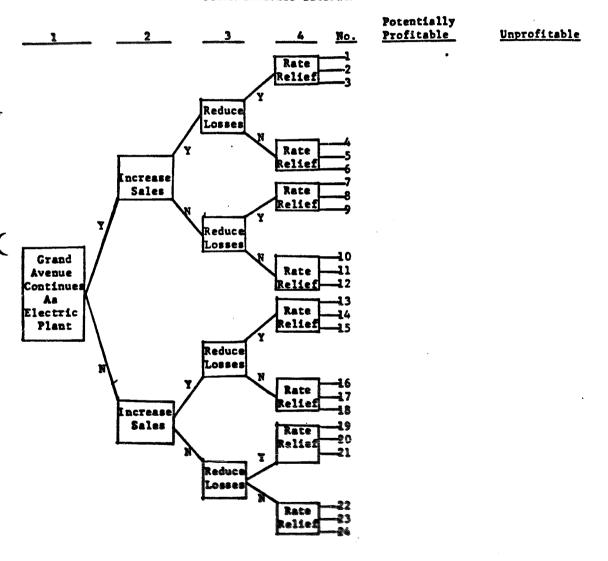
Alt. 3: Prices reflect full cost of service by 1985 and thereafter.

The initial analysis consisted of developing a steam model case to simulate each decision tree path and project the likely financial results over the next ten-year period if that particular combination of events occur. These 24 cases provided the basis for evaluating the future profitability of the steam business. Detailed financial results for these cases are included in Appendix 5. From this information, some conclusions are formulated in Section III about the viability of KCPL remaining in the steam heat business.

The third phase of the study (Section IV) explores alternatives to current operations such as operating the business as a distinguishable profit center, as a cogeneration project, or a plan to get out of the business by selling to another party—the city, another energy company, or another interested party.

# ILLUSTRATION C

# STEAM BUSINESS DECISION TREE



#### III. FINANCIAL ANALYSIS

# A. Price of Steam Based on Full Cost of Service

1. Grand Avenue Station Retired Beyond 1990

Chart 1 illustrates the projected price of steam in c/MMBtu for Cases 3, 6, 9, and 12 on the decision tree under the assumption that KCPL earns its full required return of 13% on net steam distribution plant by 1984 and that the electric service portion of Grand Avenue Station is retired after 1990. The projected steam prices are compared to the projected price of natural gas (General Service) as delivered and also the equivalent cost of gas converted to steam using a 65% efficiency ratio.

Case 12 is a reference case and represents the status quo:

- -- Sales from existing customers continue at current levels and are diminished slightly by increased price elasticity effects.
  - -- No large customer is added to the system.
  - -- Losses at the 40% level continue unabated.

This reference case indicates that steam prices would not be competitive with equivalent gas even after the full deregulation of gas prices beyond 1985 start to take effect. All cases show significant rate increases above inflation rates over the next few years if a 13% rate of return is to be achieved by 1984.

The competitive advantage of steam prices improves as adjustments to the reference case are made. Case 9 assumes reduction of losses from 40% to 20% and shows steam prices become competitive by 1986. This assumes that loss reduction is a direct source of revenue. Case 3 contains the additional assumption that a very large steam customer (twice the size of all existing customers combined) could be added in 1983 on an attractive steam rate at the

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equivalent price of delivered natural gas. The short run impact is to raise the overall price of steam above Case 9 in the years prior to 1986, but steam prices remain flat and below Case 9 thereafter. In the long-run, the overall steam price falls below even the delivered price of gas beyond 1989 and becomes very competitive.

#### Grand Avenue Station Retired in 1984

Chart 2 contains the cases of Chart 1 modified to include the retirement of the electric portion of Grand Avenue Station in 1984. This causes more steam boiler plant to be allocated to the remaining steam business in 1985 and beyond, thus raising the overall cost of steam. Case 15 is the only case in this group that becomes competitive with gas, and this doesn't occur until 1988. This case assumes the reduction in losses from 40% to 20% and sales to a very large customer. Retiring the electric business delays the cross-over point where steam prices become competitive by two years over Case 3 in Chart 1. Case 21 shows that reduction in losses alone is not sufficient for steam to become competitive with gas if the electric plant is retired in 1984. To cover cost of service upon retiring Grand Avenue electric rates would practically have to double in all cases.

## 3. Summary of Full Cost of Service Cases

If the price of steam is permitted to rise to its fully allocated cost of service, which implies significant increases over the next two years, and is to become competitive with deregulated gas within five years (1986), then

(a) steam losses must be reduced to 20% or less and (b) large steam sales must be attained and (c) the retirement of the electric business at Grand Avenue Station would have to be delayed beyond 1990.

If the electric service is retired in 1984, then the competitive point between steam and gas is delayed two more years to 1988.

SCHOOLE 1-26

Name of the American	
	1377 FOMER & LIGHT COMPANY 2/04/04 TIME 14157 [AT MODEL
	STEAM MATES CENTS/HHBTU 1991-1990 GRAND AVENUE ELECTRIC RETINES ELECTRIC OPERATION CHART 2
- SCHEDULE 1-27	O - DAD PRICE EDITANTE  O - DAD PRICE CONVENTED DASK EPFICIENCY  S - CASE 45 STEAM PRICE COA-, S-, RL-, RICS)  A - CASE 24 STEAM PRICE COA-, S-, RL-, RICS)  A - CASE 24 STEAM PRICE COA-, S-, RL-, RICS)

# B. Price of Steam Increased at the Rate of Inflation of Variable Fuel Costs to Produce Steam

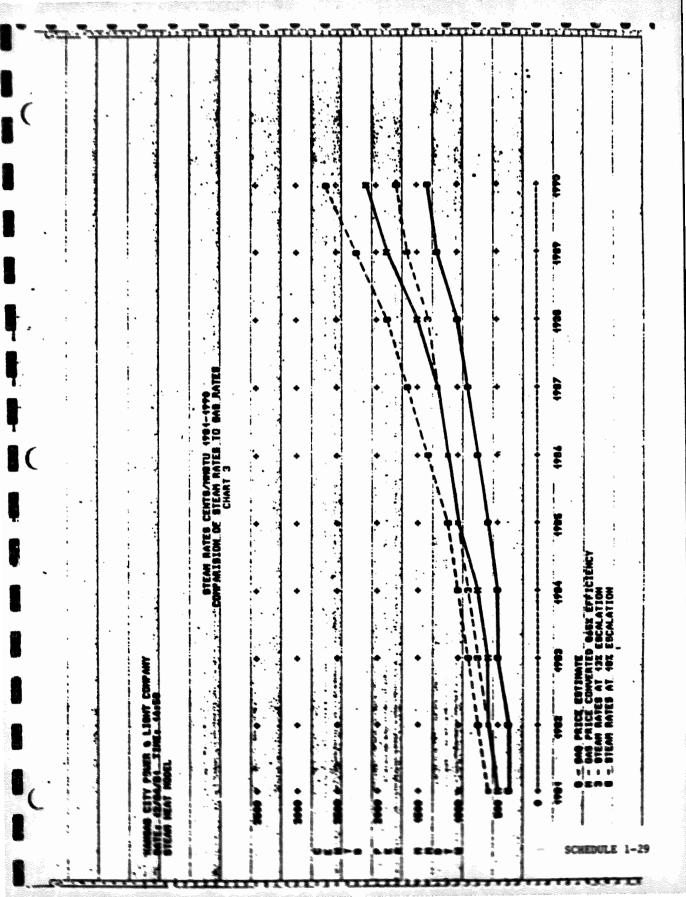
The next series of cases addresses the branches in the decision tree that assume that the price of steam escalates at the rate of variable fuel costs. For this analysis, fuel is assumed to increase at 13% per annum from 1981 to 1990. Chart 3 shows that at this rate of inflation, steam prices would be slightly above gas in 1983 and 1984, and competitive with deregulated gas in 1985 and beyond. (Chart 3 also shows that if steam increases at the rate of inflation projected for gas prices—18% per annum—then steam never becomes competitive with deregulated gas.)

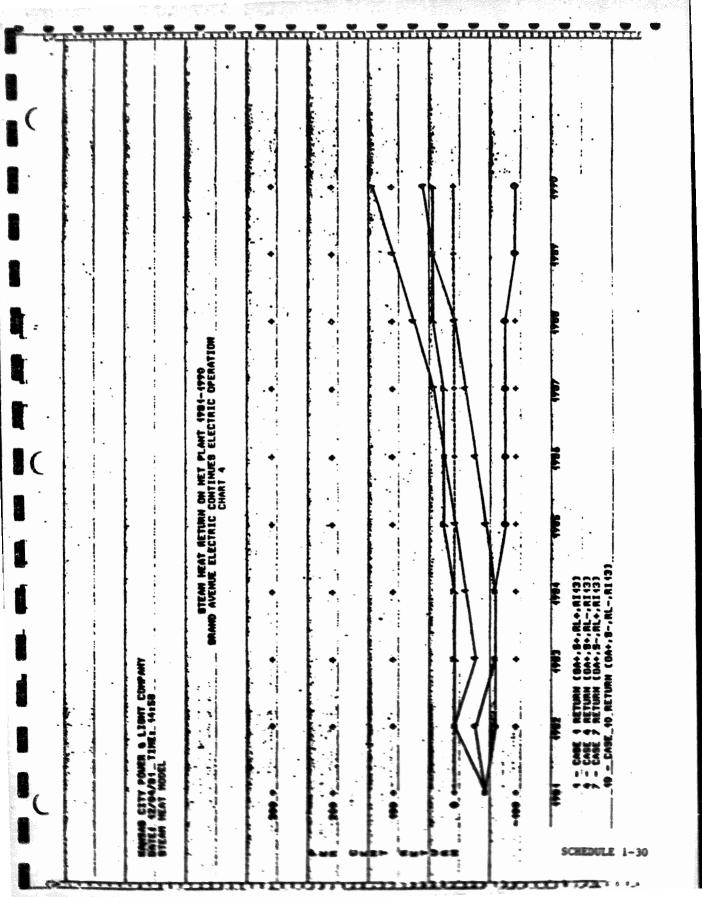
# 1. Grand Avenue Station Retired Beyond 1990

Given that steam price increases are limited to 13% escalation of fuel costs, then Chart 4 compares the rate of return earned on net steam distribution plant investment for cases reflecting changes in sales and steam losses (Cases 1, 4, 7, 10). Case 7 indicates that at a minimum, steam losses should be reduced to less than 20% just to break even over the three years and then a respectable return could be earned thereafter. Case 1, which also assumes the addition of a large customer, delays profitability to 1986. Both cases indicate rates of return beyond 1986 are considerably higher than the 13% required in the fuel cost of service cases discussed in Section III-A. This suggests that steam price increases could be held well below the rate of inflation of variable fuel costs beyond 1986 if losses are reduced (see Cases 3 and 9 on Chart 1).

#### 2. Grand Avenue Station Retired in 1984

Chart 5 plots the rates of return for Cases 13, 16, 19, 22 of the decision tree which have the same 13% steam price escalation as above but include the





|--|

effect of retiring the electric service out of Grand Avenue Station. Only

Case 13 (reduce losses, increase sales with a large customer) eventually

becomes profitable beyond 1988. This indicates that 13% increases in the

price of steam alone are not sufficient to maintain profitability while absorbing

the impact of retiring the electric side of Grand Avenue Station.

# 3. Summary of 13% Price Increase Cases

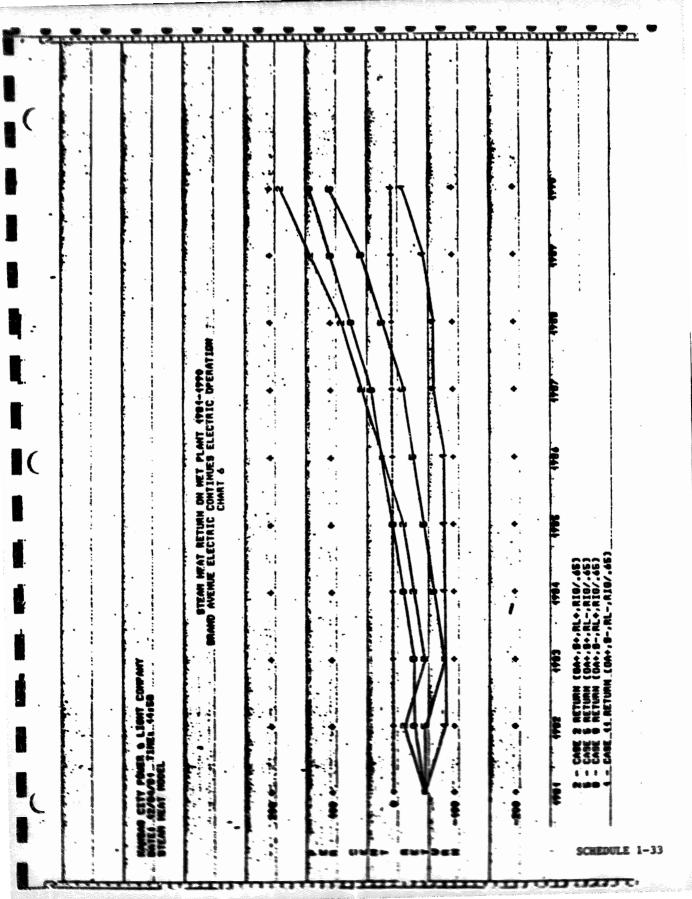
These cases indicate that steam price increases at the rate of inflation (13%) of variable fuel costs are not sufficient to achieve profitability once the electric side of Grand Avenue is retired in 1984 even if losses are reduced to 20% and a large steam sale is consummated. Even if Grand Avenue continues to operate, losses must be reduced or sales increased substantially for the steam business to become profitable.

C. Price of Steam Increased to Match Equivalent Price of Natural Gas

This aeries of cases from the decision tree assumes that steam prices are
increased annually to match the price of gas on a cents-per-Btu basis adjusted
for a 65% efficiency factor as shown on Chart 3. This section will discuss
the impact of this limitation on expected rate of return for the same assumptions
on steam losses, sales increases, and the retirement of Grand Avenue Station.

#### 1. Grand Avenue Station Retired Beyond 1990

Chart 6 indicates that if steam prices are constrained to increase no faster than equivalent gas prices, then no positive return can be earned until after 1985 even if losses are reduced (Case 8). Case 2 where both sales are increased and losses reduced does not improve profitability before 1985. Once gas is deregulated beyond 1985, then both Cases 2 and 8 become profitable. If sales are increased and losses are not reduced, profitability does not improve until 1988 as is illustrated by Case 5.



# Grand Avenue Station Retired in 1984

Chart 7 shows again that retirement of Grand Avenue Station is an impediment to profitability even after gas prices are deregulated in 1985. Case 14 shows that even with reduced losses and increased sales a positive return would not be earned until 1988.

## 3. Summary of Competitive Gas Price Cases

Restricting steam prices to competitive gas price increases would require stable prices through 1982 and then increases at an 18% per year rate thereafter. This delays a positive return until after 1985 even with reduced losses and increased sales. The retirement of Grand Avenue Station in 1984 further retards profitability until 1988. If steam prices continue to escalate at projected gas price escalation rates, however, and no major new investment is required, high rates of return may result after profitability is established.

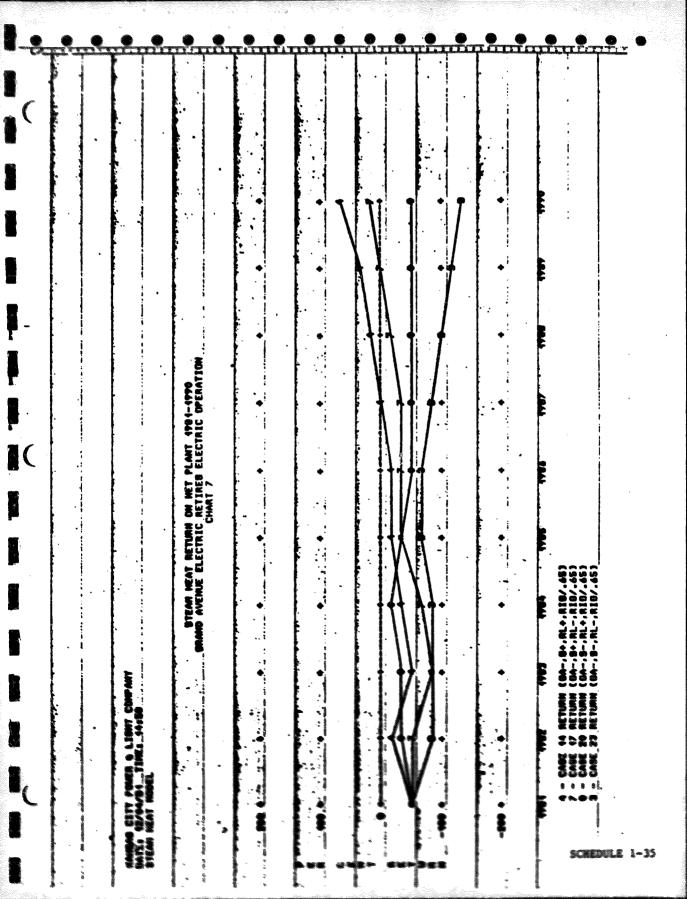
# D. Comparison of Cumulative Net Cash Flow

#### Grand Avenue Retired Beyond 1990.

Chart 8 demonstrates the cumulative net cash flow expected in cases 2, 5, 8, and 11. These cases assume that steam prices can match projected gas prices on a cents-per-Btu basis adjusted for a 65% efficiency factor. This chart shows the impact reducing losses has on cash flow. Cases 2 and 8, the cases in which losses are reduced, experience a positive cumulative cash flow in 1988. The other cases remain negative throughout the decade.

#### Grand Avenue Retired in 1984.

Chart 9 demonstrates the cumulative net cash flows for Cases 14, 17, 20, and 23. This chart shows that if Grand Avenue retires and rates match an equivalent gas price, it would take both loss reduction and a large increase in sales to experience positive cash flow by the end of the decade.



STEAM MEAT FINANCIAL STUDY 1981-1990 COMPANISION OF CUMULATIVE NET CASH FLOW CHART 8 SCHENUL 1-36

	11ML Hill	STEAN HEAT FINANCIAL STUDY 1981-1990 COMPANISION OF CUMULATIVE NET CASH FLOW CHART 9			CASE (* (009MR10/.45) CASE (* (009MR10/.45) CASE 20 (009MR10/.45) CASE 20 (009MR10/.45)
	MARKER CITY POWER & LIGHT CON- BREAM MEAT MODEL TIMES 16137				

# 3. Summary of Cash Flow Comparison

If the equivalent price of gas on a cents-per-Btu basis is an approximation for the maximum price that could be charged for steam, then reducing losses and increasing sales are the major factors leading to a positive cash flow by the end of the next ten years. It should be noted that the financial model assumes that losses are all at the customers end consequently an improvement in losses results in a revenue increase with no additional expenses. If the losses are a result of some other problem, the positive impact on cash flow may not be achievable in this decade.

Charts 8 and 9 illustrate the fact that cumulative cash requirements will most likely exceed cash inflows for the next six years or so. If steam rates escalate at a rate that is less than expected for natural gas rates (such as the projected fuel price escalation rate of 13%), then this negative cash position could persist even longer. To attain the high level of returns depicted by Cases 2 and 8 on Chart 6 will cause a cash drain in the near term. Less optimistic conditions may cause such a cash drain to continue much longer.

#### IV. CONCLUSIONS AND RECOMMENDATIONS

#### A. Conclusion

The financial impact model analysis suggests that the steam business could be made less unprofitable in the short run by reducing steam losses below 20% and aggressively applying for rate relief to bring the earned rate of return on the steam business closer to the required return of 13%. Such action would place steam prices above the competitive price of matural gas before it is deregulated in 1985. If steam price increases are restricted to

the competitive price of gas, then profitability and net positive cash inflows are unattainable prior to gas deregulation in 1985.

The addition of a very large stesm customer (twice total existing steam sales) at an assumed price, which is the equivalent price of delivered natural gas, has an immediate dampening effect on profitability because of the major shift in the allocation of costs to the steam side of the business. The assumed price of steam to the large customer should be examined to further evaluate its short run impact on earned return on steam plant investment. In the long run as the delivered price of gas is deregulated, these additional large sales provide revenue to more than cover variable costs, contribute to fixed charges and improve profitability.

The retirement of the electric side of Grand Avenue Station in 1984 has a considerable negative impact on profitability, cash flow, and the long-run price of steam relative to natural gas. This analysis indicates that retirement more than triples the allocation of boiler plant from the electric business to the steam business. The effect is to not earn the required return on the steam business without exceeding the competitive price of natural gas until the late 1980s when the full effect of gas price deregulation takes place.

### B. Recommendations

In the short run, KCPL should immediately establish the steam business as a specific profit center or KCPL subsidiary under the direction of a Director or Manager of Steam Operations reporting to a Vice President who is made responsible for developing a plan for the long-run profitability of the steam business or its eventual divestment.

He should consider the following actions:

### PAGE 21

- Seek to minimize steam business earnings losses in the short run and improve profitability in the long run for KCPL by:
  - (a) Immediate resolution of the steam loss problem.
  - (b) Pursuit of steam price increases commensurate with profitability goals and competitive energy sources.
  - (c) Investigate further the desirability of large customer additions and pricing to absorb existing or future steam capacity.
  - (d) Investigate further the impact of retiring Grand Avenue Station in its entirety and look at the feasibility and economics of providing steam supply from electric boilers supplied by electric power purchased from the KCPL system. The study should consider the possibility of competition because of the availability of smaller electric boiler installations to steam customers who would purchase electricity on a large commercial/industrial rate. How many existing customers could convert to this type of system? How would these systems compete with natural gas options?
  - (e) Analyze the accounting allocation procedures to ascertain if the allocation system accurately defines the true costs of the steam business.
- With the help of KCPL personnel (ESCC, etc.) and/or engaging a qualified consultant, investigate the possibility of KCPL divesting itself of the steam business by:
  - (a) Selling the steam business "as is" upon the retirement of Grand Avenue Station. Who are the potential buyers and on what terms? What are the regulatory considerations? What changes could be made to the business to make total or partial devestment possible?

### PAGE 22

- (b) Selling the steam business, following potential refurbishments and retirement of Grand Avenue Station as suggested under 1.(d) above. What conditions would make the sale attractive to a prospective purchaser? What are the political and regulatory considerations in the sale?
- (c) Considering an alternative to retiring Grand Avenue Station—
  refurbishing and structuring the operation of Grand Avenue Station
  as a co-generation project over the next 10 years. Establish a
  separate company which sells by-product electricity to the KCPL
  system. What would be the required price of steam and revenue from
  electric output sold to KCPL to make this alternative an attractive
  venture to a potential buyer?

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#### I - EXECUTIVE SUMMARY

# Introduction and Purpose

After supplying low-pressure steam service in downtown Kansas City for nearly 100 years, a series of recent events focused KCPL's attention on the urgent need for a long-range study of the downtown steam system. On March 9, 1982, the Electric Supply Coordinating Committee (ESCC) issued a Statement of Scope for the Long-Range Steam Heat Planning Study. The purpose of this study is to develop a recommendation for a long-range plan for KCPL's downtown steam system, with primary emphasis on a plan that is technically and economically feasible, and will contribute to maintaining steam as a competitive and reliable heat source through the year 2000.

Concentrating on the period 1984-2003, the study consists of engineering and economic evaluations of alternative plans for meeting future steam requirements. The criteria for evaluating an effective plan rests on the two basic strategies of (i) providing downtown steam service which is both reliable and competitive in price with natural gas and (ii) maintaining steam rates such that KCPL can recover the costs of steam heat operation.

### The Downtown Steam System

The downtown steam system can be separated into two components - the steam distribution system and the steam generating facility at Grand Avenue Station.

The steam distribution system consists of nearly twelve miles of underground pipe buried beneath the streets of downtown Kamsas City. Two high pressure steam mains originate at Grand Avenue Station and transport steam to two

desuperheating and pressure reduction stations, prior to final distribution to customers in the downtown area. Most of the steam distribution pipe is quite old, with less than 20% of the total footage installed since 1960 and with some sections now over 75 years old.

Steam usage is measured on the customer's premises primarily with condensate meters. Although the meter itself is an accurate device, leaks in the condensate line, intentional diversion of condensate, non-condensing uses for steam, and other factors can result in less condensate being returned to the meter than that which corresponds to actual steam usage.

Steam losses have increased substantially over the past four years, and now are reported to be between 30 and 40%. The aging steam distribution system, combined with metering problems, have contributed to this increase.

Programs are currently underway to correct this problem.

Steam for the downtown heating system is generated at Grand Avenue Station, a dual-use electric and steam facility which has been in operation since the early 1920's. There are currently three dual-fueled (coal or natural gas) boilers that provide the bulk of the steam requirements. Due to the fact that these boilers were designed primarily to serve turbine-generator needs, steam for the downtown system is generated at a higher temperature and pressure than would otherwise be required, introducing an inherent thermal inefficiency in the overall steam heat cycle.

Grand Avenue is now the oldest active generating station in the KCPL system, a factor contributing significantly to several operating constraints that impact the cost of steam. Designed in an era prior to plant automation.

operations are highly labor intensive. Further, with no electric generation, the boiler design itself limits the burning of coel to high steam loading periods, requiring that more expensive natural gas fuel be burned during lower load periods.

The customer uses steam primarily for space heating with minimal non-winter loads and summer use limited mainly to domestic hot water heating and use in kitchen facilities. This results in an extremely low system load factor - approximately 28%.

The customer base served by the steam system has been declining over the past few years, and at the end of 1981 consisted of 204 customers. Annual steam sales have experienced a corresponding decline. During 1981, steam operations resulted in book revenue of about \$3,894,000, and a year-end net operating loss of \$595,366. Presently the average price of downtown steam is about \$8.50 per MIb.

A forecast of future steam heat load was prepared for the year 1984 and held constant for the remaining 20 years in the study period. This forecast consisted of the existing customer base, adjusted for known future changes. The forecasted steam load is well within the steaming capacity of the existing Grand Avenue equipment throughout the study period.

Because of its dual function of electric generation and steam heat production, Grand Avenue is subject to a complex allocation of property and expenses for rate case purposes. When the electric generating facilities are retired, the remaining plant and expenses will be borne entirely by the downtown ratepayer.

# Steam System Scenarios

A series of related long-range planning scenarios were studied by utilizing computer programs which simulate the production and cost accounting aspects of the steam system. These scenarios concentrated upon the steam generation segment of the system, addressing the primary issues of fuel costs, electric facility retirement, boiler age and efficiency, and system load factor.

Unique cases were developed to simulate the following steam system scenarios:

- 1. A base case representing a continuation of the current steam system serving the existing customer base;
- A variation on the base case which limits downtown steam service to the six-month winter heating season only;
- The use of electrode boilers for minimum load and/or standby service;
- 4. Modifications to Grand Avenue equipment that will allow coal burning for minimum load conditions;
- 5. Substitution of either electrode boilers, coal-fired package boilers, or fluidized bed boilers for existing Grand Avenue steam generating equipment;
- 6. The addition of a new large, high load-factor customer to the existing customer base;

# Conclusions

For each of the major scenarios outlined above, the resulting cost of steam service to the customer is compared to the forecast cost of natural gas.

Based upon this comparison, and a detailed analysis of the results of the simulated steam operation, the following conclusions result:

- 1. A continuation of the present operating system of serving the existing customer base with existing facilities results in a downtown steam system which cannot be both profitable and competitive with natural gas. Contributing factors include:
  - low system load factor together with minimum load constraints on the boilers results in high use of natural gas in the six-month non-winter season;
  - inherent thermal inefficiencies of producing superheated steam for delivery to the customer at low pressure and temperature;
  - the need to provide "quick start" backup capability results in a large volume of natural gas burn to keep a boiler on hot standby; and
  - Grand Avenue Station age and design result in a very labor intensive operation with high operations and maintenance expense.
- 2. With the electric facilities retired in 1990 as planned, the downtown steam system becomes even less competitive with netural gas due to the following:

- although total station OSM is reduced by 32% with electric retirement, the loss of allocation to electric more than offsets this effect resulting in an increased cost of steam;
- the cost of steam to the customer is 1.7 times the cost of natural gas in 1990, and the cost of steam increases by a factor of 4 during the period 1982-1990.
- 3. Of the possible new technologies for generating steam, electrode boilers results in the lowest cost steam; however, steam is still not competitive with natural gas in the near-term;
- 4. Shutdown of the steam system during the six-month off-peak period, use of electrode boilers for standby, and the burning of coal at minimum load all result in a reduced steam cost but the system is still not competitive with natural gas until late in the study period;
- Addition of new winter peaking, low load-factor steam loads does nothing to improve the viability of the steam system;
- 6. Fuel and OSM expenses represent 81% of the cost of providing downtown steam in 1990. To make the existing steam system competitive with natural gas after Grand Avenue electric facilities are retired, projected fuel and OSM expenses have to be reduced by about 50%. It is unlikely that such a reduction could be achieved while retaining an acceptable level of service;

- 7. Investigations currently underway may identify method which could reduce operating costs in the short-term. These would include:
  - coal mill and burner modifications to permit coal burning at low steam conditions thereby reducing fuel costs:
  - reduced pressure boiler operation to mitigate thermal cycle inefficiency; and
  - transfer of major maintenance projects to Central Maintenance to reduce maintenance labor at Grand Avenue.
- 8. The addition of a new large, high load-factor customer has the effect of lowering the cost of downtown steam such that the system is competitive with natural gas. This results from the following:
  - increased system load factor permits coal to be burned year round, reducing fuel cost per Mlb by about 40% in 1990;
  - O&M expense is spread over more units of output reducing
     O&M cost per MIb by over 60%;
  - even with electric retirement, the price of downtown steam in 1990 is reduced from \$38 to \$23/Mlb and the cost to the customer is competitive with the cost of natural gas.
  - downtown steam remains competitive as long as the new customer is on the system and provided that no large capital expenditures are needed.

# Recommendations

Based upon the results of this study, the following long-range plan is recommended for the steam system:

- Add a new large, high load-factor steam customer as soon as possible but definitely prior to the retirement of electric facilities at Grand Avenue;
- 2. In the interim period until the new large customer has been added, continue to operate Grand Avenue as a joint electric and steam plant and improve steam's competitive position with natural gas by implementing cost saving measures which include:
  - greatly reducing natural gas usage for boiler hot standby and under minimum load conditions;
  - reducing labor expense by shifting major maintenance projects to Central Maintenance;
  - investigating the possibility of reducing coal costs by purchasing Grand Avenue coal from small suppliers on the spot market during periods of soft market conditions.
- Continue to run the existing coal-fired Grand Avenue boilers for the foreseeable future to avoid large capital expenditures required for a techology changeover;
- 4. If there is no prospect for the addition of a new large, high load factor customer, the following course of action should be considered:

- by year end 1985, "freeze" the availability of the steam rate to prevent new customer entry onto the system;
- upon retirement of electric facilities at Grand Avenue, consider the possibility of seasonal steam service only during the slx-month heating season to reduce fuel and OSM expense;
- as the customer base is reduced through attrition,
   continue to aggressively pursue plant and expense
   cutbacks at Grand Avenue Station;
- at the point that electric heat becomes competitive with steam heat, promote customer conversion with an incentive such as leased electrode boilers and/or an incentive electric heat rate.
- 5. Update the study of downtown steam at intervals no greater than every two years. In the interim, continue to investigate and where appropriate, implement, cost reduction measures particularly as they relate to fuel and O&M expenses.

### 11 - INTRODUCTION

Low-pressure steam service has been supplied to downtown Kansas City for nearly 100 years. Although provided since 1929 as a convenient by-product of electric generation at Grand Avenue Station, downtown steam has now grown to be depended upon as a primary heat source for most of the downtown business district.

As electric operations at Grand Avenue have declined in magnitude and importance, steam costs have risen and steam service has become more of a primary product of Grand Avenue operations. For the past several years there has been growing awareness that Grand Avenue overall equipment age and condition could eventually limit future steam heat business. This general perception was crystallized with the November 1981 approval of KCPLAN which projected the retirement of Grand Avenue electric facilities by about 1990. Although KCPLAN identified the refurbishment of older coal-fired generation as an alternative to retirement at some stations, a subsequent study by Black & Veatch confirmed earlier indications that Grand Avenue electric equipment was beyond the point of economic revitalization.

At this same time, four other separate but related events helped focus attention on the urgent need for a new long-range study of the downtown steam system. First, the conversion of a major downtown retail store to natural gas heating raised concern for both the immediate and long-term competitiveness of steam heat.

Next, the request by a major industry for process steam that could eventually more than triple annual steam output and increase peak-hour demand by 70% focused attention on the aging Grand Avenue steam facilities. Third, questions were raised as to the long-term availability and cost of steam heat as Kansas

City enters a period of downtown revitalization. And, finally, an internal report presented several questions concerning the long-term financial viability of the present steam heat system.

in response to these challenges, the internal management of the steam heat system received renewed attention in early 1982. Subsequently, on March 19, 1982, the Electric Supply Coordinating Committee (ESCC) issued a Statement of Scope for the Long-Range Steam Heat Planning Study.

# III - PURPOSE

The purpose of this study is to develop a recommendation for a long-range plan for KCPL's downtown steam system. The primary emphasis of the study is to develop a plan that is technically and economically feasible, and will contribute to maintaining steam as a competitive and reliable heat source for the downtown area through the year 2000.

Concentrating on the twenty-year period beginning in 1984, the study consists of engineering and economic evaluations of alternative plans for meeting future steam requirements. Development of the plans examined in the study was guided by the following presuppositions:

- 1. KCPL will continue to provide steam heat service in the future;
- Alternatives such as discontinuing service, divestiture, or establishment as a nonregulated subsidiary are beyond the scope of this study; and
- Solutions to immediate problems, such as large steam losses, are assumed to be successfully implemented as planned in the period prior to 1984.

The criteria for an effective long-range plan rests on two basic strategies:

- (i) providing downtown steam service which is competitive with natural gas as an economic and reliable heat source for the long term; and
- (ii) maintaining steam rates such that KCPL can recover the fixed and variable costs of steam heat operation, while earning an adequate rate-of-return on steam heat investment.

Both of these strategies must be effectively satisfied to keep the steam system viable.

# IV - EXISTING STEAM SYSTEM

The distribution of steam for heating purposes in downtown Kansas

City was begun in 1888 by the Kansas City Electric Light Company from its

electric generating station at 604 Wall Street. The system was expanded to a

larger customer base in the following years and a second source of steam

supply was added at 1308 Baltimore. In 1929, Grand Avenue Station began supply
ing high pressure (185 psig) steam to the downtown area. Over the years, the

two older stations at Wall Street and Baltimore were phased out as Grand Avenue

Station assumed more of the steam load.

The downtown steam system can be separated into two components. The first is the steam distribution system - nearly twelve miles of underground pipe beneath the streets of Kansas City. The second is the steam generating facility at Grand Avenue Station.

# **Distribution System**

The downtown steam system covers about 100 square blocks in the downtown business district, extending approximately from 6th Street on the north to 14th Street on the south. The west boundary is Broadway and a high pressure steam line runs as far east as Holmes.

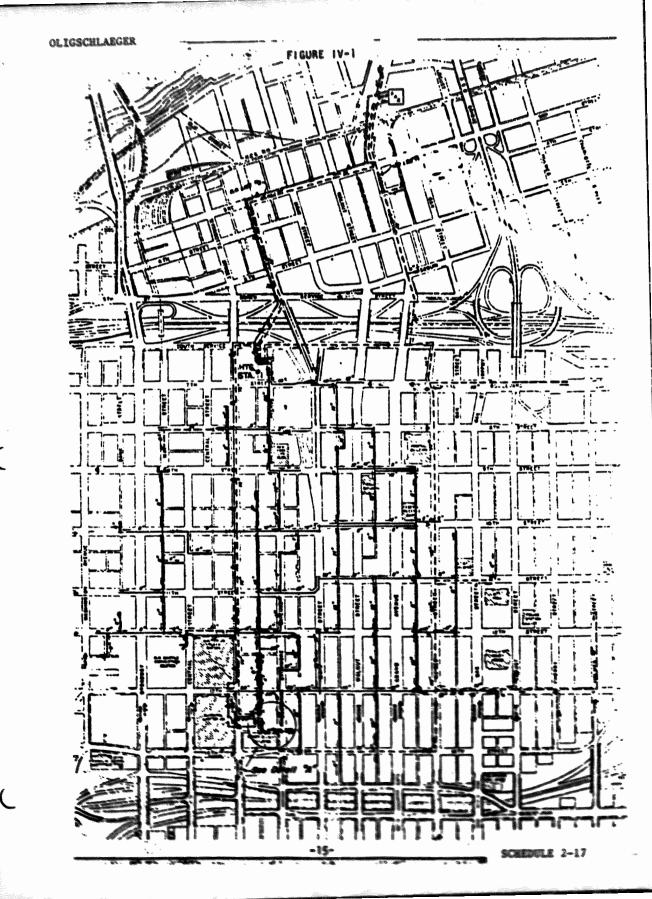
Two high pressure (185 psig) steam mains originate at Grand Avenue Station, each capable of carrying the entire downtown steam load. The high pressure steam is transported to two desuperheating stations located at 1319 Wyandotte and 604 Baltimore (the old Wall Street steam plant Site). At the desuperheating stations, the steam pressure is reduced to 105 psig and 15 psig for distribution to the majority of customers. After the steam is used, the condensate is

discharged to the sewer system requiring total make-up from city water at Grand Avenue Station. A diagram of the downtown steam system is shown on Figure IV-1.

The last major steam main extension took place in 1958 when the second high pressure line from Grand Avenue was installed. Less than 20% of the total 62,000 feet of steam distribution mains has been installed since 1960. Some sections of the downtown distribution network date back to the Kansas City Heating Company and are over 75 years old.

An important element of the distribution system is the metering. Steam is measured and billed in units of thousands of pounds (Mlb.) through either a flow meter or a condensate meter. Flow meters are an electro-mechanical device that directly measure the volume of steam. This type of meter is not commonly used on KCPL's system for two reasons. First, a flow meter is more costly than a condensate meter and, secondly, it requires a relatively long length of straight steam flow at the entrance to the customer's property. For the latter reason, its applicability is severely limited.

Condensate meters are commonly used on the downtown steam system. A mechanical device, the condensate meter measures steam input into a building by measuring the condensate flow out of the building. After the usable heat has been extracted from the steam, the steam condenses - returns to water - and is piped through the meter before discharge to the sewer system. Although the condensate meter itself is an accurate device, the potential for inaccurate measurement of steam input to a building is great because all the condensate may not be returned through the meter. Leaks in the condensate line, intentional diversion of condensate, and non-condensing uses for steam such



as humidification can result in less condensate being returned through the meter than steam input to the building.

System steam losses have increased substantially over the past four years. Until 1978, losses (measured as the difference between steam sendout at Grand Avenue and steam metered on the customer premises for billing) generally were between 10% and 20%. In the last four years, losses have steadily increased to between 30% and 40%. The decline in load levels, aging steam distribution system, and metering problems have contributed to this increase.

A number of measures have been implemented in the last several months to correct the high loss problem. Formal schedules have been established for steam maintenance, meter reading, inspections and other operating activities. The Steam Department is utilizing infrared scanning to detect leaks in the system and customer inspections to identify condensate leaks, diversions, and faulty meters. The number of people assigned to steam maintenance has increased from five to ten, including a maintenance supervisor and two labor crews.

Because of the corrective action currently underway, for this study losses were assumed to be 20% - a significant improvement over recent history. The reduction in losses to 20% seems reasonable in light of the fact that losses averaged only 13% for the period 1960 to 1978.

### Grand Avenue Station

In 1927, KCPL purchased the facility that later would be known as Grand Avenue Station. The station began providing steem service in 1929 and through the years was modernized until by 1950 it assumed essentially the equipment configuration that exists today.

There are currently three dual-fueled (coal or natural gas) boilers designated #6, #7, and #8 that provide the bulk of the steam requirement. Full-load steaming capability of the boilers totals 910,000 pounds per hour and is distributed as follows:

Boiler #6 340,000 lbs./hour Boiler #8 285,000 lbs.hour
Boiler #7 285,000 lbs./hour

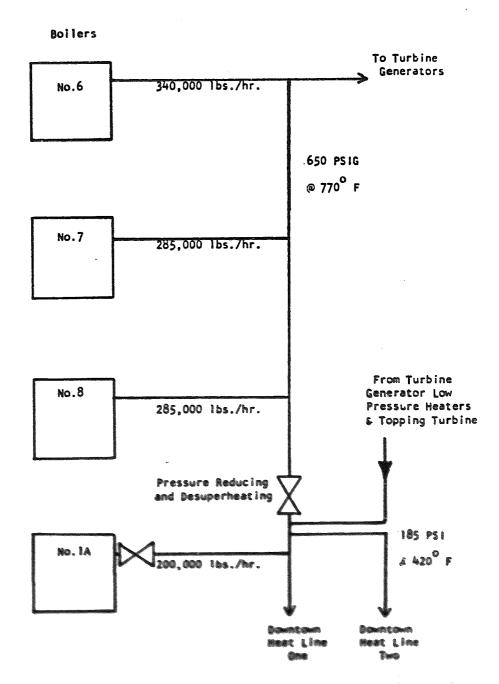
In 1969, IA boiler, an oil and natural gas fueled package boiler with a 200,000 lb./hour capability, was added to supplement the station steam supply.

As shown in Figure IV-2 the three large coal-fired boilers are connected through a common header. Steam at the header can be extracted for sendout to the downtown steam system or passed through a turbine for electrical generation. Boiler IA, which is currently in need of major repair, produces lower pressure steam for use directly in the downtown steam system or for boiler feedwater heaters. Because of the turbine requirement, superheated steam is produced at about 650 psig by the three coal-fired boilers. The steam is then cooled (desuperheated) and the pressure is reduced to 185 psig for sendout to the high pressure steam system.

In the winter, at times of high steam heat load, a portion of the steam heat sendout is first passed through #5 turbine generator. This turbine (a so-called "topping" turbine) acts as a pressure reducing valve which utilizes high pressure, superheated steam to produce electricity and then exhausts 185 psig steam to the downtown steam system. This is a very efficient cycle but it can only be used in winter when the downtown steam load is high.

In the 1970's, electric generating capability at Grand Avenue was as high as 108 MV. Over the past few years turbine generators have been retired or put on inactive reserve status so that current accredited capacity is 40 MV. Retirement

# STEAM GENERATOR FLOW DIAGRAM



of the remaining electric generation at Grand Avenue is projected for 1990.

Although the amount of capacity at Grand is relatively minor, the importance of that capacity is not. The downtown area is served electrically through a low voltage underground network system. In the event of multiple system contingencies that would interrupt electric service to the downtown network, Grand currently provides the electrical backup for the Kansas City business district.

Because of its dual function of electric generation and steam heat production, Grand Avenue is subjected to a complex allocation of property and expenses for rate case purposes. Historically, the allocation had been based on the premise that Grand Avenue was primarily an electric generating station with steam a secondary product. In recent years, as Grand has assumed primarily an electrical peaking function and as generation has been retired or deactivated, the steam heat segment of the business has assumed an increasing share of the Grand Avenue costs. If the remaining electric generating facilities are retired in 1990, the remaining plant and expenses will be borne entirely by the downtown steam ratepayer.

It is important to understand some of the inherent operating constraints at Grand Avenue that contribute to the cost of steam. These include (i) the relatively high OSM expenses associated with the station, and (ii) design and operating constraints that adversely impact fuel costs.

# (i) OSH expenses

Grand Avenue is now the oldest active generating station in the KCPL system. Purchased in 1927, the station was originally designed and operated to provide 25 hertz electric power for the streetcar system.

Although reconstructed after its purchase with new coal-burning facilities added in the late-1940's, Grand Avenue remains an essentially non-automated power plant characteristic of the late 1940's. This basically labor intensive operation is further increased by the station's age which requires that a great deal of maintenance be performed to keep equipment operating properly.

### (ii) Fuel Costs

The largest component in the cost of steam is fuel expense. Here, as in the case of O&M expenses, Grand Avenue's physical characteristics present some significant problems.

Located on the Missouri River adjacent to the main business district of Kansas City, Grand Avenue has limited space for coal handling and storage facilities. As a result, coal for Grand Avenue is delivered via unit trains to Hawthorn Station, with a few coal cars subsequently diverted to Grand Avenue as needed. Coal unloading is a time consuming manual process, using a gantry crane and conveyor system. Both of these factors add to the transporation and unloading costs of Grand Avenue fuel, and directly impact the coal cost reflected in the steam rate.

Steam can be produced at a moderate fuel cost on coal, but because of minimum load constraints, high cost natural gas must be used to produce steam during most of the six-month non-winter season. When downtown steam load falls below 100,000 pounds per hour and there is no need for electric generation, the boilers must be fired with natural gas because of inherent boiler instability and coal pulverizer limitations.

contributing to the high fuel cost is the natural gas burned to keep a boiler on "hot-standby". Boilers take several hours to be brought up to operating pressure and temperature. Consequently, in order to provide reliable service in the event of forced outage of the primary boiler supplying steam service, a second boiler must be kept hot by the use of natural gas pilots. At present, the estimated cost of natural gas for hot standby is approximately \$650,000 per year.

Another factor that affects fuel efficiency for downtown steam production is the boiler design itself. The boilers are designed to produce the superheated steam under conditions necessary for the electric turbines. The steam for downtown heat is then desuperheated and the pressure reduced for sendout. This requires fuel input to the boiler of approximately 1700 BTU to produce a pound of steam for sendout that has a heat content at the customer's premises of about 1200 BTU. A boiler designed solely to produce the lower pressure and temperature steam necessary for the heat system would require significantly less fuel input.

# V - FUTURE STEAM LOAD

Forecasting future steam load is essentially an empirical process, subject to a considerably less rigorous process than that followed in electric load forecasting. It essentially consists of evaluating the existing customer base and their possible changes in the future, adding in the effects of new customer additions, and finally adjusting for perceived future economic and competitive conditions. This was the process followed in developing the steam forecast for this study.

# Existing Customers

At the end of 1981, KCPL had 204 customers receiving downtown steam service. This represented a 3% decline from 1980, and a decline of 68 customers since 1971 when the system served a total of 272 customers.

Annual steam sales in 1981 were about 500,000 Mlbs., with a peak steam demand of about 364 Mlbs. per hour experienced during the winter season. Due to an unusually mild winter during 1981, steam sales were especially low. A more representative year would be 1980, at which time annual steam sales were about 634,000 Mlbs., with a peak winter demand of about 383 Mlbs. per hour.

Annual steam sales have also declined over the past 10 years from a 1971 level of 1,141,000 Mlbs.

The price of steam has increased significantly over the past few years. Presently, the average price of steam is about \$8.50 per Mib. This compares to a 1971 average rate level of about \$1.50 per Mib., which had been held essentially constant since the early 1960's. During 1981, steam operations generated

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book revenue of \$3,894,125, resulting in a year-end net operating loss of \$595,366.

As previously discussed, steam sendout or input into the system is metered at Grand Avenue Station. Steam sales are metered on the customer premises. However, because the metering is primarily of the condensate type, the meter registers sales volume <u>after</u> it has passed through the customer's internal piping system. The difference between sendout and sales are the system losses.

Table V-1 illustrates the declining trend in steam sales over the last decade.

Steam input has also declined, but at a lesser rate so that losses have increased substantially.

# Forecast

A 1984 projection of the peak hour steam sendout of 359,000 pounds per hour was used as the starting point forecast for the study. The peak load and annual steam sendout were then adjusted for known changes, such as the addition of the Vista Hotel and two other major downtown office projects. In addition, steam sendout was reduced by 5% in order to recognize that less steam will be required as system losses are reduced from the current 40% to 20%. The assumption is that of the projected 20% reduction in losses resulting from corrective action currently underway, one-fourth (5%) is due to correctable problems with the steam distribution system. The remaining three-quarters (15%) of correctable losses were acided to the projected steam sales because it occurs beyond the point of delivery to the customer, either through unmetered condensate or malfunctioning meters.

The adjusted forecast is a 1984 peak steam load of 364,000 pounds per hour, with annual sceam sendout of 887,000 hibs. Losses are 20% resulting in annual

TABLE V-1

# HISTORICAL GRAND AVENUE STEAM HEAT STATISTICS

	Customers Connected	Input to System (MMLB) (Less Company Use)	Sales (MMLB)	2 Loss
1971	272	1346.5	1141	15.3
1972	259	1354.5	1169	13.0
1973	258	1218.8	1139	6.5
1974	251	1137.6	882	22.5
1975	252	1120.1	922	17.7
1976	253	1126.6	868	23.0
1977	248	1115.0	308	18.6
1978	222	1243.5	864	30 . 5
1979	218	1195.5	764	36.1
1980	272	1053.0	634	39.8
1981	204	920.0	503	44.8

#### OLIGSCHLAEGER

steem sales of 709,600 Mlbs. The forecast was considered a constant over the study period.

### Load Factor

Steam is used primarily for space heating with only minimal non-winter load. The resulting system load factor is very low - approximately 28%. The forecasted winter peak load of 364,000 pounds per hour contrasts sharply with the forecasted summer minimum load of about 15,000 pounds per hour. Figure V-l is a plot of the forecasted monthly peaks illustrating the seasonal load shape. Summer use is limited primarily to domestic hot water heating and use in kitchen facilities. The Federal Office Building, the largest summer steam consumer, is in the process of converting from steam turbine driven air conditioning to an electric drive system.

In 1972, system load factor was severely degraded with the closing of the Schlitz Brewery. The brewery was not only a large steam user, but it was a high load factor consumer using large volumes of steam in all months of the year.

The importance of load factor improvement cannot be overemphasized. A substantial increase in off-peak sales during the non-heating season could greatly reduce overall cost of steam production by negating the minimum load constraints at Grand Avenue Station. If off-peak steam sendout can be increased to over 100,000 pounds per hour, coal can be burned instead of high cost natural gas. The reduced fuel cost coupled with the largely fixed operations and maintenance expenses being distributed over more pounds of steam output would greatly reduce the cost per pound to the customer. The steam load duration curve in Figure V-2 illustrates the extent of the problem. Over 60% of the hours in the year, load is less than 100,000 pounds.

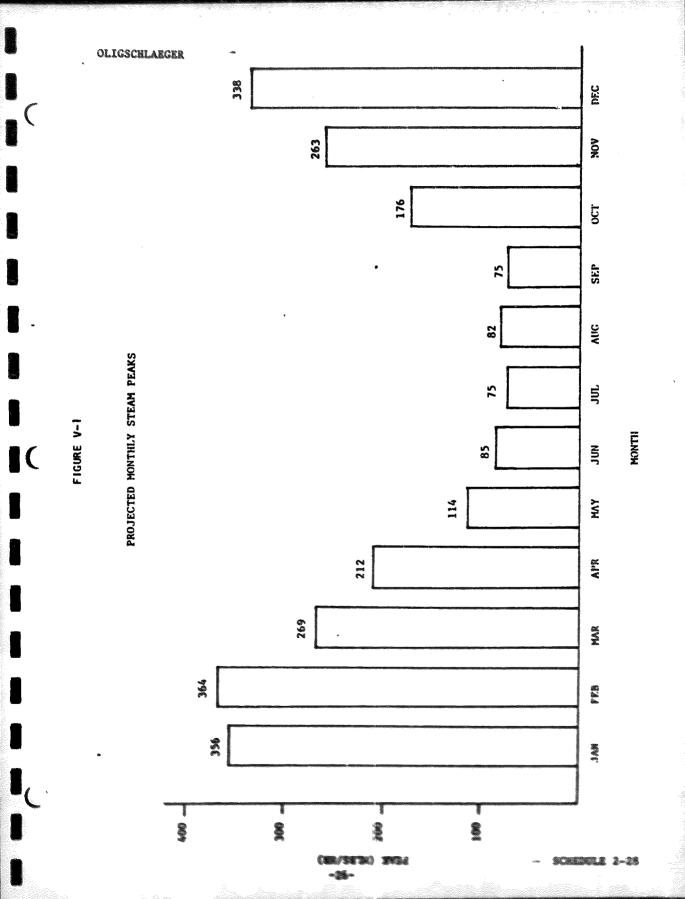
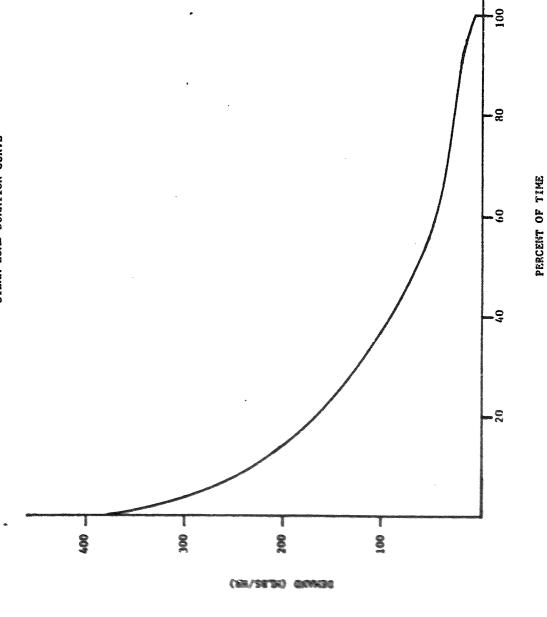


FIGURE V-2

STEAM LOAD DURATION CURVE



### VI - KEY STUDY ISSUES

The scope of this study covers the 20 year period from 1984 through 2003. 1984 was selected as the starting point for the study in order to avoid modeling short-term operational changes currently being implemented in the steam system and to "filter out" the effects of the current general business slowdown. A horizon year of 2003 was chosen so that the period of study is sufficiently long to test both the implementation and impact of various alternatives. Primary analysis, however, will concentrate on the early years of the study period.

### Overview

The critical year in the study is 1990, when the electric generation facilities at Grand Avenue Station are projected for retirement. At that point in time, the remaining boiler facility will have been in service for over 40 years. As a result, in all cases studied, electric generation was retired in 1990.

The study effort concentrates on the steam generation segment of the system. The present level of distribution system O&M expense was increased by 50% and escalated into the future. The increased distribution system expenditures are projected to reduce distribution system losses from 40% to 20% by 1984 and maintain a reliable distribution system in future years. To put the increased distribution system expenditures in perspective, the amount of increase could cover the installation of over 400 feet of new steam main annually in addition to the present level of activity.

The steam generating system at Grand Avenue presents a number of existing operating constraints that have a major impact on the cost of downtown steam. In addition, the future retirement of electric facilities, the addition of a large industrial customer, or the eventual replacement of the existing boilers each

have an impact on the downtown steam customers. Scenarios examined in the study addressed each of these subjects. In all cases, a 13% rate of return on net plant was held constant.

Herein follows a brief description of the primary issue addressed in the study by means of computer simulation of the steam system.

### Fuel Mix

The present fuel mix at Grand Avenue is approximately 40% natural gas and 60% coal. Of the \$4.5 million fuel cost experienced during 1981, over half was for natural gas. As discussed in Section IV the large gas burn is the result of two operating constraints - minimum load and hot standby.

In an attempt to overcome these fuel cost obstacles, cases were constructed to reduce the natural gas burn by substitution of electrode boilers for hot standby and to carry the steam load during low load periods. Electrode boilers have the capability to reach operating temperature and pressure in a matter of minutes rather than hours, without the pilot fuel requirements. The tradeoff is the capital cost for new electrode boilers. Electrode boilers used in this operating mode can be thought of as "peaking" units much the same as combustion turbines on the electrical system.

Another possibility that was studied to reduce the natural gas burned during minimum load conditions was to convert to a seasonal form of service. Steam heat could be provided only during the six-month winter space heating season. Not only is there an obvious fuel savings, but QCM expense could be reduced significantly. This mode of operation is possible only if the electric generation is retired.

### Electric Retirement

In all cases, electric is projected to retire in 1990 resulting in an increase in cost of steam charged to the downtown customers. Under the present allocation method for this dual function generating station, approximately 80% of the plant and over 75% of non-fuel operations and maintenance are allocated to electric. Of the total 1981 Grand Avenue fuel burn of \$4.5 million, \$2 million was charged to electric generation. The net electrical generation for 1981 was 21,600 megawatt hours.

The retirement of Grand Avenue electric facilities results in a reduction in total property and a significant reduction in O&M expense (estimated at about one-third of the present total). However, the remaining plant and expenses, part of which were previously allocated to electric, are then directly assigned to downtown steam. The overall impact is that elimination of the dual function and the allocation of plant and expenses overshadows the reduced expense benefit of electric retirement resulting in increased cost of steam to the customer.

### Boiler Age and Efficiency

By 1990, the boilers at Grand will be 40 years old or older. As discussed in Section 1V, these boilers are designed to produce turbine quality steam (650 PSIG and 770°F) which requires more fuel input than would be necessary to produce the quality of steam necessary for downtown heat customers (185 PSIG and 420°F). To overcome this thermal inefficiency, alternate technologies were studied with the objective of completing a steam equipment change-over by 1990.

New boilers could greatly increase fuel efficiency, reduce operations and maintenance expense and extend the life of the system. The trade-off is the high capital cost required for essentially a new plant. A description of the new

technology aptions studied follows:

1. Electrode Boilers. Commercial electrode boilers are readily available in sizes up to 135,000 pound per hour steaming capacity. The boiler is a single steel pressure vessel with water pumped through during the heating process. An electrical current is passed through the water using the resistance of the water as a heat generator. KCPL has electrode auxiliary boilers in service at latan Generating Station.

The advantages of electrode boilers include significantly lower OSM costs and capital costs compared to similar sized coal fired boilers. In addition, an electrode boiler requires minimal space, it is efficient, and it can be designed to supply steam at the pressure and temperature necessary for direct sendout to the system.

The preliminary concept for this alternative was to install electrode boilers on the Grand Avenue Station turbine deck when electric generation is retired to take advantage of the existing electrical system to the generators. This would also permit installation of electrode boilers independent of the final disposition of the existing coal-fired boilers.

Preliminary cost estimates in 1982 dollars is \$1 million for a 135,000 pound per hour electrode boiler. In addition, one 40 MVA transformer would be required to support the operation of four electrode boilers. Additional boilers would require additional transformation capability. Cost of electrical.

energy input was assumed to be KCPL's then current system average cost of fuel and OSM.

2. Package Boiler. Coal-fired package boilers are commercially available, however, they require all of the current clean air equipment (scrubbers and precipitators) usually associated with large electrical generating stations. Because of the space requirement for this type of system, the addition of package boilers would be difficult without dismantling the existing boilers.

Estimated 1982 cost of a 135,000 pound per hour package boiler is \$14 million, including installation of coal, lime and ash handling systems.

3. Fluidized Bed Boilers. In a conventional coal-fired boiler, pulverized fuel is fed into the boiler flame where combustion takes place in the air stream. A fluidized bed boiler is different in that a bed of coal and limestone is combusted in the lower portion of the boiler. Fluidized bed technology is capable of coal-fired operation without complex air quality control equipment and still meets flue gas limitations imposed by current air quality regulations.

One commercial size boiler is currently marketed in the United States based on developmental work done in Finland where nine such boilers are in operation burning various fuels, including trash, peat, and coal. The cost estimate in 1982 dollars for a 135,000 pound per hour fluidized bed boiler is \$9 million.

Although this is significantly less than a conventional package boiler, the operating costs for fluidized bed are estimated to be significantly higher.

### Load Factor

As previously discussed, load factor improvement could have a significant favorable impact on the cost of downtown steam and was therefore studied in detail. The addition of a large industrial process load with a very high load factor could eliminate the natural gas burn during low load periods. In addition, the largely fixed OSM expenses and return on net plant could be spread over more units of output. The impact of these two effects can result in a greatly reduced cost per unit of steam output.

#### VII - PLANNING SCENARIOS

The series of related long-range planning scenarios were studied by utilizing the Power System Simulation (PSS) program for production costing and a simplified accounting model for approximate steam cost to the customer. These planning scenarios first involved the development of a base case, which represented a continuation in the future of the present steam system serving the existing customer base. Subsequently, variations from this base case were developed which were directed toward exploring the key issues reviewed in Section VI. For each scenario, the cost of steam service to the customer, expressed in cents per million BTU and in dollars per MIb., is compared to the cost of natural gas to the customer in the years 1990 and 2003.

The FSS program was modified to simulate the operation of the downtown steam system, with the Grand Avenue boilers dispatched to meet bi-hourly steam loads. A load model for downtown steam was constructed from actual load shape date for periods that closely matched the 40 year average heating degree days. The PSS program calculated annual fuel and OSM expense for Grand Avenue steam service.

The fuel and OSM expense was used as input to a simple model that simulates the cost accounting for the steam heat business in order to estimate the price of steam to the customer. The calculation is not intended to be a precise determination of steam price, but rather an estimate. For example, the model uses net plant-in-service as a surrogate for rate base and it does not include working capital nor is it offset by deferred income tax reserves.

\*\*Example\*\*, these are relatively minor components of the overall revenue require
\*\*Tagic with fuel and production OSM representing over \*\*OX of the cost of service.

A complete list of the engineering and economic parameters used in this study are contained in Appendix A. In addition, copies of the detailed computer output summaries for each major scenario are contained in Appendix B.

The following summarizes the results obtained for each major scenario developed:

Case 1 (Base). The Base Case represents a continuation of the current steam system serving the existing customer base, and essentially represents a "business as usual" approach. Grand Avenue continues as a dual function station until 1990, at which time the electric generation is retired and overall OSM expenses are reduced to reflect the related labor and materials savings. Labor is reduced by approximately one-third as the authorized manpower dropped from over 140 to 94 people. Materials for turbine generator related maintenance are eliminated resulting in about a 15% reduction. All remaining expenses are directly charged to downtown steam, and as previously noted, results in an overall increase in steam system OSM.

Natural gas continues to be burned for hot standby at the rate of 20 MCF per hour throughout the year. Gas also continues to be burned in the primary boiler whenever steam load is under 100,000 pounds per hour. Boilers #6, #7, and #8 are dispatched to meet load and boiler IA is not considered operational for this case.

Table VII-1 compares the cost of steam to natural gas for the years 1990 and 2003. Steam is not competitive with gas in the 1980's and the price spread increases with the retirement of electric in 1990. The price of steam from 1989 to 1990 increases from \$26/Mlb. to \$38/Mlb. - almost double the price of gas.

The next series of cases were developed to simulate methods of reducing the cost of steam primarily through fuel and O&M savings.

Case 2 (Seasonal Service). Given the results of the Base Case, Case 2 eliminates the non-heating season natural gas burn by shifting in 1990 to six-month (winter) seasonal service. In 1990 this results in significant savings of about \$8 million (40%) in fuel and O&M as compared to the Base Case. As shown in Table VII-1, the price of steam is reduced about \$6/Mlb. to \$32/Mlb., but natural gas is still the cheaper heat source.

The OSM reduction with seasonal service reflects the reduction in labor expense during the summer. The personnel removed during the summer could conceivably be shifted to Hawthorn 1-4, provided that Hawthorn is at that time still operating as a seasonal peaking unit. The two stations could complement each other in regard to manpower.

Case 3 (Electrode Boilers for Standby). Case 3 utilizes two 135,000 pound per hour electrode boilers for standby service to eliminate the natural gas burn for hot standby. A coeffired boiler is retired coincident with the installation of

the electrode boilers. The price of steam in 1990 is \$33.50/ Mlb. but steam still cannot compete with natural gas.

Case 4 (Electrode Boilers for Minimum Load). This case is an extension of Case 3. With the electrode boilers already in place for standby service, they could be operated during minimum load conditions to reduce natural gas burn and 06M expense. Operation of electrode boilers in non-heating months would permit a significant further reduction in manpower at Grand Avenue. The 1990 cost of steam is reduced by about \$11/Mlb., however, the price of steam is still not competitive with natural gas until late in the study period.

Case 5 (Coal for Minimum Load). Case 5 analyzes the cost effect of burning coal under all load conditions. Although not possible at this time, investigations are underway to determine the feasibility of coal mill and boiler modifications that could reduce or eliminate the minimum load constraint on coal burning.

The effect of achieving these modifications is that the 1990 fuel cost was reduced by \$5 million from the \$12.3 million in the Base Case. Steam at \$30.20/Mlb., however, is still 40% higher in cost than natural gas. In addition, the actual savings achieved would be less than that shown in Table VII-1 if some as yet undetermined capital cost is included for the conversion.

### TABLE VII-1

### STEAM PRICE TO DOWNTOWN CUSTOMERS

CASE	<u>1990</u>	2003
Natural Gas	1950¢/MBTU	7223c/MMBTU
Base	3282¢/MMBTU \$38.2/M#	10342c/MMBTU \$120.3/M#
Seasonal Service	2752c/MMBTU \$32.0/M#	8317¢/MBTU \$96.7/M#
Electrode Boiler for Standby	2884¢/MMBTU \$33.5/M#	8729¢/MMBTU \$101.5/M#
Electrode Boiler for Minimum Load	2314¢/MMBTU \$26.9/M#	6532c/mmstu \$76.0/m#
Coal for Minimum Load	2600¢/MMBTU \$30.2/M#	7756c/MMBTU \$90.2/M#

The next series of cases simulate complete changeover to a new steam generating technology by 1990. The new technologies offer substantial fuel and OSM savings, but all require large capital expenditures.

# Cases 6, 7, and 8 (Electrode Boilers, Coal-Fired Package Boilers, and Fluidized Bed Boilers.

In these cases, new technologies are phased in prior to 1990 to replace the existing steam generators at Grand Avenue. Electrode boilers represent a high fuel cost option with low capital and 06M cost while coal-fired options have high capital cost and low fuel and 06M cost. Table VII-2 shows the cost of steam in 1990 and 2003. In all cases, the Installation of these new technologies result in a steam price well in excess of natural gas in 1990. The electrode boiler case did result in significant savings from the Base Case, and in the long term appears competitive with natural gas.

The next series of cases simulate the addition of a new, high load factor customer:

Case 9 (Large Customer). A large customer was added in 1984 and electric facilities were retired in 1990. The customer was assumed to have a peak load of 250,000 pounds per hour at 100% load factor. The steam sendout at Grand Avenue increased from 887,000 Mlbs. per year to 3,055,000 Mlbs. The price of steam to the large industrial customer was well below the cost of natural gas. Because of the additional steam load, reliability of service was maintained by rehabilitating 1A boiler for standby service.

### TABLE VII-2

# STEAM PRICE TO DOWNTOWN CUSTOMERS WITH NEW TECHNOLOGY

CASE	<u>1990</u>	2003
Natural Gas	1950¢/MMBTU	7223c/MMBTU
Base	3282¢/MMBTU \$38.2/M#	10,342¢/MBTU \$120.3/M#
•		
Electrode Boilers	2859¢/MMBTU \$33.6/M#	7256c/MMBTU \$84.4/M#
Coal Fired Package Boilers	5594¢/MMBTU \$65.1/M#	7709¢/MMBTU \$89.7/M#
Fluidized Bed Boilers	5511¢/MBTU \$64.1/M#	10,034¢/MBTU \$116.7/M#

Table VII-3 shows the cost of steam with the addition of the new customer. In 1990 the cost of downtown steam is competitive with natural gas. The large customer reduces 1990 fuel cost from the \$8.52/MMBTU in the Base Case to \$4.97/MMBTU due to the fact that coal can be burned all year. The fixed 06M expenses are also distributed over increased output resulting in a reduction in 06M expense per Mlb. The addition of a large customer is the only case that results in competitive downtown steam.

A number of variations of Case 9 were studied. The first variation simulated a technology changeover to electrode boilers by 1990 to serve the new high load factor steam system. In order to maintain downtown steam price competitive with natural gas, the industrial customer would have to absorb most of the new equipment capital cost. As a result, the cost of steam to the industrial customer would almost double in 1990. Therefore, it was concluded that new steam generating equipment cannot be effectively integrated into the steam system without either jeopardizing the continued service to the large industrial customer or losing the competitive pricing of downtown steam.

A case was also studied to examine the alternative of electrode boilers for standby rather than the rehabilitation of IA boiler. The results were inconclusive. Natural gas fuel savings were almost totally offset by the increased capital cost of the electrode boilers. Because there was not any clear advantage to electrode boilers, case runs with the large customer were assumed to include IA boiler for standby.

### TABLE VII-3

## STEAM PRICES WITH THE ADDITION OF A NEW HIGH LOAD FACTOR CUSTOMER

CASE .	<u>1990</u>	2003
Natural Gas	1950¢/MM8TU	7223c/MMBTU
Base .	3282¢/MMBTU \$38.2/M#	10,342c/MMBTU \$120.3/M#
With New Customer:		
Downtown Steam	1986¢/MMBTU \$23.1/M#	5790¢/MBTU \$67.3/M#
Large New Customer	1039¢/MMBTU \$12.7/M#	3475¢/MMBTU \$42.4/M#

The addition of the large, high load factor customer does make downtown steam competitive in price with natural gas. The addition of any high load factor industrial customer can benefit the existing steam customer. A smaller volume customer, however, would have to be charged a higher price to achieve the same effect and to maintain downtown steam's competitive posture as with the large customer.

Finally, other scenarios were investigated by reviewing the results of previously developed cases. They are summarized as follows:

<u>Unit Rehabilitation</u>. Rehabilitation of steam generating facilities at Grand Avenue Station was not studied in detail due to a lack of definitive engineering data on the feasibility of such a program.

in all cases without the addition of the large customer, however, the cost of rehabilitation would only add to an already uncompetitive situation. In the case with the large customer, downtown steam is just competitive with gas in 1990 so that the cost of rehabilitation would have to be borne by the large customer.

In 1990 the large industrial customer's cost for steam is \$10.39/MMBTU as compared to gas cost at \$19.50/MMBTU and downtown steam at \$19.86/MMBTU. If \$3/Mlb. were added to the industrial price, the cost would still be well below the cost of natural gas. The additional \$3/Mlb. would permit some \$30 million in capital improvements for rehabilitation.

Additional Winter Heating Load. The addition of new, low load factor winter heating load does not improve the competitive position of steam heat as compared to natural gas. Addition of this type of new customer merely adds to the winter peak while doing nothing to relieve the minimum load conditions that contribute so significantly to increased steam costs.

#### VIII - CONCLUSIONS AND RECOMMENDATIONS

### Conclusions

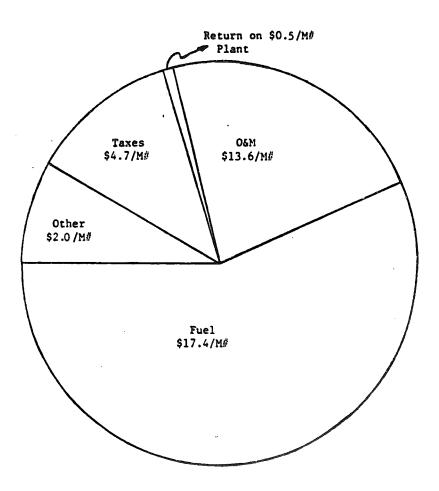
Based upon the investigation documented in this report, a long-range plan for KCPL's downtown steam system can be developed which will contribute to maintaining steam as a competitive and reliable heat source through the year 2000. The development of this plan is based upon the following conclusions:

The Base Case demonstrates that the present steam system cannot be both profitable and competitive with natural gas. A number of factors contribute to the uncompetitive cost of steam. The greatest impact is due to the high proportion of expensive natural gas burned for steam production. The natural gas burn is caused by equipment limitations that prohibit coal burn under minimum load conditions caused by low system load factor. The need to keep a backup boiler on hot standby further increases the natural gas burn.

Another factor that contributes to the high fuel cost is the design of the existing boilers. Greater fuel input to the boilers is required to produce the superheated steam required for turbine operation. The superheated steam is then cooled and the pressure is reduced for steam sendout. A boiler designed or modified to directly produce steam at the 185 psig sendout pressure would reduce fuel costs.

Operations and maintenance expense at Grand Avenue is also relatively high because of the age and design of the facility. Figure VIII-1 illustrates the importance of fuel and OSM to the cost of downtown steam. In 1990, those two components represent \$12 of the cost per Mib.

### 1990 STEAM COSTS WITH ELECTRIC GENERATION RETIRED



TOTAL \$38.2/8#

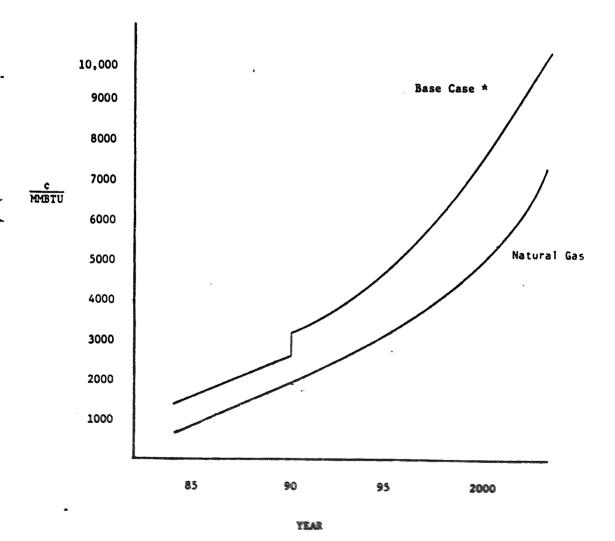
Retirement of the electric generation in 1990 further increases the cost advantage of natural gas over steam. Although total O&M expense is reduced by several million dollars with retirement, the loss of allocation to electric results in a net increase in the cost of steam. Figure VIII-2 graphically illustrates the cost of steam and natural gas over the study period. Steam is not competitive with gas in the 1980's and the situation is aggravated with the retirement of electric generation in 1990.

The results of examination of new steam generating technologies indicates that a new, more efficient supply will not result in a near-term competitive position for downtown steam. Coal-fired options had the effect of greatly reducing fuel and O&M expense, but the capital costs more than offset the savings. Electrode boilers, which are relatively low capital cost, was the best option of new technologies, however even this did not result in a competitive steam price until late in the study period. As a result, steam generator changeover is not a prudent course of action.

A number of scenarios were studied in an attempt to reduce fuel and O&M expense. Specific cases included seasonal service, electrode boilers to serve minimum load and for standby, and plant modifications that permit coal-fired operation under all load conditions. In all cases, some savings were realized, but natural gas is still the less costly source of heat for the downtown customer until late in the study period. Figure VIII-3 shows the cost of steam for the various cases.

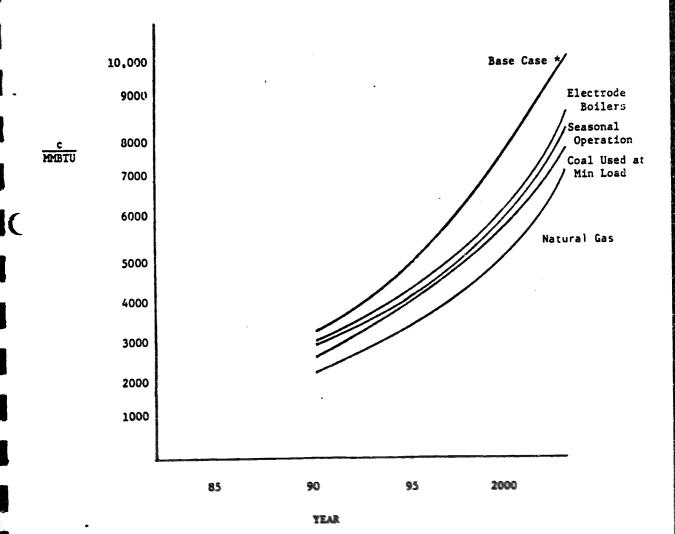
Investigations currently underway could result in significant short-term fuel and OCM savings. These include examining the feasibility of coal mill and boiler modifications to permit coal to be fired under minimum

### DOWNTOWN STEAM PRICE COMPARED TO NATURAL GAS PRICE



\*Base Case \* Downtown customer steam price with electrical generation retired in 1990.

### OPTIONS TO REDUCE COST WITHOUT LARGE BASE LOAD CUSTOMER



\* Base Case - Downtown customer steam price with electric : generation retired in 1990

### OLIGSCHLAEGER

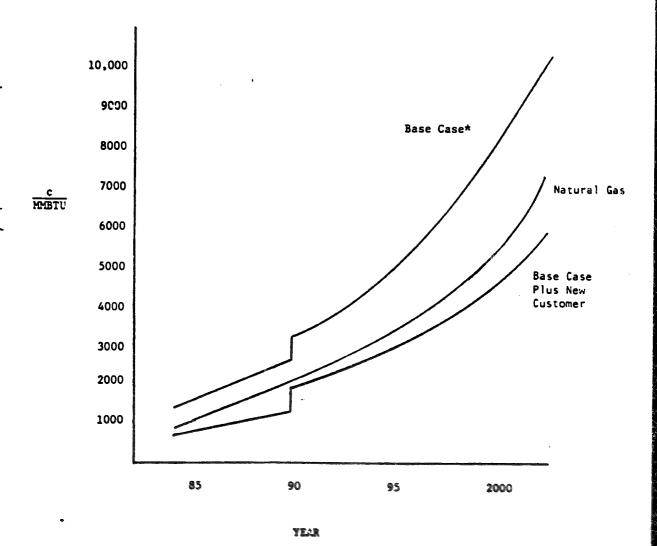
load conditions. Another efficiency modification being investigated is boiler conversion to low pressure operation to reduce fuel cost upon retirement of the electric generation.

OSM expenses are also in the process of being reduced. It was recently announced that manpower at Grand will be reduced by 30 people resulting in significant labor cost savings. This reduction in force was not factored in to this study until 1990 when electric is retired. In addition, the feasibility of transferring major maintenance to the Central Maintenance Department is being studied.

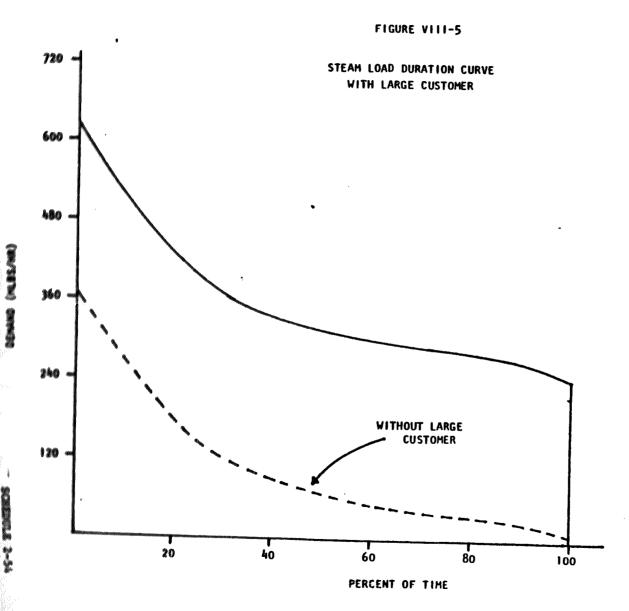
The most promising scenario included the addition of a large, high load factor customer. Figure VIII-4 compares the cost of downtown steam with a large customer to the Base Case cost and to the cost of natural gas. The natural gas cost does not include fixed charges on the customer capital expenditure necessary for a boiler and auxiliary facilities. With a large high load factor customer added to the system, downtown steam is competitive with natural gas.

The turnaround is achieved because the load factor improvement as shown in Figure VIII-5 permits coal fuel to displace natural gas fuel at Grand Avenue throughout the year. In 1990, fuel cost alone was reduced by 40% with the addition of the new customer. Increased sales from 887,000 Mlbs. to 3,055,000 Mlbs. allows 06M expense to be distributed over more units of output further reducing the cost of steam. The price of steam to the downtown customer in 1990 is reduced from \$38/Mlb. to \$23/Mlb. with addition of the large customer. Figure VIII-6 shows the change in fuel mix that occurs with the addition of a large customer.

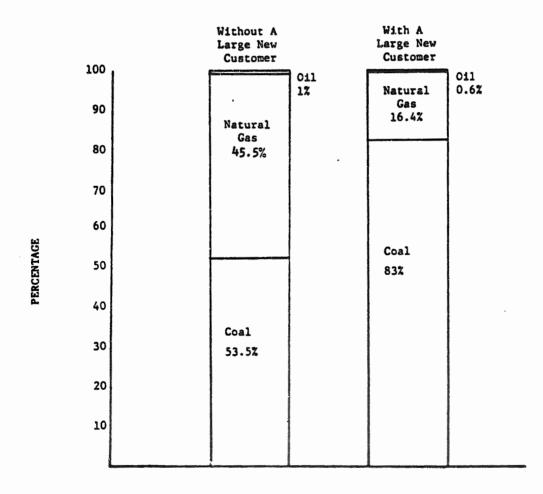
DOWNTOWN STEAM PRICE COMPARED TO NATURAL GAS WITH NEW CUSTOMER



\*Base Case - Downtown customer steam price with electrical generation retired in 1990.



% FUEL MIX IN 1990



Rensas City area plant. Acquisition of this customer can maintain downtown steam in competition with natural gas. Only a high load factor customer can improve the situation. The addition of new winter peaking, low load factor customers does not improve the viability of the steam system.

### Recommendations

Based on the results of this study, the following long-range plan for the downtown steam system is recommended:

- 1. Add a new large, high load factor customer as soon as possible but definitely prior to retirement of electric facilities at Grand Avenue Station. The resultant load factor improvement and increased steam sales is the most effective way to reduce the cost of downtown steam to a position that is competitive with natural gas.
- 2. In the interim period until a large customer can be added, continue to operate Grand Avenue as a joint use facility and improve downtown steam's competitive position through continued implementation of cost saving measures. Specific measures to be investigated include:
  - Reducing natural gas usage for hot standby and under minimum load conditions.
  - Reducing labor expense by shifting major maintenance to Central Maintenance.
  - Reducing coal costs through spot market purchases.

- 3. Continue to operate the existing boiler facilities to avoid large capital expenditures for new steam generators. Complete changeover to a new steam supply system would result in steam costs well in excess of natural gas cost until late in the study period.
- 4. If there is no prospect for the addition of a large high load factor customer, the following course of action should be considered:
  - By year end 1985, "freeze" the steam rate to prevent new customer entry on the system. This does not mean that the price is frozen, only new customer entry.
  - In 1990, when eletric generation is retired, consider providing only winter season steam service to reduce fuel and OSM expense.
  - Continue to aggressively pursue expense cutbacks at Grand Avenue. As the customer base is reduced through attrition, the cost of steam will increase due to decreased sales so that it is essential to cut costs as sales drop.
  - Promote customer conversion to electric heat with incentive rates and possibly leased electrode boilers where applicable.
- Update the study of downtown steam at least every two years.
   Continue to investigate and implement measures designed to reduce fuel and OSH expense.

### APPENDIX A - STUDY PARAMETERS

• O&M Expense Escalation: 10% per year thru 1983 8.5% per year 1984-2003

source: KCPLAN

• 1984 Base Fuel Prices (c/MMBTU):

Coal - 192 Oil - 1074 Gas - 476

source: KCPL Fuel Budget 10/22/81

Gas (Customer Cost) - see Case Runs

• Fuel Price Escalation:

	<u>1984-86</u>	1987-2003
Coal	11.6%	9.6%
011	11.7%	10.9%
Gas	28.5%	10.6%

source: KCPL Fuel Budget 10/22/81

Gas (Customer Cost) - see Case Runs

• Grand Avenue Accounts:

Plant & Distribution Account Increase - 1% per year Plant & Distribution Depreciation Rate - 3.67% per year

Tax Rates:

Franchise Tax - 11.22 Composite Income Tax - 47.52

Load Model Selection - see Table | (attached).

TABLE 1

### MEATING DEGREE DAYS MONTH & YEAR SELECTED FOR HOURLY LOAD DATA

Month	Year Selected	Heating Degree Days	43 Year Ave. *
Jan	1982	1311	1116
Feb	1981	798	866
Mar	1982	591	664
Apr	1982	364	286
May	1981	83	86
Oct	1981	192	199
Nov	1980	557	600
Dec	1980	931	949
		4227	4740
TOTAL:		4827	4768

<sup>\*</sup> Table B-2, KCPLAN, Page B-21

APPENDIX B

Case Runs

CASE & DOUNTOWN STEAM ONLY - RETIRE ELECTRIC IN 1990 - 1845FF NAMSAS CLTY POWER ELIGHI COMPANY STEAM MEAT OPERATING RESULTS 1964-2073

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CASE 1: DOWNTOWN STEAM UNLY - REVINE ELECTRIC 34 1990 - 1845E1	ABNSAS CITY POECA C LIGHT COMPANY STEAT MEAT OPERATING RESULTS	FUUC-39F1

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CASE 2: DOUNTOUN STEAM ONLY - SEASONAL SERVICE HANSAS CITY POURR & LIGHT COMPANY STEAM HEAT OPERATING DESULTS

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CASE 31 ELECTROPE BOILERS FOR STANDRY IN 1984	KANSAS CITY POWER E LIGHT COMPANY	STEAT HEAT OPERATING RESULTS	E002-+9E1

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	3.60C, 1C4	1,762,35	-	2,126,332	2,266,223	2,473,261	2,466,130	2.687.649	3,330	39 347 128 E
Intent lasts	466.021	634,193	781.847	726,978	675,57	623,647	567,376	512,150	26.0 ° 46.2	264,000
TOTAL OFTENTING CRP	13.304.113	14.812.145	16.131.461	16.176.936	19.665.692	21,369,717	23.377.600	25.236.283	27.442.346	27,600,266
	88 88 88 89 89 89 88	61	## ## ## ## ## ## ## ## ##	11	11 11 11 11 11 11 11 11 11 11 11 11 11	61 61 61 54 54 61 61	## ## ## ## ## ## ##	## 61 10 10 11 11 11	60 60 60 61 61 61 61	60 60 60 60 60 60
OPERATING INCOME	474,674	124,373	77.740	90F.C3F	246,943	687,360	627,133	566.279	504,854	**2,605
	8 8 8 8 8									****
ME # 8848 F104	1,505,5%	1,534,344 2,114,44	1,482,54C	1,43C,332	1,377,582	1,324,185	10.270,324	1,215,924	3,340,980	13.467.258
0**** 6** 6***	38,048,00		32,297,365	32,433,066	12,537,197	12.662.558	12,789,194	12,717,086	•	13,176,739
1010, MET PLANT	7,534,600	7,015,163	6.647.158	6.205.305.4	5.746.106	5,267,370	4,824,687	4,356,350	3.663,534	3,406,193
PK lubs da mf 7 Pl. An?	£1.		.13	13	E4.	.13	.33	.33	.33	
	25 25 26 26 26 26 26 26 26 26 26 26 26 26 26	00 04 02 00 00				**	::			20 10 10 11 60
			ž i	ISIC OPERAT	BASIC OPERATING ASSUMPTIONS	SWOI				
								0	0	•
		001.101	70.150	001.650	70, 660	201.600	201.504			
	447, 857									
VI 1944 1944 114	500			615				819		
	~			32•			₽.	2.		
			49-44	15.85.	579.68	644.37				20.35°
	76"676	•		1441.15	E N - E 15 1	17.2.98	1949.29	2155.45	2384.15	
0.00 0.00 0.00 0.00	23.13		2		2		_			*
- -		20.1	11.11		24.6		 		. 4 . 4	

•										
	75-7	1115	1961	1997	***	1999	03u2	2002	2002	
STUNDE SERENCES	32,344,34	35,740,795	34,972,17	42,336,453	46,132,664	50,333,005	54,463,695	\$0,166,790	15, 409, 349	72,037,424
	35,236,000	34.677.033	16,570,000	20,440,030	22,630,000	24,965,000	827, 564, 068	30,443,558	33.537,000	37,015,000
	523.585		L16.734	151-644	724.035	787.747	102.459	127.356	1.004.181	
1111111	3,841,719			3.611.590	1,744,564	1,697,192	2,056,453	2,233,422	•	, i
86.73	117,447			F60,634	162,793	176.630		207, 133	•	
655 67 507 7 1 5 1	184,751	1,000,11	10.114.53A	055.64		703.451	710.465	279.546	7225	
	3, 660, 914				5.366,463	5,63.,760			•	
*	343,769				111,331	51,756	0	0	6	
TOTAL OPERATING CAN	32,465,132	•	É		46.76.585	20	54, 745, A75	10,146,770		72,037,424
340341 941114346	340,000	316,626	252,874	350 350 350	323,04	57,228				21 E3 41 14 61 61 61 61 61
	8 8 8 8 8	1							•	****
10 1 11 11 1 1 10 10 10 10 10 10 10 10 1	1.947.437	172.630	135.656	POP. 5.40	43°,589	760.676	710,465	717.590	724.76	732,034
\$4# N( ) \$4\$H 71.00	14.534.5%	15,529,527	36,465,182	•	_	38,423,355	17,633,840	20,351,429	21,076,195	23,608,209
01110 111 14 55040	13,300,464		-	13,711,745	17,848,463	136,987,351	34,327,224	34,268,496	34,411,383	24.555.23
		4,976,111	5,027,842	5.478.171	15.,451.2	5,183,242	5,232,045 0	8,64,35,8	5,337,480	
							•	• ;	<u>.</u> ۱	' ;
MI TOTAL ON ME! PLANT	90 99 	F ::	E							M H 11
			<b>6</b> i	ASIC OPERATING	BASIC OPERATING ASSUMPTIONS	1045				
1 100					6		001			<b>3</b>
	177.438									
	467,000	647, 870	- 20° - 20° -	067,500	987,109	667,000	A&7,000		687.	
170 A CON 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10% . 37	1166.34				1732			2332. LE	
					4364					
	;			54.62	2	2	20.00		24.5 00.	50.101
***************************************		•	•	•	4.5	4.10				

CASE 4: ELECTRODE BOTLERS FOR NIMIMUM LOAD - DEM TO MANTHORM	MARSAS CITY POETS C LIGHT COMPANY	STEAM HEAT OPERATING PESULTS	できたが、ままずべ
ELECTROBE 0	A S A A A	316	
ASC 41			
J			

	38.1	2465	1964	1967	1984	1961	1.90	1441		S
	12,552,400	13,441,621	34,523,440	15.566,356	15.547.823	110.406.74	14,097,390		22,021,647	23,432,272
30 324	4.17.000	5,523,333 2,695,375	6,242,047	٠٠٠ وي	7,475,000	8.25.000	9.039.000	9.696.000	10,774,600	
	831, 706 556, 040							410,154	145,034	
6007 ACC13	156.45					79.121	64.761	13.26		12. TO 1
	111.000						6700675	727,938	764.743	
	3.405.170 661.021	_	1,624	4		1,993,71	ž	2,278,53	2. 445. 453 4. 445. 453	2,44,78
		•		ij	٠	:		191111111	Pro 1467	9/1. COO.
TOTAL SPECIMENTS CEN	11.572,72	37,517,446	13,656,947	34,760,320	15,807,928	17,113,70	18,420,259	*	21,517,026	23, 34, 543
740341 541 140748		122,373	•	a66,036	246,413	187,360	L27,130	566,299	£50° 805	
	88188888			***************************************						
	3.505.5%	1,534,349	3,462,58	1,430,313	1,377,513		1,270,323	1.215.923	3.150.750	1.205.487
	1. 50 5, 57		4,63?	6,332,847		8.734.544	10,504,667	11,226,791	12.301.	13.467.258
		12,166.460	32,290,365	12.413.066		32,662,568	12.789.194	12.917.081	13.006.254	23.274.719
	7.534.000	7.675.163	4,551,666 6,647,958	6.200.260	5.746.106	5.257.373	4.824.687	4.783.867	4,631,704 FAA.53	F. 680,023
	<b>(</b> ***	£1.	21							
	9 50 92 93 93	0 84 0 85 0 83 0 9	11	* :: * :: * ::	1 11 1 11 1 11 1 11	- :: - :: - ::	- ::	3 !!	9 11 9 11 11 11	3 H 4 H 11 11
			21	DASIC OPERATIN	DASIC OPERATING ASSUMPTIONS	SHO				
							0	6	6	
							209,600	204.600	201.100	
	607.600	667.000	887.	000,000	667.100	687.000	177,400	177.400 867.600	177, 400	177,485
							848	216	818	818
8						•	2.	02.	R:	ě.
							2216.03	20 Tane	21.55	
			1233.93			17-2-98	1949.75	2155-45	2384.65	24.37.40
			# C		P. P. P.			5F. 45	31.03	43°64
\$41.80 BATE 184.05 ASS		~	2.3	7.20	L.33	7.57	7.28	7.47	, c	

	7667	2118	1996	5442	1	1441	200	1001		
serves servences	88.708,148	27,77,LA3	29.146.11	32,548,647	35.267.15	38,284,242	41,436,651	25. Jen. Pub.	4.000	53, 408, 653
**************************************	33,062,000		15,566,909	17,447,600	18,723,FD <sup>n</sup>	20,510,000	22,33%,000 9,324,583	24,627,000	26.747.000	
	523, 688		1,166,734	644,156	724,735	747,747	A54,70L	477, 256 27, 264		1,011,757
	117.887			•		174.630	274.454	£66°202	475.408	
#4% #4%	136,527	1.098.793	1,014,538 547,584		1,204,518	454°E64	1,516,676 710,485	3,645,638	207.20C.2 724.245	
\$ 10 VANC	2,676,702			•••	5,457,169	4,267,635	80.041.8	5.078.433	5, 53b, 944	Ĵ
			4631	45.00.4	456 444	BC / 4 C			3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
TOTAL OFTENTING CLP	25. 38.2 . 54.0	<b>S</b>	27,674,076	32,340,32	35,364,969	443	41,436,653	45,343,138	100 CE 7 100	53, 702, 62
ladiat ballenies		376,626	252,413		123,107	57,227				
		8 8 8 8 8		;					•	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
4(1 CASH FLOW		5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	735,656 14,44,5,142	877,40° 90°,546,54	914,585	767,676 18.923.355	19.653.840	80-517,545 854,625	21.076.15	195,001
\$1400 Pt. 487 64740	13,308,481	13,441,870	3,675,986	5,171,745	5,124,453	13,197,353	34,127,224 5,232,045	5.264,345	14, 422, 183 5,337, 204	14.555.23 5.370.562
both of Front	8,984,877	2,477,141	1,945,336	1,448,612	146,421	440,213	0	<b>E</b>		
# 1/**	(Fig. 61) 	0 00 0 00 0 00	M !!		£1.	. 13	.13	.13		हुगी, 64 सम्बंध 80 स्ट 64 88 88
		1								
		٠	21	PASIC OPERATING ASSUMPTIONS	THE ASSURPT	IONS				
	•				E					
			104.607		704,607	701,500	704,600	704,500	704.100	
	467,503	687		6.7						
M. OPTOM CAPACITY	S. C.		5.00 5.00						250	64 65 67 K
7384 04600 826 11013		1054	1150.37		1386	15-12-51	1658	1826.93		
		PRI)	36.98.37	_		*L34.03	-	S448.37	5116.85	
		3266.33	3568. Lu	44-44 44 44	65° 736 7	4627.39	5339.17	05.80F2		
							,			
311 94 98 1 34C P( 85C	7.94	8.03	7.61		•	4.4	6-53	g. 43	<b>6</b> -	-

<u> </u>	CASE SI DOMNIONA SIERM ONLY - RETIRE ELECTRIC IN 1984 - ALL COSE	RANSAS CITY POREM E LIGHT COMPANY	SICAR MEAT OPERATING BESULTS	£_0c-94C1	11111
	#5f 51 E				

Slealing of which		1985 194,784,608	36.36.38.38.38.38.38.38.38.38.38.38.38.38.38.	1987 17,145,663	1988	1961	E02.88.48	23.04 23.04 23.04 23.04 23.04 23.04 23.04 23.04 23.04 24.04 25.04 26.04	25,756,25	
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5.106.00 000.00 000.00 000.00 000.00 000.00 000.00	4,887,300 8,840,300 1,005,403 1,005,403 1,005,403 1,005,403 1,005,403	4,674,000 4,011,000 4,017,770 55,434 616,434	5,458,000 6,575,4 100,675,4 6,75,75 6,75,43,4 0,45,85,	6.034.000 7.076.00 321.05 77.365 52.003	<b>2</b> 10		0031466 003146	40	
ARD SERVICE CRESSES TO THE COLUMN TO THE COLUMN THE COL	1,520,600 1,520,600 1,520,607 1,520,607 1,520,607 1,520,607 1,520,607		~ i 💥 ii			2,223,035 3,223,035 3,223,035 3,233,035 3,133,035 1,135,035 1,135,035	ณ์ เล้า	ลั เล็แ		
# # # # # # # # # # # # # # # # # # #	1,185,184 1,185,184 1,185,186 1,185,186 1,185,186 1,185,186 1,185,186 1,185,186 1,185,186 1,185,186 1,185 1,	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	1,289,544 3,188,333 5,189,45 4,581,685 4,581,581	1,145,451 5,110,764 13,311,473 4,547,503 4,125,7603	5.25G.44G. 6.25G.44G. 13.4435.6439.6439.6439.855.6439.855.6439.855.6439.655.655.655.655.655.655.655.655.655.65	1, 193	1,000,430 13,746,430 4,736,503	13-14-15-15-15-15-15-15-15-15-15-15-15-15-15-	10.040 14.040 16	
of twen on mit Plant	(PT 52 	m 11 ph 10 0 10 00 00 00	(* 1) (* 1)	52	.13 .13 .13 .10 .15 .15 .15 .15 .15 .15 .15 .15 .15 .15	E4.	(7) 11 (4) 11 (1) 11 (1) (1)	# :: :::	FR 11 P3 11 0 11 11 11	(PT) 80 (PT) 80 (PT) 80 80 80
		789.420 67.20 67.20 67.20 67.20 71.10 71.00 71.00 71.00 71.00	201-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	700-078 417-040 417-040 417-040 417-040 417-040 418-040 418-040 418-040 418-040 418-040	703 177 177 1867 1867 1867 1868 187 187 187 187 187 187 187 18	209-600 137-400 187-700 50-700 50-00-34 1849-34 1849-34 1849-7-9	004.F05 004.754 000.754 000.75 000.82 01.82 74.32 74.32 74.52 74.52 74.52 74.52 74.52 74.52 74.52 74.52 74.52	201-100 277-400 877-400 910 617-00 318-18 318-18	PANA AMA PANA A

CASE 5: DOLMIOUM STEAP ONLY - RETIPE CLECTRIC IN 1984 - ALL COAL NAMES CITY POWER L LIGHT COMPANY STEAP MEAT OPERATING PESULTS 17A4-2CM3
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\$ 100 14 10 588 F08 14	121° E 88° L&	31.875.16	34,723,547	37.663.271	349° - 144	PFF4 PE3,650.2#	E40.31.000	2003 065,774,62	5005 2005 2005		
######################################	3.5 545 CCC 3.5 545 CCC 523 566 3.7 547 47 3.7 547 3.2 545 3.2	11,454,000 12,52,000 5,64,16 3,346,416 12,457 1,000 1,		34.52C.COG 34.74C.COG 34.74C.COG 34.75C.CG 34.	15.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0	\$7,564,000 \$7,354,000 \$7,37,747 \$,617,518 \$1,518 \$1,25,6	24.460.000 24.635.000 254.706 2.056.453 2.056.453 2.056.453 2.056.853		22.173.000 3.000.161 2.000.161 2.423.263 2.723.263 3.745.403 4.55.403 6.54.403 6.54.403	2000 000 000 000 000 000 000 000 000 00	
elek gegmaning gur			34,721,547	37,463,671	317.646.19	45,079,534		54.62.62 56.66.62 66.66.63 66.			
4	743,333	733,564	72F, 85F 13, 340, 876	728,058 14,168,935	735,339	542,547 542,345,81	750,119	357,620	745,347	772.6% \$6.5%;750	
**************************************	84°38°84 4°38°8 658°8 658°8	161,44,44 4,978,131 152,705	54,623,792 5,927,693	64,85,44 5,186,128	\$,127,528 5,128,953	15,055,604 5,150,242 0	15,707,369 5,73,564,8 0	35,359,248 5,284,345	15,512,833 £,337,207	35.567.963 5.370.561	
医乳蛋白 医乳 医乳 医二甲苯甲二甲苯甲二甲苯甲二甲甲二甲甲甲二甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲甲	679 84 678 88 9 90 90 90 93	0 00 0 00 0 00 0 00 10	# II		7: ii		# II	(%) 11 (%) 11 (1) (1)	(M) 11 (A) 11 0 11 11 01	177 01 170 01 0 00 00 00	
			2 ;	ASIC OPERAT	MASIC OPERATING ASSUMPTIONS	10%					
1	ODDODE SARR	201-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	133.FC7 133.FC7 133.FC7 133.FC7 135.FC7 145.FC	0010-00-00-00-00-00-00-00-00-00-00-00-00	25 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	701-600 67-600 687-600 700 700 700 700 700 700 700 700 700	703-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600 177-600	001-F07 501-F07 501-F08 501-F0	0 177-400 687-600 687-600 7-601 7-7-601 7-7-601 7-7-601 7-7-601 7-7-601 7-7-601 7-7-601	001, F05 001, F05 001, F05 001, F05 001, F05 101, F05 101	
								*:-			

CASE &: ELECTROPE BOILERS - TOTAL REPLACEMENT IN 1988 RANSAL CITY POWER E LIGHT COMPANY STEAM HEAT OPERATING RESULTS 1984-2073

	***	1165	1961	1987	1.00	1161	1490	1991		Ē
sjaming minite	14,293,350	15,736	17,496,267	14,070,713	20,517,662	22,131,567	23,542,503	25,383,488	24,717,066	20,101,15
	4,151,000	5.570,073	5,724,607	7.610.CE0 5.5F3.CE0	11,764,960	12,683,500	13,764,000	303,451,486	34,204,000	77,587,000 2,584,000
	231,708	251,493		245,458	321,115	345,439	378,624	410,154		102.6%
	21.42			64,340	72.003	79.121	94.76	37.46		542.404
1	411,220		20.303	525,247	56. 493	615,334	5-10-1	727,418	784, 743 Leg - 243	
	1.000.61	Ä	•	2.178.080		2.475.736	P. 642.304	2.826.326	3.614.714	3,27,557
INCOME TABLES	150,031			726,478		1,257,130		1,157,774	1,166,335	1,054,381
THE SPECIAL CEP	33,313,729	14.616.323	16,633,733	36,174,678	14,364,637	20,734,354	22,255,532		∾	27.642.240
THE SAME SECOND	40 40 40 40 40 40 40 40 40 40 40 40 40 4	110000		2000 1000 E	1.257.557	ACC. CPC. 1	1.334.472		**********	1. 25.635.
				5						
		: -						1 4 6 7 6 24	1.828.1.32	
10 1 10 1 10 1 10 1 10 1 10 1 10 1 10	7.505,54	3,111,445	1,62,53	6, 432, 847	6.063.46	10,045,724	11,777,611	13,654,154	15,187,827	17:44:12
18831 PLANT 6044D	22,644,000	32,368,480	32.290.365		11,261,197	11,373,506	11,467,546	11,602,421	33.738.445	11,035,630
	*. ***. ****	4.83E.120 7.045.183	4,553,666	4,547,203 6,c00,28C	11,134,106	10.701.457	4,736,503 30,280,565	4,783,667	1,631,704,1	6.267.97
	.13	4	E. 4.	.13	.13	. 33	.13	619	.23	
	20 20 20 20 20 20 20	64 60	**	***	***	**	**	::	#	88 68 68 88
			2;	SIC OPERAT	RASIC OPERATING ASSUMPTIONS	10 M S				
3	0 6			000		00		964	901-100	6
	177.400									
	867, C33	687.070	000,700	667.	667,000					060.734
				02.						
V.C. F. 10 V.C.		366.27		25	100	1155.	1252.43	1750.67		
	14.45.44 Je 646	_		6 3 DC • 30	1543.43					
ON ONE WE THE DE	2	2	34.15						E.	
	3			20.4		90.	93.	36.4		20.7
					•				•	

CASE &: ELECTPOEE BOTLERS - TOTAL REPLACEMENT BW 34PB RANSAS CLIV PONER E LIGHT COMPANY STEAM HEAT OPERATING PESULIS 31EAM HEAT OPERATING PESULIS

•				•	• • • • • • • • • • • • • • • • • • •					
Singale exiterial	35,662,735	33,332,588	35,501,514	36.215.420	10-14 11,337,64*	3999	2000	2001	\$805	100.00.72
	34,971,600	20.647.099	22,404,90°	24,345,000	35,436,45	26.563.000	31, 121,000	33,744,000	W. 44. 4	34,751,000
# TAB	523,688	566.436	1.485.327	1.411.580	724.735			450,000 450,000		
	117, 46,7	127,452	136,285	•	7,0	1.376.630		207,433	225,458	244,785
KFF(C1) 10x	611,811			•		451,205				
•	1,701,108		615,367			731.565	175,813	119,405	367,786	305,375
TOTAL OPERATING CUP	24,754,774	•	34,511,464	•	46,247,773	43,451,550		50,732,151	54,548,253	\$7,321,700
240341 541146240	1,107,614		996,039		46 676	859.676	147,307	165,102	12.23	554.84
101 COSH FLOR	1,727,415	1,675,011	\$,622,083 22,493,636	1,568,625	1,514,639	1,463,101	1,405,023	3,349,376	3,273,23	1,2%, %5 32,327,083
\$6055 PLANT GENED \$6055 0157 \$0161 NC PLANT	11,153,966 4,420,623 6,521,673	12,073,525 4,176,111 6,070,130	12,194,261 5,927,992 7,615,621	\$2,3\$4,203 \$4,078,17 \$1,55,795	35,434,545 5,326,453 6,613,350	12,563,759 5,183,242 6,222,285	32,689,396 5,232,045 5,748,520	12,816,289 5,244,315 5,276,018	12, 444, 452 5,337, 284 4,786,738	13.073.61 (1.310.61)
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######################################	14.5 10.5 10.5					4627.37 62.37 0.00			1530.78 78.17 000 7.88	

•			CASE 78 HANSA STE	Pachage mol	E 7: PACABGE ROLLEMS IN 1988 E 1996 Ransas City Power E Light Company Steam meat operating pesults 1984-2073	B C 3440 OMPANY LTS				
Simple salleales	34,177,48	38,434,795	14P1 12,342,551	18,032,536	346£ 28,434,473	1464 	940,846,44	1991	3772 570,071,74	17,6%5,142
		5,567,000 4,667,003 605,403 605,403 56,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73 76,73	5,055 20,	2.65.958 2.65.958 2.65.958 312.978 2.65.958 2.65.958 2.65.958 2.65.958	6430,445,000 6431,425,000 878,425,55 878,655 878,656,55 878,654,65 848,654,65 848,654,65	6 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	04400,000 0456,000 0456,000 047,000	4,554,400 4,654,400 4,654,400 4,654,400 4,654,400 4,654,400 5,653,400	5,347,000 6,645,014 645,014 1,075,74 1,075,74 1,03,54 5,243,03,11	2.44.000 2.44.0
1019 08581185 Car		367.25.436	_	~		### 0 44 55	39,157,433	34,013,653	10 10 10 10 10 10 10 10 10 10 10 10 10 1	35.467.864
Car Mil Cata Flow		1473,253 8,417,838	3,423,526	1,369,240 5,788,575	1,756,407	6,522,622 23,017,718	17,032,788	36.243.543	11,346,433 73,042,074	34.001.045 64.013.140
60000 P. SPT GEORG 60000 P. S. S. FORE, M. P. SPT	**************************************	58.354.440 4.506.620 6.625.356	12,741,185 4,551,686 6,174,134	12,414,096 4,597,203 5,730,199	56,444,45 56,643,4 56,675,038	55,344,224104,672,633 4,64,637 4,736,503 4,64,64100	.04,672,6703 4,736,503 .00,076,00	05,423,3457 4,763,667 47,353,433	105-421.945204.980.6822088.886.4584.74.4.2869.888.4.74.4.51.4.888.4.74.4.51.51.4.51.4.51.51.51.51.51.51.51.51.51.51.51.51.51.	542.045.4 4.660.074 545.045.4
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CASE 7: PACKAGE BOILFRS IN 1429 C 1440 RANSAS CITY POWER C LIGHT COMPANY SIEAM MEAT OPERATING RESULTS 144-2013

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Sinalala Sattemies	1994	244,553,040	30,626,537	144.701.18	39.263.624	94.437.424	\$000	2005	2002	2003
	7.877.000	7.873.000 4.846.000	1,273,000	6,561,600 10,052,030	10.115.00	10,365,000	83	13,413,000	13,562,000	20777
	523, 666 5, 543, 544		~	1,111,500	1,744,564	1,617,147	2,056,453	457,356 8.833,428	421	
	127, 127	1.000.1	~	150.034	1,266,51	1,345.042	3 2	1,645,618	7, 265, 204	
	6, 105, 43° 8, 447, 430	5,549,942	3 00	5,613,663	955.46	4, 341, 520 6, 153, 036	L. 346.343	6.506.371		7.25.484
	04,746,04	70,011,107	- • •	-		540.354.6	45,444,4	24.40/1/	91:	24 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1978, GFC #1785 CFF GPC #1786 18COK	37.374.905 23.22.22.23 33.465.337	2019 FEB. 18	945'649'61	15,265,734	1.557.636	1000145161 111111111111111111111111111111111	450.020.0	064.604.8	11111111111111111111111111111111111111	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
46.1 CASH FLOW	15.453.321	15.27.281	\$\$#\$#\$	14,578,546	14,213,776	13.645.344 77,64,73	13,473,242 11,673,2002	13,047,431 04,346,6362	32,737,659 34,708,4%	12, 334, 482 21, 242, 175
\$5055 PLANT \$220 \$5055 PLAT \$0155 PLAT	124, 130, 1251 1, 146, 623 66, 141, 16	150.882,883 4,174,515 65,141,572	18.822.22311.324.444112.437.657113.562.663114.647.681115.844.656117.8033.101118.173.139119.384.868 4.478.11 5.727.842 5.278111 5.128.453 5.180.242 5.732.045 5.284.365 5.337.807 5.3370.583 85.144.572 82.873.722 78.967.113 75.629.437 72.660.387 69.459.644 66.226.846 67.461.808.8	132,437,6573 5,u78,171 78,967,133	17,562,0691 5,124,153 75,624,437	14,697,6811 5,183,242 72,663,387	15,884,6563 5,232,945 67,457,644	17,003,1011 5,244,315 66,226,846	18,173,1301 5,337,207 62,461,638	14.254.668 5.370.561 5.464.01
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			21	PASIC OPERATING ASSUPPTIONS	MG ASSUPPTION	\$ 1				
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	517.8 56.71.8				45.4344		676.72 Lebb.13	81.7515		
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			CASE PE FLU Kansa Ste	PLUIDIZED PED NSAS CITY POWE STEAM HEAT OPE LIGHT	FLUIDIZED PEO BOTLEPS IN 1948 G ANSAS CITY POWER E LIGHT COPPANY SIEAM HEAT OPPANING PESULIS 194-2[7]	1966 6 2990 Oppany LTS				
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total seconting tra- seconting secont	1	2222222 861,270	35.54C.354	16,087,611 111,087,611 111,087,087	22,530,634 ::::::::::	23,703,743 :::::::: 4,553,134	34,750,004	38.0%5.833 :::::::::::::::::::::::::::::::::::		
MI COSH FLOR		1,473,253	3,421,527	1,369.240 5,768,575	4,364,601 12,153,177	6,224,628	\$2,628,747 30,314,552	\$1,777,335	33,707,314	35,285,357 bx,786,528
\$8055 P. MT 6000 \$8055 9157 1074, MT P. AN	12.844.308 4.442.003 7.014.203	12,154,490 4,506,620 6,625,156	12,241,185 4,551,686 6,174,104	12,414,096 4,5°7,203 5,730,179	46,451,237 4,644,175 36,727,497	46,855,747 4,681,607 35,023,176	74,004,365 4,736,503 70,245,414	74,784,347 4,783,867 66,143,533	75,418,781 *,631,706 65,020,324	76.246.796 4.869.823 63.875,473
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CASE 8: FLUTO12ED BED BOTLE¶S 14 19AB 6 1996	RANSAS CITY POLER C LTGHT COMPANY	STEAM MEAT OPERATING RESULTS	
CASE BE	=		

PPERSTING PEVENUES	PP4 PP5,275,58	24,44,255	36,714,737	57.2	3776	1994	2000 075,84270	13,110,401	\$005 \$1,107,47	2003
746. 746.		20.241.000 20.241.000 1.310.412 1.000.743 1.000.743 1.000.743 1.000.743 1.000.743 1.000.743 1.000.743 1.000.743 1.000.743	4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.		25,657,000 27,657,000 37,748,748 37,748,748 37,749,748 57,749,678 57,749,678 57,749,678	26,035,000 26,035,000 1,747,172 1,747,132 1,345,032 1,345,032 1,345,032 1,345,032 1,571,457	11,522,000 30,451,000 2,547,000 2,547,645 3,547,676 3,547,628 5,572,628 63,245,628	32.444.000 32.444.000 2.724.335 20.434.22 3.645.610 3.645.610 3.645.610 5.846.610 5.84	35.617.000 35.617.000 35.617.000 37.625.00 37.65.704 37.75.204 5,124.007 5,124.007 5,124.007 5,124.007	24.5.5.4 25.5.5.5.5 25.5.5.5.5 25.5.5.5.5 25.5.5.5.5 25.5.5.5 25.5.5.5 25.5.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5.5 25.5
MET CASH FLOW Cun MET CASH FLOW RROWS PLANT GRAND	11,054,343	30,775,005 64,342,473		50,456,675	747,451,741	57,457,r 57,25,653, 60,757,00	136,746,77	4,54,625 4,54,526,545 4,556,545	2,000,000 154,000,000 50,000,000	4,14,507 13,524,532 64,223,785
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			•	16,360	77,71	75,121	24.763	71.966	19.783	
				467,631	A7A , L34	953,318	1.034.350	1.122.270	1.27.046.1	
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				3/6./66	BE4. FE	306,627	479,748	411.082	347.663	272,586
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	3.611, EEO	3,365,474	3,117,532	5,067,C10			3,690,737	3,640,737 3,162,175	2.4.28.33.54.54.54.54.54.54.54.54.54.54.54.54.54.	7 24 . C. C. C.
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			373.7ª	377.56	15.004	450.4	476.99	548.03	76.	444
			710.00	64.467 44.467	7235.63 64.3.63	24.52.40	3281.62	35.2.46	3616.72	1372.32
			12.1.43	4 S L + 4 S L	1543.43	1762.36	1765.26	2355.45	230° 86 2384.65	2.3 <b>2.</b> 55
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		18.74	54°50	17.7A	. S. C	<b>1.</b> 3.	35.56	<b>3</b>	5	#4 4 ≪
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RASIC OPERATING ASSUMPTIONS

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<b>***</b>	1,433,463				9	2.155.437	7.338.643	2.527.438	2000 CUV	
	756, 63				764.	744,556	AD2, 534	610,559	P. S.	4
	161.692	_			3,3	3,751,445	4,105,560	4,475,250	4. P.S. B.34	5,353
SERIA LANGE	7					<b>ن</b> د	n <b>a</b>	9 6	r c	
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6000 FLA4 6000 6075 735 7075 87 8404	55.673.778 6.526.923 5.544.954	15,8?7,3Ft 4,978,111	15,766,769 5,727,897 7,721	16.546.35h 5.378.373	14,707,587 c,128,453	16,470,663 5,18.J,242 0	3,732,745 0	36.465.2 5.664.365	36,947,748 5,337,289	17,134,437 5,370,581 0
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