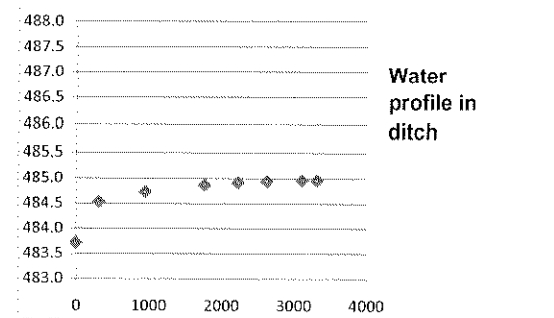


**Ameren Labadie Energy Center Utility Waste Landfill**  
**Perimeter Ditch Water Profile: 25-yr, 1-hr event**  
**Elevation for Stated Flow**  
**Counter Clockwise from Pond 3**  
**Table N-7**

|           |       |                          | $S_{s, \text{left}} = 3$ |               | $S_{s, \text{right}} = 3$ |       | Base Width<br>(ft) = 9 |          | Mannings N = 0.02         |                          | So (ft) = 0 |          | Runoff Factor for 2.63 in/ hr rainfall= 0.017 |                |               |            |                       |       |
|-----------|-------|--------------------------|--------------------------|---------------|---------------------------|-------|------------------------|----------|---------------------------|--------------------------|-------------|----------|-----------------------------------------------|----------------|---------------|------------|-----------------------|-------|
| Elevation | Depth | Channel Bottom Elevation | Slope of Water Surface   | Adjusted Base | Adjusted Height           | Area  | Velocity               | $v^2/2g$ | Specific Energy           | Hydraulic Radius         | Slope       | S-So     | Distance                                      | Total Distance | True Distance | Location   | Distance from Culvert | Q     |
|           |       |                          |                          |               |                           |       | Average Velocity       |          | Change in Specific Energy | Average Hydraulic Radius |             |          |                                               |                |               |            |                       |       |
| (ft)      | (ft)  | (ft)                     | (ft/ft)                  | (ft)          | (ft)                      | (sf)  | (fps)                  | (ft)     | (ft)                      | (ft)                     | (ft/ft)     | (ft/ft)  | (ft)                                          | (ft)           | (ft)          |            | (ft)                  | (cfs) |
| 483.72    | 0.72  | 483                      |                          |               |                           | 8.04  | 4.058                  | 0.2557   | 0.976                     | 0.593                    |             |          |                                               | 0              | 0             | Pond 3     | 0                     | 32.61 |
|           | 0.81  |                          | 0.0024                   |               |                           |       | 2.813                  |          | 0.592                     | 0.853                    | 1.77E-03    | 1.77E-03 | 334                                           | 334            | 320           |            |                       |       |
| 484.53    | 1.53  | 483                      |                          | 9.00          | 1.5300                    | 20.79 | 1.568                  | 0.0382   | 1.568                     | 1.113                    |             |          |                                               |                |               | Letdown 13 | 320                   | 32.61 |
|           | 0.20  |                          | 0.0003                   |               |                           |       | 1.415                  |          | 0.187                     | 1.172                    | 2.94E-04    | 2.94E-04 | 635                                           | 969            | 960           |            |                       |       |
| 484.73    | 1.73  | 483                      |                          | 9.00          | 1.7300                    | 24.55 | 1.262                  | 0.0247   | 1.755                     | 1.231                    |             |          |                                               |                |               | Letdown 12 | 960                   | 30.97 |
|           | 0.14  |                          | 0.0002                   |               |                           |       | 1.106                  |          | 0.129                     | 1.271                    | 1.61E-04    | 1.61E-04 | 803                                           | 1772           | 1780          |            |                       |       |
| 484.87    | 1.87  | 483                      |                          | 9.00          | 1.8700                    | 27.32 | 0.950                  | 0.0140   | 1.884                     | 1.312                    |             |          |                                               |                |               | Letdown 29 | 1780                  | 25.96 |
|           | 0.05  |                          | 0.0001                   |               |                           |       | 0.860                  |          | 0.045                     | 1.326                    | 9.21E-05    | 9.21E-05 | 491                                           | 2262           | 2240          |            |                       |       |
| 484.92    | 1.92  | 483                      |                          | 9.00          | 1.9200                    | 28.34 | 0.770                  | 0.0092   | 1.929                     | 1.340                    |             |          |                                               |                |               | Letdown 28 | 2240                  | 21.82 |
|           | 0.03  |                          | 7E-05                    |               |                           |       | 0.670                  |          | 0.021                     | 1.347                    | 5.47E-05    | 5.47E-05 | 381                                           | 2643           | 2640          |            |                       |       |
| 484.95    | 1.95  | 483                      |                          | 9.00          | 1.9450                    | 28.85 | 0.570                  | 0.0051   | 1.950                     | 1.355                    |             |          |                                               |                |               | Letdown 27 | 2640                  | 16.46 |
|           | 0.02  |                          | 3E-05                    |               |                           |       | 0.480                  |          | 0.013                     | 1.359                    | 2.77E-05    | 2.77E-05 | 480                                           | 3123           | 3120          |            |                       |       |
| 484.96    | 1.96  | 483                      |                          | 9.00          | 1.9610                    | 29.19 | 0.389                  | 0.0023   | 1.963                     | 1.364                    |             |          |                                               |                |               | Letdown 26 | 3120                  | 11.35 |
|           | 0.00  |                          | 2E-05                    |               |                           |       | 0.250                  |          | 0.002                     | 1.365                    | 7.50E-06    | 7.50E-06 | 246                                           | 3369           | 3330          |            |                       |       |
| 484.97    | 1.97  | 483                      |                          | 9.00          | 1.9650                    | 29.27 | 0.112                  | 0.0002   | 1.965                     | 1.366                    |             |          |                                               |                |               | Letdown 25 | 3330                  | 3.27  |

**Notes:**

1. Rainfall event used is 25-yr, 1-hr storm which produces 2.63 inches of rain.
2. Longitudinal slope of channel assumed to be as stated for So.
3. Flows are split generally at half the distance between the entrances to the pond along the perimeter ditch.
4. Flows coming to a letdown structure and from below the bench served by the letdown structure are combined as the flow at the letdown structure for modeling purposes.
5. Model is adapted from Illustrative problem on page 380 in "Elementary Fluid Mechanics" by John Vennard, Wiley and Sons, 1961.



**Ameren Labadie Energy Center Utility Waste Landfill  
Stormwater Management Pond 1  
Pond Volume Calculations  
Table N-8**

| Base Width of Pond in feet  |        | 373                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
|-----------------------------|--------|------------------------|----------------------------|-------------------------------------|------------------------------------|----------------------------------------|-----------------------------------|--------------------------------------|---------------------|
| Base Length of Pond in feet |        | 573                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Rise of Slope in feet       |        | 1                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Run of Slope in feet        |        | 3                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| WIDTH<br>(FT)               | LENGTH | WATER<br>LEVEL<br>(FT) | AVERAGE<br>AREA<br>(SQ FT) | VOLUME PER<br>INCREMENT<br>(VOL/FT) | TOTAL VOLUME<br>OF POND<br>(CU FT) | TOTAL VOLUME<br>OF POND<br>(ACRE FEET) | CAPACITY<br>IN USE<br>(ACRE FEET) | REMAINING<br>CAPACITY<br>(ACRE FEET) | Elevation<br>(FEET) |
| 373                         | 573    |                        |                            |                                     |                                    |                                        |                                   |                                      | 468                 |
| 379                         | 579    | 1                      | 108,293                    | 108,293                             | 108,293                            | 2.5                                    | ----                              | ----                                 | 469                 |
| 385                         | 585    | 2                      | 111,167                    | 111,167                             | 219,459                            | 5.0                                    | ----                              | ----                                 | 470                 |
| 391                         | 591    | 3                      | 114,077                    | 114,077                             | 333,536                            | 7.7                                    | ----                              | ----                                 | 471                 |
| 397                         | 597    | 4                      | 117,023                    | 117,023                             | 450,558                            | 10.3                                   | 0.0                               | 34.3                                 | 472                 |
| 403                         | 603    | 5                      | 120,005                    | 120,005                             | 570,563                            | 13.1                                   | 2.8                               | 31.5                                 | 473                 |
| 409                         | 609    | 6                      | 123,023                    | 123,023                             | 693,585                            | 15.9                                   | 5.6                               | 28.7                                 | 474                 |
| 415                         | 615    | 7                      | 126,077                    | 126,077                             | 819,662                            | 18.8                                   | 8.5                               | 25.8                                 | 475                 |
| 421                         | 621    | 8                      | 129,167                    | 129,167                             | 948,828                            | 21.8                                   | 11.4                              | 22.8                                 | 476                 |
| 427                         | 627    | 9                      | 132,293                    | 132,293                             | 1,081,121                          | 24.8                                   | 14.5                              | 19.8                                 | 477                 |
| 433                         | 633    | 10                     | 135,455                    | 135,455                             | 1,216,575                          | 27.9                                   | 17.6                              | 16.7                                 | 478                 |
| 439                         | 639    | 11                     | 138,653                    | 138,653                             | 1,355,228                          | 31.1                                   | 20.8                              | 13.5                                 | 479                 |
| 445                         | 645    | 12                     | 141,887                    | 141,887                             | 1,497,114                          | 34.4                                   | 24.0                              | 10.2                                 | 480                 |
| 451                         | 651    | 13                     | 145,157                    | 145,157                             | 1,642,271                          | 37.7                                   | 27.4                              | 6.9                                  | 481                 |
| 457                         | 657    | 14                     | 148,463                    | 148,463                             | 1,790,733                          | 41.1                                   | 30.8                              | 3.5                                  | 482                 |
| 463                         | 663    | 15                     | 151,805                    | 151,805                             | 1,942,538                          | 44.6                                   | 34.3                              | 0.0                                  | 483                 |
| 469                         | 669    | 16                     | 155,183                    | 155,183                             | 2,097,720                          | 48.2                                   | 37.8                              |                                      | 484                 |

- NOTES:
- 1 The table is valid for a triangular pond with a uniform interior side slope.
  - 2 The table utilizes the 'end area method' of volume estimation utilizing the area of each one foot increment of pond depth, beginning at the bottom.
  - 3 The volume due to the bottom slope below the 468 feet elevation was not considered in the capacity volume calculations. A minimum depth of three feet in the pond bottom is planned at all times.
  - 4 The upper three feet of the pond are not counted in the capacity volume calculations due to the need to maintain a minimum freeboard to prevent wave damage above the maximum water level at all times.

Elevation:

|     |                            |                                                                    |
|-----|----------------------------|--------------------------------------------------------------------|
| 468 | Pond Bottom                |                                                                    |
| 471 | Minimum working depth      | Three feet of water to prevent growth of objectionable vegetation. |
| 483 | Reserve for storm          | 25 year, 24 hour storm event.                                      |
| 484 | Maximum high water         | Three feet below emergency spillway.                               |
| 487 | Flood protection elevation | Height of emergency spillway.                                      |

<sup>1</sup> Rainfall intensities are from RAINFALL FREQUENCY ATLAS OF THE MIDWEST by Floyd A. Huff and James R. Angel, Midwestern Climate Center, 1992, <http://www.sws.uiuc.edu/pubdoc/B/ISWSB-71.pdf>

**Ameren Labadie Energy Center Utility Waste Landfill  
Stormwater Management Pond 2  
Pond Volume Calculations  
Table N-9**

| Base Width of Pond in feet  |        | 144                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
|-----------------------------|--------|------------------------|----------------------------|-------------------------------------|------------------------------------|----------------------------------------|-----------------------------------|--------------------------------------|---------------------|
| Base Length of Pond in feet |        | 714                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Rise of Slope in feet       |        | 1                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Run of Slope in feet        |        | 3                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| WIDTH<br>(FT)               | LENGTH | WATER<br>LEVEL<br>(FT) | AVERAGE<br>AREA<br>(SQ FT) | VOLUME PER<br>INCREMENT<br>(VOL/FT) | TOTAL VOLUME<br>OF POND<br>(CU FT) | TOTAL VOLUME<br>OF POND<br>(ACRE FEET) | CAPACITY<br>IN USE<br>(ACRE FEET) | REMAINING<br>CAPACITY<br>(ACRE FEET) | Elevation<br>(FEET) |
| 144                         | 714    |                        |                            |                                     |                                    |                                        |                                   |                                      | 468                 |
| 150                         | 720    | 1                      | 105,408                    | 105,408                             | 105,408                            | 2.4                                    | -----                             | -----                                | 469                 |
| 156                         | 726    | 2                      | 110,628                    | 110,628                             | 216,036                            | 5.0                                    | -----                             | -----                                | 470                 |
| 162                         | 732    | 3                      | 115,920                    | 115,920                             | 331,956                            | 7.6                                    | 0.0                               | 42.0                                 | 471                 |
| 168                         | 738    | 4                      | 121,284                    | 121,284                             | 453,240                            | 10.4                                   | 2.8                               | 39.2                                 | 472                 |
| 174                         | 744    | 5                      | 126,720                    | 126,720                             | 579,960                            | 13.3                                   | 5.7                               | 36.3                                 | 473                 |
| 180                         | 750    | 6                      | 132,228                    | 132,228                             | 712,188                            | 16.3                                   | 8.7                               | 33.3                                 | 474                 |
| 186                         | 756    | 7                      | 137,808                    | 137,808                             | 849,996                            | 19.5                                   | 11.9                              | 30.1                                 | 475                 |
| 192                         | 762    | 8                      | 143,460                    | 143,460                             | 993,456                            | 22.8                                   | 15.2                              | 26.8                                 | 476                 |
| 198                         | 768    | 9                      | 149,184                    | 149,184                             | 1,142,640                          | 26.2                                   | 18.6                              | 23.4                                 | 477                 |
| 204                         | 774    | 10                     | 154,980                    | 154,980                             | 1,297,620                          | 29.8                                   | 22.2                              | 19.8                                 | 478                 |
| 210                         | 780    | 11                     | 160,848                    | 160,848                             | 1,458,468                          | 33.5                                   | 25.9                              | 16.2                                 | 479                 |
| 216                         | 786    | 12                     | 166,788                    | 166,788                             | 1,625,256                          | 37.3                                   | 29.7                              | 12.3                                 | 480                 |
| 222                         | 792    | 13                     | 172,800                    | 172,800                             | 1,798,056                          | 41.3                                   | 33.7                              | 8.4                                  | 481                 |
| 228                         | 798    | 14                     | 178,884                    | 178,884                             | 1,976,940                          | 45.4                                   | 37.8                              | 4.2                                  | 482                 |
| 234                         | 804    | 15                     | 185,040                    | 185,040                             | 2,161,980                          | 49.6                                   | 42.0                              | 0.0                                  | 483                 |
| 240                         | 810    | 16                     | 191,268                    | 191,268                             | 2,353,248                          | 54.0                                   | 46.4                              |                                      | 484                 |

- NOTES:
- 1 The table is valid for a rectangular pond with a uniform interior side slope.
  - 2 The table utilizes the 'end area method' of volume estimation utilizing the area of each one foot increment of pond depth, beginning at the bottom.
  - 3 The volume due to the bottom slope below the 468 feet elevation was not considered in the capacity volume calculations. A minimum depth of three feet in the pond bottom is planned at all times.
  - 4 The upper three feet of the pond are not counted in the capacity volume calculations due to the need to maintain a minimum freeboard to prevent wave damage above the maximum water level at all times.

Elevation:

|     |                            |                                                                    |
|-----|----------------------------|--------------------------------------------------------------------|
| 468 | Pond Bottom                |                                                                    |
| 471 | Minimum working depth      | Three feet of water to prevent growth of objectionable vegetation. |
| 483 | Reserve for storm          | 25 year, 24 hour storm event.                                      |
| 484 | Maximum high water         | Three feet below emergency spillway.                               |
| 487 | Flood protection elevation | Height of emergency spillway.                                      |

<sup>1</sup> Rainfall intensities are from RAINFALL FREQUENCY ATLAS OF THE MIDWEST by Floyd A. Huff and James R. Angel, Midwestern Climate Center, 1992, <http://www.sws.uiuc.edu/pubdoc/B/ISWSB-71.pdf>

**Ameren Labadie Energy Center Utility Waste Landfill  
Stormwater Management Pond 3  
Pond Volume Calculations  
Table N-10**

| Base Width of Pond in feet  |        | 233                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
|-----------------------------|--------|------------------------|----------------------------|-------------------------------------|------------------------------------|----------------------------------------|-----------------------------------|--------------------------------------|---------------------|
| Base Length of Pond in feet |        | 598                    |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Rise of Slope in feet       |        | 1                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| Run of Slope in feet        |        | 3                      |                            |                                     |                                    |                                        |                                   |                                      |                     |
| WIDTH<br>(FT)               | LENGTH | WATER<br>LEVEL<br>(FT) | AVERAGE<br>AREA<br>(SQ FT) | VOLUME PER<br>INCREMENT<br>(VOL/FT) | TOTAL VOLUME<br>OF POND<br>(CU FT) | TOTAL VOLUME<br>OF POND<br>(ACRE FEET) | CAPACITY<br>IN USE<br>(ACRE FEET) | REMAINING<br>CAPACITY<br>(ACRE FEET) | Elevation<br>(FEET) |
| 233                         | 598    |                        |                            |                                     |                                    |                                        |                                   |                                      | 468                 |
| 239                         | 604    | 1                      | 70,923                     | 70,923                              | 70,923                             | 1.6                                    | -----                             | -----                                | 469                 |
| 245                         | 610    | 2                      | 73,452                     | 73,452                              | 144,374                            | 3.3                                    | -----                             | -----                                | 470                 |
| 251                         | 616    | 3                      | 76,017                     | 76,017                              | 220,391                            | 5.1                                    | -----                             | -----                                | 471                 |
| 257                         | 622    | 4                      | 78,618                     | 78,618                              | 299,008                            | 6.9                                    | 0.0                               | 24.0                                 | 472                 |
| 263                         | 628    | 5                      | 81,255                     | 81,255                              | 380,263                            | 8.7                                    | 1.9                               | 22.2                                 | 473                 |
| 269                         | 634    | 6                      | 83,928                     | 83,928                              | 464,190                            | 10.7                                   | 3.8                               | 20.2                                 | 474                 |
| 275                         | 640    | 7                      | 86,637                     | 86,637                              | 550,827                            | 12.6                                   | 5.8                               | 18.2                                 | 475                 |
| 281                         | 646    | 8                      | 89,382                     | 89,382                              | 640,208                            | 14.7                                   | 7.8                               | 16.2                                 | 476                 |
| 287                         | 652    | 9                      | 92,163                     | 92,163                              | 732,371                            | 16.8                                   | 9.9                               | 14.1                                 | 477                 |
| 293                         | 658    | 10                     | 94,980                     | 94,980                              | 827,350                            | 19.0                                   | 12.1                              | 11.9                                 | 478                 |
| 299                         | 664    | 11                     | 97,833                     | 97,833                              | 925,183                            | 21.2                                   | 14.4                              | 9.7                                  | 479                 |
| 305                         | 670    | 12                     | 100,722                    | 100,722                             | 1,025,904                          | 23.6                                   | 16.7                              | 7.3                                  | 480                 |
| 311                         | 676    | 13                     | 103,647                    | 103,647                             | 1,129,551                          | 25.9                                   | 19.1                              | 5.0                                  | 481                 |
| 317                         | 682    | 14                     | 106,608                    | 106,608                             | 1,236,158                          | 28.4                                   | 21.5                              | 2.5                                  | 482                 |
| 323                         | 688    | 15                     | 109,605                    | 109,605                             | 1,345,763                          | 30.9                                   | 24.0                              | 0.0                                  | 483                 |
| 329                         | 694    | 16                     | 112,638                    | 112,638                             | 1,458,400                          | 33.5                                   | 26.6                              |                                      | 484                 |

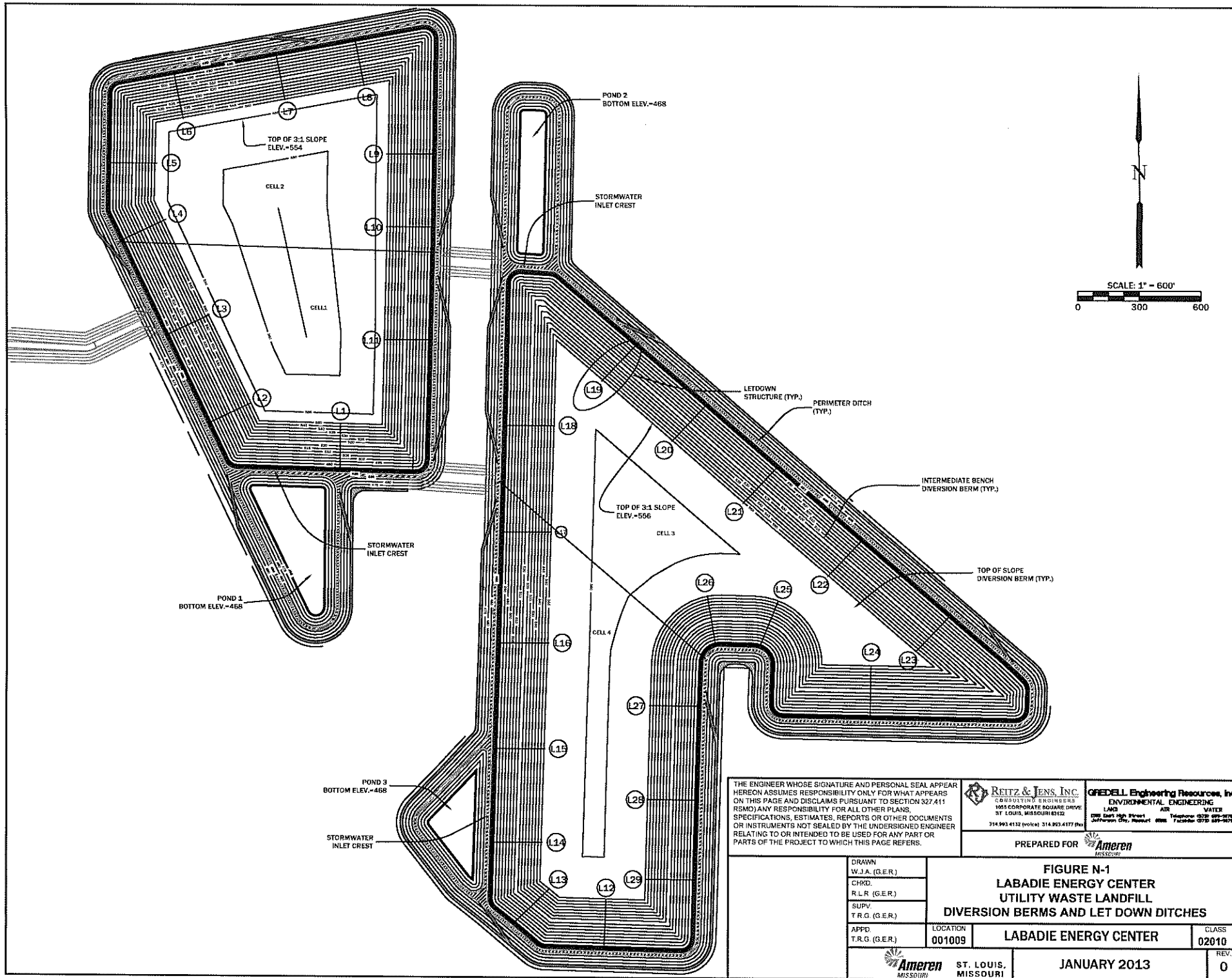
- NOTES
- 1 The table is valid for a triangular pond with a uniform interior side slope.
  - 2 The table utilizes the 'end area method' of volume estimation utilizing the area of each one foot increment of pond depth, beginning at the bottom.
  - 3 The volume due to the bottom slope below the 468 feet elevation was not considered in the capacity volume calculations. A minimum depth of three feet in the pond bottom is planned at all times.
  - 4 The upper three feet of the pond are not counted in the capacity volume calculations due to the need to maintain a minimum freeboard to prevent wave damage above the maximum water level at all times.

Elevation:

|     |                            |                                                                    |
|-----|----------------------------|--------------------------------------------------------------------|
| 468 | Pond Bottom                |                                                                    |
| 471 | Minimum working depth      | Three feet of water to prevent growth of objectionable vegetation. |
| 483 | Reserve for storm          | 25 year, 24 hour storm event.                                      |
| 484 | Maximum high water         | Three feet below emergency spillway.                               |
| 487 | Flood protection elevation | Height of emergency spillway.                                      |

<sup>1</sup> Rainfall intensities are from RAINFALL FREQUENCY ATLAS OF THE MIDWEST by Floyd A. Huff and James R. Angel, Midwestern Climate Center, 1992, <http://www.sws.uiuc.edu/pubdoc/B/ISWSB-71.pdf>

# FIGURES



# **Appendix O**

## H.E.L.P Model Results

**Ameren Missouri Labadie Energy Center  
Utility Waste Landfill  
Franklin County, MO  
December 2012**

**H.E.L.P. Model Summary Results  
Appendix O**

This appendix summarizes the H.E.L.P. model results. The model cases and inputs follow the liner and leachate collection design details provided on Sheets 16 through 19 of the plan sheets. Version 3.07 of the Hydrologic Evaluation of Landfill Performance (H.E.L.P.) computer model was used to evaluate the anticipated performance of the design of the leachate collection and cover systems for selected cases. Three cases were modeled: 1.) The initial Coal Combustion Products (CCP) placement, 2.) An “operational” condition, and 3.) The final closed condition. The cases are described below.

Table O-1 (Cell 1), Summary of H.E.L.P. Model Results & Input Parameters, provides a summary of the results from the H.E.L.P. model cases. H.E.L.P. model reports for each case listed in Table O-1 are included in sub-appendices. For consistency, the following assumptions were made:

- The aggregate drainage layer is unaffected by textile intrusion.
- The geocomposite drainage layer is affected by textile intrusion as described by Robert M. Koerner in “Designing with Geosynthetics”, fifth edition published in 2005 (Table O-2).
- Where textile intrusion is anticipated, the amount of intrusion resulting from the maximum height of CCP placed on the geocomposite is modeled beginning with the initial placement of CCP and is held constant as additional CCP was placed on the liner.
- The drainage layer is not affected by biological clogging.
- Initial moisture content was user specified in all cases. All layers, where applicable, were modeled at field capacity except for fly ash, which was modeled at 0.22 vol/vol (Provided by Reitz & Jens, Inc.).

The H.E.L.P. Model evaluations were run using precipitation, temperature, solar radiation, and evapotranspiration for St. Louis, Missouri and soil data for the Ameren Missouri Labadie Energy Center UWL. The H.E.L.P. model cases were run for appropriate periods and the peak daily values are presented to represent worst-case conditions.

Properties of the various materials for design of the layers were considered. The H.E.L.P. Model cases utilizing an aggregate drain layer with a minimum hydraulic conductivity of 0.25 cm/sec and only the initial layer of CCP indicates that the minimum value of hydraulic

conductivity of locally available aggregate materials resulted in less head on the liner than the regulatory limit of 12 inches. The particle gradation of the protective layer above the drain layer was designed to prevent the fine fly ash from migrating into, and plugging, the drain layer. The protective layer gradation analysis is provided in memo by Bruce Dawson, P.E., dated June 22, 2012 (Appendix O-1). For the alternate use of geocomposites, the manufacturer's stated transmissivity, shown on the product sheets, was reduced using Koerner's method (Table O-2).

Results in Table O-1 are reported for the cases of initial, operating and closed conditions, for aggregate material and geocomposite drain layers for: (1) the 1% base (floor) for the landfill, (2) the 33% side slope; (3) and the Schroeder approximation. Results for the maximum head on the liner, peak daily leachate flow, average annual leachate flow and the annual leachate volume are reported.

The potential effect of geotextile intrusion in the drainage layer was evaluated for the initial placement of CCP over a geocomposite drainage layer. The product data sheets (Appendix O-1) are summarized in the attached table titled "Effect of Reduction Factors on Hydraulic Conductivity", Table O-2. The H.E.L.P. Model cases for the geocomposite drain layer were run with a resultant hydraulic conductivity of 1.3 cm/sec as specified by the GSE PermaNet HL (10oz/yd<sup>2</sup>) geocomposite in Table O-2. The transmissivities reported for each geonet are converted into hydraulic conductivity by dividing the transmissivity by the thickness of the geonet. These transmissivities are further reduced by factors for creep, chemical clogging, geotextile intrusion and particle clogging in a method proposed by Koerner in *Designing with Geosynthetics* 5<sup>th</sup> Edition. Koerner divided (reduced) the transmissivity by each factor. The reduction factors assumed by Koerner are also summarized in the attached table. A brief description of each of the reduction factors follows:

Creep is the deformation of the geonet under an applied load. The pressure from coal combustion products will reduce the thickness of the geocomposite. Published values for creep are used where available, otherwise a value of 1.8 was assumed. Creep was not considered an influence for gravel.

Chemical clogging occurs when dissolved substances form a precipitate that deposits in the drainage layer. Most of the coal combustion products are expected to have low solubilities in water. A value of 1.8 was assigned to reduce transmissivity by 55% for both the gravel and the geocomposite.

Geotextile intrusion occurs when the geotextile is forced into the geonet. For bonded geotextile-geonet-geotextile composites, this intrusion is considered. A factor of 2 has been assigned to account for geotextile intrusion into the geonet. For the 12 inch gravel layer, geotextile intrusion is not expected to be a significant problem.

Particle clogging from infiltration occurs when particles fill in the openings in the geotextile. In a similar way to a coffee filter protecting the drain in a coffee pot from

plugging, the geotextile serves to protect the geonet or gravel from plugging. Koerner handles particle clogging as a filtration problem. To be consistent with this analysis, the transmissivity was reduced by a factor of 1.8 to account for particle clogging. Dawson provides analysis of local materials to be used to prevent particle clogging.

Koerner also suggests biological clogging. This clogging of the geonet or gravel occurs when microbes have a supply of organic nutrients and water. The disposal of coal combustion products is not anticipated to supply organic nutrients to the extent that a sanitary landfill might. Therefore, it is assumed that biological clogging will not affect the drainage layer and the factor is set at 1.

Taken together, these reductions on the hydraulic conductivity result in a more-than ten-fold reduction in the published values for the geocomposite materials.

The cases modeled include initial, operating and closed conditions. The H.E.L.P. model runs are identified by the conditions modeled and the material used in the leachate collection layer. The case identification numbering system is also explained below:

#### Condition

- Initial condition is identified by "I" and models the initial phase of construction with waste still below the top of berm. This condition is modeled for a period of seven years (7 yr.).
  - AM signifies aggregate materials used for the leachate drainage layer and is layered (top down) as;
    - Coal Combustion Products. (vertical percolation)
    - A protective layer of graded aggregate to keep fly ash from migrating into the leachate collection layer. (vertical percolation)
    - Geotextile separator between the protective layer and the aggregate materials of the leachate collection layer. (not included in H.E.L.P model)
    - Aggregate materials are clean aggregate with a minimum hydraulic conductivity. (lateral drainage or leachate collection layer)
    - A geomembrane liner (primary liner) is next. (synthetic barrier)
    - Finally, a layer of 2-foot thick compacted clay soil (secondary liner) in contact with the geomembrane to form the composite liner. (soil barrier)
  - Case Identification Numbers 1, 2 and 3 indicate modeling of the 1% floor of the cell, the 33% inner side slope of the cell and the Schroeder approximation of the floor and side slope of the cell. Schroeder's approximation is used to approximate the longest length to the leachate collection pipe in order to accurately estimate head on the liner. It was used for the Initial and Operational cases to model the combined effects of the

33% sidewall and 1% floor of the bottom liner. The equation for Schroeder's Approximation ( $L'$ ) is: length of the bottom slope \* (volume of water from the bottom + volume of water at sidewall) / volume of water from the bottom  $\{L'=L_b*(V_b+V_s)/V_b\}$ . Schroeder's approximation was not used on the final, closed condition case. Dr. Paul Schroeder of the USCOE, provided this approximation to the Missouri Department of Natural Resources in response to a question about a very long side slope at another landfill. It is used here to make sure no extreme flows are being missed.

- The designation like R003, is reserved for the use of revisions to any particular run using the format of Rxxx, where xxx is the run number.
- GE signifies geocomposites used in the leachate collection layer and is layered (top down) as:
  - Coal Combustion Products. (vertical percolation)
  - A protective layer of graded aggregate to keep fly ash from migrating into the leachate collection layer. (vertical percolation)
  - The geocomposite is manufactured as a composition of geotextile fabric-geonet-geotextile fabric. (lateral drainage or leachate collection layer)
  - A geomembrane liner (primary liner) is next. (synthetic barrier)
  - Finally, a layer of 2-foot thick compacted clay soil (secondary liner) in contact with the geomembrane to form the composite liner. (soil barrier)
- Operating condition models the placement of coal combustion products above the top of the perimeter berm and having an additional layer of soil placed as an intermediate cover for the cell. The intermediate cover is used for both the aggregate material and the geocomposite leachate models. The operating conditions were modeled for a period of 25 years.
- Closed condition models the placement of a final cap over the top of landfill. For both aggregate materials and geocomposite leachate collection it is modeled as:
  - A vegetative soil layer to support grasses. (vertical percolation)
  - A geotextile used as a cushion and drainage layer. (lateral drainage)
  - A geomembrane liner is used as a primary liner to prevent water from getting to the coal combustion products. (vertical barrier)
  - Layering below follows the pattern in the operating and initial conditions.

The operating condition is found to be the case that produces the most leachate. The precipitation falling on the initial layer of CCP has little chance for storage in the CCP column. It is more quickly transported to the leachate drainage layer and geomembrane

liner. The hydraulic head forces this water to flow into the leachate collection system. If the maximum hydraulic head can be maintained below the regulatory limit under the case of initial CCP placement, placement of additional CCP allows for more storage of water within the CCP mass and may lower the maximum hydraulic head on the geomembrane liner.

The H.E.L.P. model cases are sensitive to the length of the flow path of leachate in the drainage layer. As proposed, Phase 1/Cell 1 has the longest flow path present in any of the phases of the UWL. Cell 1 is also the cell that is opened first. The longest distance of 541 feet was scaled from the toe of slope to the leachate collection system perpendicular to contours. The side slope was also modeled and the impact on flow was incorporated using the Schroeder approximation.

As proposed, Phase 3/Cell 3 is expected to have the maximum leachate flow present in any of the phases of the UWL due to size (57 acres). The largest leachate collection zone in Cell 3 is smaller than the largest collection zone in Cell 1. The longest distance of 400 feet (as scaled from the dividing break-line in the leachate collection zone perpendicular to the leachate collection line contours) is significantly shorter than Cell 1. Therefore, Cell 1 represents the worst case scenario.

Critical cases presented indicate that the design parameters proposed will meet the regulatory standards for effectively collecting leachate while not allowing a hydraulic head on the liner that exceeds the regulatory limit of 12-inches. These cases are summarized on Table O-1 with H.E.L.P. results in Appendices O-2 through O-13.

The H.E.L.P. model results indicate that the leachate collection, liner and cover systems meet regulatory requirements. The model results also indicate that peak leachate flows and maximum hydraulic head on the bottom liner occurs during the intermediate operation of each cell when there is an average 20-foot thickness of CCP over the liner and leachate collection system, and intermediate cover is in place. Therefore, the worst case is expected to be short-lived and the performance of the liner and leachate collections system is expected to improve as additional CCP is placed in the disposal cell. After closure, the leachate generation rates drop substantially.

# TABLES

**Ameren Missouri  
Labadie Energy Center Utility Waste Landfill  
Franklin, County Missouri**

**TABLE O-1: SUMMARY OF HELP MODEL RESULTS & INPUT PARAMETERS  
for Cell 1**

| Sub Appendix                                                                                   | Case No. | Acres | Case Modeled                                                                                                                        | Drainage Layer Material | Drainage Length (ft) | Maximum Head on Liner (in) | Peak Daily Leachate Volume |                                 | Average Annual Leachate Volume |                                 | Rainfall                               |                                   |
|------------------------------------------------------------------------------------------------|----------|-------|-------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----------------------|----------------------------|----------------------------|---------------------------------|--------------------------------|---------------------------------|----------------------------------------|-----------------------------------|
|                                                                                                |          |       |                                                                                                                                     |                         |                      |                            | (ft <sup>3</sup> /day)     | Flow GPM (GPAD) See Notes 5 & 6 | (ft <sup>3</sup> /year)        | Flow GPM (GPAD) See Notes 5 & 6 | Average Annual (ft <sup>3</sup> /year) | Peak Daily (ft <sup>3</sup> /day) |
| Initial Waste Placement Condition - Modeled at 7 Years - 7 ft of Waste - No Intermediate Cover |          |       |                                                                                                                                     |                         |                      |                            |                            |                                 |                                |                                 |                                        |                                   |
| O-2                                                                                            | IAM1R003 | 28.1  | Cell 1 using Aggregate Material in the leachate collection system for the 1% bottom slope of the landfill.                          | Aggregate Material      | 541                  | 0.540                      | 746                        | NA                              | 91,489                         | NA                              | NA                                     | NA                                |
| O-3                                                                                            | IAM3R003 | 31.4  | Cell 1 using Aggregate Materials in the leachate collection system. Use Schroeder's approximation for drainage length (See Note 3). | Aggregate Material      | 725                  | 0.7                        | 812                        | 4.2 (193.4)                     | 108,533                        | 1.5 (70.8)                      | 3,869,852                              | 296,354                           |
| O-4                                                                                            | IGE1R003 | 28.1  | Cell 1 using Geocomposite in the leachate collection system for the 1% bottom slope of the landfill.                                | Geocomposite            | 541                  | 0.114                      | 803                        | NA                              | 91,742                         | NA                              | NA                                     | NA                                |
| O-5                                                                                            | IGE2R003 | 3.3   | Cell 1 using Geocomposites in the leachate collection system for the 33% side slopes of the landfill.                               | Geocomposite            | 60                   | 0.012                      | 253                        | NA                              | 20,904                         | NA                              | NA                                     | NA                                |
| O-6                                                                                            | IGE3R003 | 31.4  | Cell 1 using Geocomposites in the leachate collection system. Use Schroeder's approximation for drainage length (See Note 3).       | Geocomposite            | 712                  | 0.149                      | 887                        | 4.6 (211.3)                     | 108,979                        | 1.6 (71.1)                      | 3,869,852                              | 296,354                           |

Notes located on Page 3 of 3

**Ameren Missouri  
Labadie Energy Center Utility Waste Landfill  
Franklin, County Missouri**

**TABLE O-1: SUMMARY OF HELP MODEL RESULTS & INPUT PARAMETERS  
for Cell 1**

| Sub Appendix                                                                                 | Case No. | Acres | Case Modeled                                                                                                                                                                    | Drainage Layer Material | Drainage Length (ft) | Maximum Head on Liner (in) | Peak Daily Leachate Volume |                                 | Average Annual Leachate Volume |                                 | Rainfall                  |                      |
|----------------------------------------------------------------------------------------------|----------|-------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----------------------|----------------------------|----------------------------|---------------------------------|--------------------------------|---------------------------------|---------------------------|----------------------|
|                                                                                              |          |       |                                                                                                                                                                                 |                         |                      |                            | (ft³/day)                  | Flow GPM (GPAD) See Notes 5 & 6 | (ft³/year)                     | Flow GPM (GPAD) See Notes 5 & 6 | Average Annual (ft³/year) | Peak Daily (ft³/day) |
| Intermediate Operating Condition - Modeled at 25 Years - 20 ft of Waste - Intermediate Cover |          |       |                                                                                                                                                                                 |                         |                      |                            |                            |                                 |                                |                                 |                           |                      |
| O-7                                                                                          | OAM1R003 | 28.1  | Cell 1 Operating Condition with Intermediate Cover using Aggregate Materials in the leachate collection system for the 1% bottom slope of the landfill.                         | Aggregate Material      | 541                  | 1.437                      | 2,060                      | NA                              | 287,168                        | NA                              | 3,411,430                 | 350,891              |
| O-8                                                                                          | OAM3R003 | 31.4  | Cell 1 Operating Condition with Intermediate Cover using Aggregate Materials in the leachate collection system. Use Schroeder's approximation for drainage length (See Note 3). | Aggregate Material      | 637                  | 1.66                       | 2,254                      | 11.7 (536.9)                    | 320,708                        | 4.6 (209.3)                     | 3,812,060                 | 392,099              |
| O-9                                                                                          | OGE1R003 | 28.1  | Cell 1 Operating Condition with Intermediate Cover using Geocomposites in in the leachate collection system for the 1% bottom slope of the landfill.                            | Geocomposite            | 541                  | 0.336                      | 2,368                      | NA                              | 287,681                        | NA                              | 3,411,430                 | 350,891              |
| O-10                                                                                         | OGE2R003 | 3.3   | Cell 1 Operating Condition for 33% side slopes with Intermediate Cover using Geocomposites in the leachate collection system.                                                   | Geocomposite            | 60                   | 0.016                      | 375                        | NA                              | 36,856                         | NA                              | 400,631                   | 41,208               |
| O-11                                                                                         | OGE3R003 | 31.4  | Cell 1 Operating Condition with Intermediate Cover using Geocomposites in the leachate collection system. Use Schroeder's approximation for drainage length (See Note 3).       | Geocomposite            | 627                  | 0.4                        | 2,571                      | 13.4 (612.5)                    | 321,394                        | 4.6 (209.8)                     | 3,812,060                 | 392,099              |

Notes located on Page 3 of 3

**Ameren Missouri  
Labadie Energy Center Utility Waste Landfill  
Franklin, County Missouri**

**TABLE O-1: SUMMARY OF HELP MODEL RESULTS & INPUT PARAMETERS  
for Cell 1**

| Sub Appendix                                                           | Case No. | Acres | Case Modeled                                                                                                                                  | Drainage Layer Material | Drainage Length (ft) | Maximum Head on Liner (in) | Peak Daily Leachate Volume |                                 | Average Annual Leachate Volume |                                 | Rainfall                               |                                   |
|------------------------------------------------------------------------|----------|-------|-----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----------------------|----------------------------|----------------------------|---------------------------------|--------------------------------|---------------------------------|----------------------------------------|-----------------------------------|
|                                                                        |          |       |                                                                                                                                               |                         |                      |                            | (ft <sup>3</sup> /day)     | Flow GPM (GPAD) See Notes 5 & 6 | (ft <sup>3</sup> /year)        | Flow GPM (GPAD) See Notes 5 & 6 | Average Annual (ft <sup>3</sup> /year) | Peak Daily (ft <sup>3</sup> /day) |
| Closed Condition - Modeled at 30 Years - ~58 ft of Waste - Final Cover |          |       |                                                                                                                                               |                         |                      |                            |                            |                                 |                                |                                 |                                        |                                   |
| O-12                                                                   | CAM1R002 | 31.4  | Cell 1 Closed Condition with Final Cover using Aggregate Materials in the leachate collection system for the 1% bottom slope of the landfill. | Aggregate Material      | 541                  | 1.322                      | 211                        | 1.1 (50.3)                      | 22,376                         | 0.3 (14.6)                      | 3,785,646                              | 392,099                           |
| O-13                                                                   | CGE1R003 | 31.4  | Cell 1 Closed Condition with Final Cover using Geocomposites in the leachate collection system for the 1% bottom slope of the landfill.       | Geocomposite            | 541                  | 0.044                      | 346                        | 1.8 (82.4)                      | 23,252                         | 0.3 (15.2)                      | 3,785,646                              | 392,099                           |

Notes:

- 1 Leaf Area Index (LAI) values for the Initial & Operational cases were set at 0.5 to assume bare ground conditions. LAI values for the Closed condition were set at 2.0 to assume average ground conditions. LAI values ranges for the Labadie area are from 0 to 4.5.
- 2 Geotextile layers at the bottom of the leachate collection protective cover and at the bottom of the Aggregate Material layer are not included in the HELP model cases. The k values of these layers are similar to their adjacent layers and their relatively small thickness make their affect negligible.
- 3 Schroeder's approximation is used to approximate the longest length to the leachate collection in order to accurately estimate head on the liner. It was used for the Initial and Operational cases to model the combined effects of the sidewall and floor of the bottom liner. The equation for Schroeder's Approximation (L') is: length of the bottom slope \* (volume of water from the bottom + volume of water at sidewall) / volume of water from the bottom (L'=Lb\*(Vb+Vs)/Vb). Schroeder's approximation was not used on the closed condition.
- 4 Depth of waste placement on side slope cases are an average height of waste over/under slope.
- 5 Gallons per minute (GPM) is calculated from the reported peak and average daily volume in cubic feet per day and cubic feet per year, respectively, within the HELP model cases.
- 6 Gallons per acre per day (GPAD) is calculated from the reported peak and average daily volume in cubic feet per day and cubic feet per year, respectively, within the HELP model cases.
- 7 Schroeder's Approximation was not used for Closed condition cases since no leachate was generated.
- 8 Vegetative soil modeled as Silt Loam (ML).
- 9 Initial moisture content was user specified in all cases. All layers (where applicable) were modeled at field capacity except for Fly Ash, which was modeled at 0.22 vol/vol (from R&J).
- 10 SCS curve numbers were determined by the HELP model in all cases.
- 11 HELP Model Case No. Description:  
Character 1: Denotes the landfill condition modeled. I - initial waste placement, O - intermediate operating, C - closed  
Characters 2 - 3: Denote the type of leachate collection system modeled. GE - geocomposite, AM - aggregate material.  
Character 4: Denotes the location along the bottom liner that was modeled. 1 - floor (bottom at 1%), 2 - side slope at 33%, 3 - Schroeder's Approximation  
Characters 5 - 8: Reserved for the use of revisions to any particular run using the format of Rxxx, where xxx is the run number.
- 12 NA - Not applicable values in the sum of leachate flow or precipitation.

**Ameren Missouri  
Labadie Energy Center Utility Waste Landfill  
Franklin County, Missouri**

**EFFECT OF REDUCTION FACTORS ON HYDRAULIC CONDUCTIVITY**

**For geonet with two sided geotextile**

Reduction Factors assumed by Koerner in Designing with Geosynthetics, 5th Ed. 2005

**Table O-2**

| GEONET WITH GEOTEXTILE<br>INTRUSION     | GEONET                  |      |                                                                            |    |                                     | REDUCTION FACTORS |                                |                                   |                                |                                                  |
|-----------------------------------------|-------------------------|------|----------------------------------------------------------------------------|----|-------------------------------------|-------------------|--------------------------------|-----------------------------------|--------------------------------|--------------------------------------------------|
| MANUFACTURER / MODEL<br>NUMBER          | THICKNESS<br>MILS    CM |      | <sup>1</sup> TRANSMISSIVITY<br>M <sup>2</sup> /SEC    CM <sup>2</sup> /SEC |    | HYDRAULIC<br>CONDUCTIVITY<br>CM/SEC | CREEP<br>FACTOR   | CHEMICAL<br>CLOGGING<br>FACTOR | GEOTEXTILE<br>INTRUSION<br>FACTOR | PARTICLE<br>CLOGGING<br>FACTOR | RESULTANT<br>HYDRAULIC<br>CONDUCTIVITY<br>CM/SEC |
| GSE PermaNet TRx (8oz/yd <sup>2</sup> ) | 300                     | 0.76 | 2.2E-03                                                                    | 22 | 28.9                                | 1.80              | 1.80                           | 2                                 | 1.80                           | 2.5                                              |
| GSE PermaNet HL (10oz/yd <sup>2</sup> ) | 270                     | 0.69 | 1.0E-03                                                                    | 10 | 14.6                                | 1.80              | 1.80                           | 2                                 | 1.80                           | 1.3                                              |
| GSE PermaNet UL (10oz/yd <sup>2</sup> ) | 300                     | 0.76 | 1.0E-03                                                                    | 10 | 13.1                                | 1.80              | 1.80                           | 2                                 | 1.80                           | 1.1                                              |

**NOTES:**

1. Transmissivity as reported for various geocomposites from manufacturer's product data sheets.

# APPENDICES

## **Appendix O-1**

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Jefferson City, Missouri 65101  
Telephone No. (573) 659-9078  
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**GREDELL Engineering  
Resources, Inc.**

# Memo

**To:** Rick Roberts, P.E.  
**From:** Bruce Dawson, P.E.  
**CC:** Tom Gredell, P.E.  
**Date:** 6/22/2012  
**Re:** Reitz & Jens: Labadie UWL/Protective Cover Specification Development

---

## **Proposed Specification Language:**

Protective cover shall consist of a well-graded aggregate with a particle size between 9.5 mm and 0.075 mm, with 0 to 10 percent passing the No. 100 U.S. Sieve, a  $d_{50}$  particle size of (approximately) 0.5 to 0.9 mm, and a  $d_{15}$  particle size of (approximately) 0.2 to 0.4 mm.

## **Background:**

**MoDOT concrete sand (Missouri Standard Specifications for Highway Construction Section 1005):**

|                               |        |
|-------------------------------|--------|
| % Passing 3/8" (9.5mm):       | 100    |
| % Passing No. 4 (4.75 mm):    | 95-100 |
| % Passing No. 8 (2.38 mm):    | 70-100 |
| % Passing No. 16 (1.20 mm):   | 45-90  |
| % Passing No. 30 (0.599 mm):  | 15-65  |
| % Passing No. 50 (0.297 mm):  | 5-30   |
| % Passing No. 100 (0.152 mm): | 1-10   |

## **Estimated Coefficient of Permeability per Eq. 2.4, Peck Hanson Thornburn, p. 40:**

$k = CD_{10}^2$ , where  $C = 100/\text{cm-sec}$  and  $D_{10}$  is expressed in centimeters  
for the above gradation,  $D_{10}$  will be between 0.0297 and 0.0152 centimeters;  
 $k$  is therefore estimated to be between 0.023 cm/sec and 0.088 cm/sec

## **Filter criteria per Table 2.2, Peck Hanson Thornburn, p. 49:**

Non-uniform, sub-rounded particles:  $R_{50}$  between 12 and 58;  $R_{15}$  between 12 and 40  
Fly ash (from Reitz & Jens Fig 3-1, Labadie):  $d_{50}$  approx. 0.027 mm,  $d_{15}$  approx. 0.02 mm  
Missouri River Sand (from examination of select sieve results from Washington Sand Co.):  
 $D_{50}$  approx. 0.5 to 0.9 mm,  $d_{15}$  approx. 0.2 to 0.35 mm  
Resultant ratios:  $R_{50}$  between 19 and 33,  $R_{15}$  between 10 and 18.

## **Conclusion:**

"Typical" Missouri river sand dredged for concrete sand will protect Fly ash, per PHT Table 2.2 criteria.

## **Notes:**

Develop "Note 5" in Detail Drawings to address Protective Cover Material requirements. Compare to similar material requirements note for non-carbonate aggregate drainage material and provide similar, parallel language.

# GSE Nonwoven Geotextiles

GSE Nonwoven Geotextiles are a family of staple fiber needlepunched geotextiles. The geotextiles are manufactured using an advanced manufacturing and quality system to produce the most uniform and consistent nonwoven needlepunched geotextile currently available in the industry. GSE combines a fiber selection and approval system with an in-line quality control and a state-of-the-art laboratory to ensure that every roll shipped meets customer specifications.



## AT THE CORE:

A family of geotextiles used for separation, filtration, protection and drainage applications.

## Product Specifications

These product specifications meet GRI GT12, GRI GT13 and AASHTO M288

| Tested Property                          | Test Method | Frequency               | Minimum Average Roll Value |               |               |                |                |                |
|------------------------------------------|-------------|-------------------------|----------------------------|---------------|---------------|----------------|----------------|----------------|
|                                          |             |                         | NW4                        | NW6           | NW8           | NW10           | NW12           | NW16           |
| AASHTO M288 Class                        |             |                         | 3                          | 2             | 1             | >1             | >>1            | >>>1           |
| Mass per Unit Area, oz/yd <sup>2</sup>   | ASTM D 5261 | 90,000 ft <sup>2</sup>  | 4                          | 6             | 8             | 10             | 12             | 16             |
| Grab Tensile Strength, lb                | ASTM D 4632 | 90,000 ft <sup>2</sup>  | 120                        | 160           | 220           | 260            | 320            | 390            |
| Grab Elongation, %                       | ASTM D 4632 | 90,000 ft <sup>2</sup>  | 50                         | 50            | 50            | 50             | 50             | 50             |
| Puncture Strength, lb                    | ASTM D 4833 | 90,000 ft <sup>2</sup>  | 60                         | 90            | 120           | 165            | 190            | 240            |
| Trapezoidal Tear Strength, lb            | ASTM D 4533 | 90,000 ft <sup>2</sup>  | 50                         | 65            | 90            | 100            | 125            | 150            |
| Apparent Opening Size, Sieve No. (mm)    | ASTM D 4751 | 540,000 ft <sup>2</sup> | 70<br>(0.212)              | 70<br>(0.212) | 80<br>(0.180) | 100<br>(0.150) | 100<br>(0.150) | 100<br>(0.150) |
| Permittivity, sec <sup>-1</sup>          | ASTM D 4491 | 540,000 ft <sup>2</sup> | 180                        | 150           | 130           | 100            | 80             | 60             |
| Water Flow Rate, gpm/ft <sup>2</sup>     | ASTM D 4491 | 540,000 ft <sup>2</sup> | 135                        | 110           | 95            | 75             | 60             | 45             |
| UV Resistance % retained after 500 hours | ASTM D 4355 | per formulation         |                            | 70            | 70            | 70             | 70             | 70             |
| <b>TYPICAL ROLL DIMENSIONS:</b>          |             |                         |                            |               |               |                |                |                |
| Roll Length <sup>1</sup> , ft            |             |                         | 850                        | 850           | 600           | 500            | 400            | 300            |
| Roll Width <sup>2</sup> , ft             |             |                         | 15                         | 15            | 15            | 15             | 15             | 15             |
| Roll Area, ft <sup>2</sup>               |             |                         | 12,750                     | 12,750        | 9,000         | 7,500          | 6,000          | 4,500          |

### NOTES:

- 1. The property values listed below are typical values. All values listed are Minimum Average Roll Values except Apparent Opening Size (mm) and UV resistance. Apparent Opening Size (mm) is the Maximum Average Roll Value. UV is a typical value.
- 2. Roll lengths and widths have a tolerance of ±1%.

GSE is a leading manufacturer and marketer of geosynthetic lining products and services. We've built a reputation of reliability through our dedication to providing consistency of product, price and protection to our global customers.

Our commitment to innovation, our focus on quality and our industry expertise allow us the flexibility to collaborate with our clients to develop a custom, purpose-fit solution.

**[ DURABILITY RUNS DEEP ]** For more information on this product and others, please visit us at [GSEworld.com](http://GSEworld.com), call 800.435.2008 or contact your local sales office.



# GSE PermaNet HL Geocomposite

GSE PermaNet HL (High Load) geocomposite is manufactured with a GSE PermaNet HL geonet heat-bonded on one or both sides with a GSE nonwoven needle-punched geotextile. The geotextile is available in mass per unit area range of 6 oz/yd<sup>2</sup> to 16 oz/yd<sup>2</sup>. The creep resistant structure of the product ensures continuous flow performance over a broad range of conditions and long durations. The geocomposite works as an efficient drainage medium and is ideal for extremely high compressive stress applications.



## AT THE CORE:

A high load geocomposite with a creep-resistant structure that ensures continuous flow performance and is ideal for extremely high compressive stress applications.

## Product Specifications

| Geocomposite                                                             | Test Method                   | Frequency                 | Minimum Average Value         |                               |                               |
|--------------------------------------------------------------------------|-------------------------------|---------------------------|-------------------------------|-------------------------------|-------------------------------|
|                                                                          |                               |                           | 6 oz/yd <sup>2</sup>          | 8 oz/yd <sup>2</sup>          | 10 oz/yd <sup>2</sup>         |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>2</sup> /sec)         | ASTM D 4716                   | 1/540,000 ft <sup>2</sup> | 4.8 (1 x 10 <sup>-3</sup> )   | 4.8 (1 x 10 <sup>-3</sup> )   | 4.8 (1 x 10 <sup>-3</sup> )   |
| Double-Sided Composite                                                   |                               |                           | 6.2 (1.3 x 10 <sup>-2</sup> ) | 6.2 (1.3 x 10 <sup>-2</sup> ) | 6.2 (1.3 x 10 <sup>-2</sup> ) |
| Single-Sided Composite                                                   |                               |                           |                               |                               |                               |
| Ply Adhesion, lb/in                                                      | ASTM D 7005                   | 1/50,000 ft <sup>2</sup>  | 1.0                           | 1.0                           | 1.0                           |
| <b>Geonet Core – GSE PermaNet HL (prior to lamination)<sup>(2)</sup></b> |                               |                           |                               |                               |                               |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>2</sup> /sec)         | ASTM D 4716                   |                           | 19 (4 x 10 <sup>-3</sup> )    | 19 (4 x 10 <sup>-3</sup> )    | 19 (4 x 10 <sup>-3</sup> )    |
| Compressive Strength, lbs/ft <sup>2</sup>                                | ASTM D 6364                   | 1/540,000 ft <sup>2</sup> | 40,000                        | 40,000                        | 40,000                        |
| Creep Reduction Factor                                                   | ASTM D 7406/7361              | per formulation           | 1.2 @15,000 psf               | 1.2 @15,000 psf               | 1.2 @15,000 psf               |
| Density, g/cm <sup>3</sup>                                               | ASTM D 1505                   | 1/50,000 ft <sup>2</sup>  | 0.94                          | 0.94                          | 0.94                          |
| Tensile Strength (MD), lb/in                                             | ASTM D 5035/7179              | 1/50,000 ft <sup>2</sup>  | 100                           | 100                           | 100                           |
| Carbon Black Content, %                                                  | ASTM D 1603 /4216             | 1/50,000 ft <sup>2</sup>  | 2.0                           | 2.0                           | 2.0                           |
| <b>Geotextile (prior to lamination)<sup>(3)</sup></b>                    |                               |                           |                               |                               |                               |
| Mass per Unit Area, oz/yd <sup>2</sup>                                   | ASTM D 5261                   | 1/90,000 ft <sup>2</sup>  | 6                             | 8                             | 10                            |
| Grab Tensile, lb                                                         | ASTM D 4632                   | 1/90,000 ft <sup>2</sup>  | 160                           | 220                           | 260                           |
| Puncture Strength, lb                                                    | ASTM D 4833                   | 1/90,000 ft <sup>2</sup>  | 90                            | 120                           | 165                           |
| AOS US Sieve (mm)                                                        | ASTM D 4751                   | 1/540,000 ft <sup>2</sup> | 70 (0.212)                    | 80 (0.180)                    | 100 (0.150)                   |
| Permittivity, sec <sup>-1</sup>                                          | ASTM D 4491                   | 1/540,000 ft <sup>2</sup> | 1.5                           | 1.3                           | 1.0                           |
| Flow Rate, gpm/ft <sup>2</sup>                                           | ASTM D 4491                   | 1/540,000 ft <sup>2</sup> | 110                           | 95                            | 75                            |
| UV Resistance, % Retained                                                | ASTM D 4355 (after 500 hours) | once per formulation      | 70                            | 70                            | 70                            |
| <b>NOMINAL ROLL DIMENSIONS</b>                                           |                               |                           |                               |                               |                               |
| Geonet Core Thickness, mil                                               | ASTM D 5199                   | 1/50,000 ft <sup>2</sup>  | 270                           | 270                           | 270                           |
| Roll Width <sup>(4)</sup> , ft                                           |                               |                           | 15                            | 15                            | 15                            |
| Roll Length <sup>(4)</sup> , ft                                          | Double-Sided Composite        |                           | 210                           | 200                           | 180                           |
|                                                                          | Single-Sided Composite        |                           | 240                           | 230                           | 220                           |
| Roll Area, ft <sup>2</sup>                                               | Double-Sided Composite        |                           | 3,150                         | 3,000                         | 2,700                         |
|                                                                          | Single-Sided Composite        |                           | 3,600                         | 3,450                         | 3,300                         |

[Product specifications continued on back]

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## PRODUCT DATA SHEET



AT THE CORE:

A high load geocomposite with a creep-resistant structure that ensures continuous flow performance and is ideal for extremely high compressive stress applications.

## Product Specifications [continued]

Figure 2

- Roll resistance: Roll resistance value measured at stress = 15 000 psi gradient = 0.1 (mm/s) 5 minutes, boundary conditions = between plates, contact SSF for program time 0.001 s, 1.5 s after time 0.001 s.
- All geometries produced are nominal average roll values except ACS, which is a maximum average roll value, and DV resistance which is a typical value
- Roll widths and lengths have a tolerance of 1%
- Modified

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[illegible]

# GSE PermaNet UL Geocomposite

GSE PermaNet UL (Ultra Load) geocomposite is manufactured with a GSE PermaNet UL geonet heat-bonded on one or both sides with a GSE nonwoven needle-punched geotextile. The geotextile is available in mass per unit area range of 6 oz/yd<sup>2</sup> to 16 oz/yd<sup>2</sup>. The creep resistant structure of this product ensures continuous flow performance over a broad range of conditions and long durations. The geocomposite works as an efficient drainage medium and is ideal for extremely high compressive stress applications.

[\*]

## AT THE CORE:

A very high compressive strength geocomposite with a creep-resistant structure that ensures continuous flow performance over a broad range of conditions and long durations.

## Product Specifications

| Test Property                                                      | Test Method                      | Frequency                 | Minimum Average Roll Width    |                               |                               |
|--------------------------------------------------------------------|----------------------------------|---------------------------|-------------------------------|-------------------------------|-------------------------------|
| Geocomposite                                                       |                                  |                           | 6 oz/yd <sup>2</sup>          | 8 oz/yd <sup>2</sup>          | 10 oz/yd <sup>2</sup>         |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>2</sup> /sec)   | ASTM D 4716                      | 1/540,000 ft <sup>2</sup> | 4.8 (1 x 10 <sup>-4</sup> )   | 4.8 (1 x 10 <sup>-4</sup> )   | 4.8 (1 x 10 <sup>-4</sup> )   |
| Double-Sided Composite                                             |                                  |                           | 6.2 (1.3 x 10 <sup>-3</sup> ) | 6.2 (1.3 x 10 <sup>-3</sup> ) | 6.2 (1.3 x 10 <sup>-3</sup> ) |
| Single-Sided Composite                                             |                                  |                           |                               |                               |                               |
| Ply Adhesion, lb/in                                                | ASTM D 7005                      | 1/50,000 ft <sup>2</sup>  | 1.0                           | 1.0                           | 1.0                           |
| Geonet Core - GSE PermaNet UL (prior to lamination) <sup>(2)</sup> |                                  |                           |                               |                               |                               |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>2</sup> /sec)   | ASTM D 4716                      |                           | 24 (5 x 10 <sup>-3</sup> )    | 24 (5 x 10 <sup>-3</sup> )    | 24 (5 x 10 <sup>-3</sup> )    |
| Compression Strength, lb/ft <sup>2</sup>                           | ASTM D 6364                      | 1/540,000 ft <sup>2</sup> | 40,000                        | 40,000                        | 40,000                        |
| Creep Reduction Factor                                             | ASTM D 7406/7361                 | per formulation           | 1.3 ± 20,000 psf              | 1.3 ± 20,000 psf              | 1.3 ± 20,000 psf              |
| Density, g/cm <sup>3</sup>                                         | ASTM D 1505                      | 1/50,000 ft <sup>2</sup>  | 0.94                          | 0.94                          | 0.94                          |
| Tensile Strength (MD), lb/in                                       | ASTM D 5035/7179                 | 1/50,000 ft <sup>2</sup>  | 100                           | 100                           | 100                           |
| Carbon Black Content, %                                            | ASTM D 1603 <sup>(3)</sup> /4218 | 1/50,000 ft <sup>2</sup>  | 2.0                           | 2.0                           | 2.0                           |
| Geotextile (prior to lamination) <sup>(2)</sup>                    |                                  |                           |                               |                               |                               |
| Mass per Unit Area, oz/yd <sup>2</sup>                             | ASTM D 5261                      | 1/90,000 ft <sup>2</sup>  | 6                             | 8                             | 10                            |
| Grab Tensile, lb                                                   | ASTM D 4632                      | 1/90,000 ft <sup>2</sup>  | 160                           | 220                           | 260                           |
| Puncture Strength, lb                                              | ASTM D 4833                      | 1/90,000 ft <sup>2</sup>  | 90                            | 120                           | 165                           |
| AOS, US Sieve (mm)                                                 | ASTM D 4751                      | 1/540,000 ft <sup>2</sup> | 70                            | 80                            | 100                           |
| Permittivity, sec <sup>-1</sup>                                    | ASTM D 4491                      | 1/540,000 ft <sup>2</sup> | 1.5                           | 1.3                           | 1.0                           |
| Flow Rate, gpm/ft <sup>2</sup>                                     | ASTM D 4491                      | 1/540,000 ft <sup>2</sup> | 110                           | 95                            | 75                            |
| UV Resistance, % Retained                                          | ASTM D 4355 (after 500 hours)    | per formulation           | 70                            | 70                            | 70                            |
| NOMINAL ROLL DIMENSIONS                                            |                                  |                           |                               |                               |                               |
| Geonet Core Thickness, mil                                         | ASTM D 5199                      | 1/50,000 ft <sup>2</sup>  | 300                           | 300                           | 300                           |
| Roll Width <sup>(4)</sup> , ft                                     |                                  |                           | 15                            | 15                            | 15                            |
| Roll Length <sup>(5)</sup> , ft                                    | Double-Sided Composite           |                           | 190                           | 180                           | 150                           |
|                                                                    | Single-Sided Composite           |                           | 200                           | 200                           | 190                           |
| Roll Area, ft <sup>2</sup>                                         | Double-Sided Composite           |                           | 2,850                         | 2,700                         | 2,250                         |
|                                                                    | Single-Sided Composite           |                           | 3,000                         | 3,000                         | 2,850                         |

[Product specifications continued on back]

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## PRODUCT DATA SHEET

[\*]

### AT THE CORE:

A very high compressive strength geocomposite with a creep-resistant structure that ensures continuous flow performance over a broad range of conditions and long durations.

### Product Specifications [continued]

#### NOTES

- This is an index transmissivity value measured at a slope of 25,000 m/s gradient. (1:1 slope) for geotextiles, boundary conditions between plates. Contact GSE for performance transmissivity value for use in design.
- All geotextile properties are minimum average roll values except AOS (mm) which is a maximum average roll value and UV resistance which is a typical value.
- Roll widths and lengths have a tolerance of 4mm.
- No deflection.

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# GSE FabriNet TRx Geocomposite

GSE HyperNet TRx geonet is produced with a unique one step process that coextrudes creep resistant columns to an intrusion resistant roof. The resulting triaxial geonet is then laminated to a nonwoven geotextile filtration media. This product achieves high in-situ transmissivity from optimally oriented flow channels that maintain porosity because of the intrusion and creep resistant nature of the triaxial structure. The geocomposite provides continuous performance over a broad range of conditions. It is well suited for use in surface water collection and removal systems, gas venting, and landfill drainage applications.

[\*]

## AT THE CORE:

A high flow geocomposite that achieves high in-situ transmissivity from optimally oriented flow channels that maintain porosity.

## Product Specifications

| Tested Property                                                           | Test Method                   | Frequency                 | Minimum Average Roll Value     |                                |                                |
|---------------------------------------------------------------------------|-------------------------------|---------------------------|--------------------------------|--------------------------------|--------------------------------|
| <b>Geocomposite</b>                                                       |                               |                           | 4 oz/yd <sup>2</sup>           | 6 oz/yd <sup>2</sup>           | 8 oz/yd <sup>2</sup>           |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>3</sup> /sec)          | ASTM D 4716                   | 1/540,000 ft <sup>2</sup> | 12.1 (2.5 x 10 <sup>-3</sup> ) | 12.1 (2.5 x 10 <sup>-3</sup> ) | 10.1 (2.2 x 10 <sup>-3</sup> ) |
| Double-Sided Composite                                                    |                               |                           | 15.7 (3.2 x 10 <sup>-3</sup> ) | 15.7 (3.2 x 10 <sup>-3</sup> ) | 13.8 (2.9 x 10 <sup>-3</sup> ) |
| Ply Adhesion, lb/in                                                       | ASTM D 7005                   | 1/50,000 ft <sup>2</sup>  | 1.0                            | 1.0                            | 1.0                            |
| <b>Geonet Core - GSE HyperNet TRx (prior to lamination)<sup>(2)</sup></b> |                               |                           |                                |                                |                                |
| Transmissivity <sup>(1)</sup> , gal/min/ft (m <sup>3</sup> /sec)          | ASTM D 4716                   |                           | 43.5 (9 x 10 <sup>-3</sup> )   | 43.5 (9 x 10 <sup>-3</sup> )   | 43.5 (9 x 10 <sup>-3</sup> )   |
| Density, g/cm <sup>3</sup>                                                | ASTM D 1505                   | 1/50,000 ft <sup>2</sup>  | 0.94                           | 0.94                           | 0.94                           |
| Tensile Strength <sup>(2)</sup> , lb/in                                   | ASTM D 5035/7179              | 1/50,000 ft <sup>2</sup>  | 75                             | 75                             | 75                             |
| Carbon Black Content, %                                                   | ASTM D 1603 1/4218            | 1/50,000 ft <sup>2</sup>  | 2.0                            | 2.0                            | 2.0                            |
| <b>Geotextile (prior to lamination)<sup>(3)</sup></b>                     |                               |                           |                                |                                |                                |
| Mass per Unit Area, oz/yd <sup>2</sup>                                    | ASTM D 5261                   | 1/90,000 ft <sup>2</sup>  | 4                              | 6                              | 8                              |
| Grab Tensile, lb                                                          | ASTM D 4632                   | 1/90,000 ft <sup>2</sup>  | 120                            | 160                            | 220                            |
| Puncture Strength, lb                                                     | ASTM D 4833                   | 1/90,000 ft <sup>2</sup>  | 60                             | 90                             | 120                            |
| AOS, US sieve (mm)                                                        | ASTM D 4751                   | 1/540,000 ft <sup>2</sup> | 70 (0.212)                     | 70 (0.212)                     | 80 (0.180)                     |
| Permittivity, sec <sup>(4)</sup>                                          | ASTM D 4491                   | 1/540,000 ft <sup>2</sup> | 1.8                            | 1.5                            | 1.3                            |
| Flow Rate, gpm/ft <sup>2</sup>                                            | ASTM D 4491                   | 1/540,000 ft <sup>2</sup> | 135                            | 110                            | 95                             |
| UV Resistance, % retained                                                 | ASTM D 4355 (after 500 hours) | per formulation           | 70                             | 70                             | 70                             |
| <b>NOMINAL ROLL DIMENSIONS</b>                                            |                               |                           |                                |                                |                                |
| Geonet Core Thickness, mil                                                | ASTM D 5199                   | 1/50,000 ft <sup>2</sup>  | 300                            | 300                            | 300                            |
| Roll Width <sup>(5)</sup> , ft                                            |                               |                           | 15                             | 15                             | 15                             |
| Roll Length <sup>(6)</sup> , ft                                           | Double-Sided Composite        |                           | 160                            | 160                            | 150                            |
|                                                                           | Single-Sided Composite        |                           | 180                            | 170                            | 170                            |
| Roll Area, ft <sup>2</sup>                                                | Double-Sided Composite        |                           | 2,400                          | 2,400                          | 2,250                          |
|                                                                           | Single-Sided Composite        |                           | 2,700                          | 2,550                          | 2,550                          |

[Product specifications continued on back]

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## PRODUCT DATA SHEET



### AT THE CORE:

A high flow geocomposite that achieves high in-situ transmissivity from optimally oriented flow channels that maintain porosity.

### Product Specifications [continued]

#### Options:

- Permeability: higher than 1000 ft<sup>2</sup>/day (measured at 1000 psi gradient) or 0.1 ft<sup>2</sup>/day or 10 ft<sup>2</sup>/day (at boundary conditions) or 1 Between plates, contact GSE for performance and transmissivity data for your application.
- Tested in machine direction (MD).
- All properties are minimum average roll values except 4.0 ft<sup>2</sup>/day, which is a maximum average roll value and 20 ft<sup>2</sup>/day is a typical value.
- Roll widths and length have a tolerance of ±3%.
- Modified.

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## **Appendix O-2**

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*****
*****
**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\IAM1R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\IAM1R003.OUT

```

TIME: 18:23      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 30
THICKNESS           =      84.00  INCHES
POROSITY             =      0.5410 VOL/VOL
FIELD CAPACITY       =      0.1870 VOL/VOL
WILTING POINT       =      0.0470 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1935 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.499999987000E-04 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0513             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 3

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 12.00          | INCHES  |
| POROSITY                   | = | 0.3970         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0320         | VOL/VOL |
| WILTING POINT              | = | 0.0130         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0322         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.250000000000 | CM/SEC  |
| SLOPE                      | = | 1.00           | PERCENT |
| DRAINAGE LENGTH            | = | 541.0          | FEET    |

LAYER 4

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

# LAYER 5

-----

## TYPE 3 - BARRIER SOIL LINER MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

## GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #30 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 1.% AND  
A SLOPE LENGTH OF 541. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 96.70  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 28.100 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 2.751  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.492  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 0.564  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 27.505 | INCHES      |
| TOTAL INITIAL WATER                | = | 27.505 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

## EVAPOTRANSPIRATION AND WEATHER DATA

-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |       |         |
|---------------------------------------|---|-------|---------|
| STATION LATITUDE                      | = | 38.70 | DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50  |         |
| START OF GROWING SEASON (JULIAN DATE) | = | 98    |         |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300   |         |
| EVAPORATIVE ZONE DEPTH                | = | 12.0  | INCHES  |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 | MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 | %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 | %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 | %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 | %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 7

|                 | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| -----           | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION   |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 1.71    | 2.08    | 3.24    | 3.42    | 3.42    | 5.13    |
|                 | 3.06    | 2.47    | 2.32    | 2.38    | 2.97    | 1.75    |
| STD. DEVIATIONS | 0.89    | 1.36    | 0.81    | 1.50    | 1.81    | 1.30    |
|                 | 1.58    | 1.66    | 1.35    | 1.37    | 1.62    | 1.07    |
| RUNOFF          |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 0.497   | 0.870   | 1.175   | 0.942   | 1.125   | 1.829   |
|                 | 1.003   | 0.656   | 0.709   | 0.709   | 1.119   | 0.290   |
| STD. DEVIATIONS | 0.245   | 0.749   | 0.885   | 0.695   | 1.168   | 0.610   |
|                 | 0.757   | 0.592   | 0.583   | 0.721   | 0.845   | 0.351   |

EVAPOTRANSPIRATION

|                 |       |       |       |       |       |       |
|-----------------|-------|-------|-------|-------|-------|-------|
| TOTALS          | 0.462 | 0.941 | 2.235 | 3.028 | 2.582 | 3.234 |
|                 | 2.493 | 1.993 | 1.446 | 1.278 | 1.318 | 0.780 |
| STD. DEVIATIONS | 0.169 | 0.484 | 0.287 | 0.647 | 0.931 | 0.966 |
|                 | 0.645 | 0.994 | 0.901 | 0.536 | 0.214 | 0.214 |

LATERAL DRAINAGE COLLECTED FROM LAYER 3

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0850 | 0.0745 | 0.0800 | 0.0959 | 0.1163 | 0.0949 |
|                 | 0.0621 | 0.0318 | 0.0310 | 0.0575 | 0.0759 | 0.0920 |
| STD. DEVIATIONS | 0.0801 | 0.0690 | 0.0768 | 0.0839 | 0.0793 | 0.0517 |
|                 | 0.0357 | 0.0257 | 0.0182 | 0.0510 | 0.0689 | 0.0740 |

PERCOLATION/LEAKAGE THROUGH LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.1046 | 0.1005 | 0.0985 | 0.1221 | 0.1432 | 0.1207 |
|                 | 0.0765 | 0.0391 | 0.0395 | 0.0708 | 0.0966 | 0.1133 |
| STD. DEVIATIONS | 0.0986 | 0.0926 | 0.0946 | 0.1067 | 0.0977 | 0.0658 |
|                 | 0.0440 | 0.0316 | 0.0232 | 0.0628 | 0.0876 | 0.0911 |

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 7

|                                            | INCHES  |            | CU. FEET   | PERCENT |
|--------------------------------------------|---------|------------|------------|---------|
| PRECIPITATION                              | 33.95   | ( 3.610)   | 3463147.5  | 100.00  |
| RUNOFF                                     | 10.923  | ( 2.5198)  | 1114135.75 | 32.171  |
| EVAPOTRANSPIRATION                         | 21.792  | ( 2.0850)  | 2222852.00 | 64.186  |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 3 | 0.89692 | ( 0.59928) | 91488.367  | 2.64177 |

|                                        |                    |       |         |
|----------------------------------------|--------------------|-------|---------|
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 5 | 0.00008 ( 0.00005) | 8.339 | 0.00024 |
|----------------------------------------|--------------------|-------|---------|

|                                   |                |
|-----------------------------------|----------------|
| AVERAGE HEAD ON TOP<br>OF LAYER 4 | 0.094 ( 0.063) |
|-----------------------------------|----------------|

|                         |                 |          |       |
|-------------------------|-----------------|----------|-------|
| CHANGE IN WATER STORAGE | 0.340 ( 1.3845) | 34663.22 | 1.001 |
|-------------------------|-----------------|----------|-------|

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| PEAK DAILY VALUES FOR YEARS                                  | 1 THROUGH | 7           |
|--------------------------------------------------------------|-----------|-------------|
|                                                              | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                | 2.60      | 265207.781  |
| RUNOFF                                                       | 1.896     | 193392.5780 |
| DRAINAGE COLLECTED FROM LAYER 3                              | 0.00731   | 745.62543   |
| PERCOLATION/LEAKAGE THROUGH LAYER 5                          | 0.000001  | 0.06296     |
| AVERAGE HEAD ON TOP OF LAYER 4                               | 0.279     |             |
| MAXIMUM HEAD ON TOP OF LAYER 4                               | 0.540     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 3<br>(DISTANCE FROM DRAIN) | 17.6 FEET |             |
| SNOW WATER                                                   | 1.38      | 140819.5620 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            | 0.3792    |             |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            | 0.0470    |             |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 7

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 18.3273  | 0.2182    |
| 2          | 0.8886   | 0.0741    |
| 3          | 0.4199   | 0.0350    |
| 4          | 0.0000   | 0.0000    |
| 5          | 10.2480  | 0.4270    |
| SNOW WATER | 0.000    |           |

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## **Appendix O-3**

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**
**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE          **
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)              **
**          DEVELOPED BY ENVIRONMENTAL LABORATORY                   **
**          USAE WATERWAYS EXPERIMENT STATION                      **
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY         **
**
**
*****
*****

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```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\IAM3R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\IAM3R003.OUT

```

TIME: 18:36      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

          TYPE 1 - VERTICAL PERCOLATION LAYER
          MATERIAL TEXTURE NUMBER 30
THICKNESS           =      84.00  INCHES
POROSITY             =      0.5410 VOL/VOL
FIELD CAPACITY       =      0.1870 VOL/VOL
WILTING POINT       =      0.0470 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1945 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.499999987000E-04 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0498             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 3

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 12.00          | INCHES  |
| POROSITY                   | = | 0.3970         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0320         | VOL/VOL |
| WILTING POINT              | = | 0.0130         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0322         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.250000000000 | CM/SEC  |
| SLOPE                      | = | 1.00           | PERCENT |
| DRAINAGE LENGTH            | = | 725.0          | FEET    |

LAYER 4

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

LAYER 5

-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #30 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 1.% AND  
A SLOPE LENGTH OF 725. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 96.60  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 31.400 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 2.864  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.492  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 0.564  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 27.572 | INCHES      |
| TOTAL INITIAL WATER                | = | 27.572 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

EVAPOTRANSPIRATION AND WEATHER DATA

-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |       |         |
|---------------------------------------|---|-------|---------|
| STATION LATITUDE                      | = | 38.70 | DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50  |         |
| START OF GROWING SEASON (JULIAN DATE) | = | 98    |         |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300   |         |
| EVAPORATIVE ZONE DEPTH                | = | 12.0  | INCHES  |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 | MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 | %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 | %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 | %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 | %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 7

|                 | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| -----           | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION   |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 1.71    | 2.08    | 3.24    | 3.42    | 3.42    | 5.13    |
|                 | 3.06    | 2.47    | 2.32    | 2.38    | 2.97    | 1.75    |
| STD. DEVIATIONS | 0.89    | 1.36    | 0.81    | 1.50    | 1.81    | 1.30    |
|                 | 1.58    | 1.66    | 1.35    | 1.37    | 1.62    | 1.07    |
| RUNOFF          |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 0.495   | 0.864   | 1.152   | 0.915   | 1.095   | 1.790   |
|                 | 0.968   | 0.641   | 0.689   | 0.706   | 1.099   | 0.283   |
| STD. DEVIATIONS | 0.241   | 0.742   | 0.889   | 0.683   | 1.148   | 0.601   |
|                 | 0.729   | 0.577   | 0.572   | 0.739   | 0.831   | 0.342   |

EVAPOTRANSPIRATION

|                 |       |       |       |       |       |       |
|-----------------|-------|-------|-------|-------|-------|-------|
| TOTALS          | 0.465 | 0.954 | 2.257 | 3.008 | 2.619 | 3.299 |
|                 | 2.410 | 2.152 | 1.455 | 1.242 | 1.312 | 0.784 |
| STD. DEVIATIONS | 0.171 | 0.495 | 0.292 | 0.675 | 1.015 | 0.980 |
|                 | 0.814 | 1.029 | 0.930 | 0.508 | 0.268 | 0.209 |

LATERAL DRAINAGE COLLECTED FROM LAYER 3

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0910 | 0.0802 | 0.0855 | 0.1013 | 0.1152 | 0.0928 |
|                 | 0.0644 | 0.0345 | 0.0358 | 0.0665 | 0.0848 | 0.1003 |
| STD. DEVIATIONS | 0.0845 | 0.0751 | 0.0805 | 0.0853 | 0.0843 | 0.0607 |
|                 | 0.0376 | 0.0249 | 0.0165 | 0.0593 | 0.0744 | 0.0785 |

PERCOLATION/LEAKAGE THROUGH LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.1501 | 0.1449 | 0.1411 | 0.1728 | 0.1901 | 0.1583 |
|                 | 0.1063 | 0.0570 | 0.0611 | 0.1097 | 0.1445 | 0.1655 |
| STD. DEVIATIONS | 0.1394 | 0.1353 | 0.1328 | 0.1454 | 0.1391 | 0.1034 |
|                 | 0.0620 | 0.0411 | 0.0282 | 0.0978 | 0.1268 | 0.1296 |

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 7

|                                            | INCHES  |            | CU. FEET   | PERCENT |
|--------------------------------------------|---------|------------|------------|---------|
| PRECIPITATION                              | 33.95   | ( 3.610)   | 3869851.5  | 100.00  |
| RUNOFF                                     | 10.697  | ( 2.5448)  | 1219280.12 | 31.507  |
| EVAPOTRANSPIRATION                         | 21.957  | ( 2.0606)  | 2502747.50 | 64.673  |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 3 | 0.95219 | ( 0.63655) | 108532.078 | 2.80455 |

|                                        |                    |        |         |
|----------------------------------------|--------------------|--------|---------|
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 5 | 0.00011 ( 0.00007) | 12.764 | 0.00033 |
|----------------------------------------|--------------------|--------|---------|

|                                   |                |
|-----------------------------------|----------------|
| AVERAGE HEAD ON TOP<br>OF LAYER 4 | 0.133 ( 0.089) |
|-----------------------------------|----------------|

|                         |                 |          |       |
|-------------------------|-----------------|----------|-------|
| CHANGE IN WATER STORAGE | 0.345 ( 1.3618) | 39279.45 | 1.015 |
|-------------------------|-----------------|----------|-------|

\*\*\*\*\*

\*\*\*\*\*

| PEAK DAILY VALUES FOR YEARS                                  | 1 THROUGH | 7           |
|--------------------------------------------------------------|-----------|-------------|
|                                                              | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                | 2.60      | 296353.187  |
| RUNOFF                                                       | 1.874     | 213547.0620 |
| DRAINAGE COLLECTED FROM LAYER 3                              | 0.00712   | 811.63214   |
| PERCOLATION/LEAKAGE THROUGH LAYER 5                          | 0.000001  | 0.08958     |
| AVERAGE HEAD ON TOP OF LAYER 4                               | 0.364     |             |
| MAXIMUM HEAD ON TOP OF LAYER 4                               | 0.705     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 3<br>(DISTANCE FROM DRAIN) | 23.2 FEET |             |
| SNOW WATER                                                   | 1.38      | 157357.0940 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            | 0.3778    |             |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            | 0.0470    |             |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 7

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 18.3947  | 0.2190    |
| 2          | 0.9023   | 0.0752    |
| 3          | 0.4397   | 0.0366    |
| 4          | 0.0000   | 0.0000    |
| 5          | 10.2480  | 0.4270    |
| SNOW WATER | 0.000    |           |

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## Appendix O-4

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*****
**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\IGE1R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\IGE1R003.OUT

```

TIME: 15:22      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 30
THICKNESS           =      84.00  INCHES
POROSITY             =      0.5410 VOL/VOL
FIELD CAPACITY       =      0.1870 VOL/VOL
WILTING POINT        =      0.0470 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1935 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.499999987000E-04 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0513             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 3

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 0.69           | INCHES  |
| POROSITY                   | = | 0.8500         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0100         | VOL/VOL |
| WILTING POINT              | = | 0.0050         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0114         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 1.299999995000 | CM/SEC  |
| SLOPE                      | = | 1.00           | PERCENT |
| DRAINAGE LENGTH            | = | 541.0          | FEET    |

LAYER 4

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

# LAYER 5

-----

## TYPE 3 - BARRIER SOIL LINER MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

## GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #30 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 1.% AND  
A SLOPE LENGTH OF 541. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 96.70  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 28.100 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 2.751  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.492  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 0.564  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 27.127 | INCHES      |
| TOTAL INITIAL WATER                | = | 27.127 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

## EVAPOTRANSPIRATION AND WEATHER DATA

-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |       |         |
|---------------------------------------|---|-------|---------|
| STATION LATITUDE                      | = | 38.70 | DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50  |         |
| START OF GROWING SEASON (JULIAN DATE) | = | 98    |         |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300   |         |
| EVAPORATIVE ZONE DEPTH                | = | 12.0  | INCHES  |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 | MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 | %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 | %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 | %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 | %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 7

|                 | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
|                 | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION   |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 1.71    | 2.08    | 3.24    | 3.42    | 3.42    | 5.13    |
|                 | 3.06    | 2.47    | 2.32    | 2.38    | 2.97    | 1.75    |
| STD. DEVIATIONS | 0.89    | 1.36    | 0.81    | 1.50    | 1.81    | 1.30    |
|                 | 1.58    | 1.66    | 1.35    | 1.37    | 1.62    | 1.07    |
| RUNOFF          |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 0.497   | 0.870   | 1.175   | 0.942   | 1.125   | 1.829   |
|                 | 1.003   | 0.656   | 0.709   | 0.709   | 1.119   | 0.290   |
| STD. DEVIATIONS | 0.245   | 0.749   | 0.885   | 0.695   | 1.168   | 0.610   |
|                 | 0.757   | 0.592   | 0.583   | 0.721   | 0.845   | 0.351   |

EVAPOTRANSPIRATION

|                 |       |       |       |       |       |       |
|-----------------|-------|-------|-------|-------|-------|-------|
| TOTALS          | 0.462 | 0.941 | 2.235 | 3.028 | 2.582 | 3.234 |
|                 | 2.493 | 1.993 | 1.446 | 1.278 | 1.318 | 0.780 |
| STD. DEVIATIONS | 0.169 | 0.484 | 0.287 | 0.647 | 0.931 | 0.966 |
|                 | 0.645 | 0.994 | 0.901 | 0.536 | 0.214 | 0.214 |

LATERAL DRAINAGE COLLECTED FROM LAYER 3

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0846 | 0.0737 | 0.0799 | 0.1030 | 0.1179 | 0.0878 |
|                 | 0.0533 | 0.0256 | 0.0338 | 0.0642 | 0.0804 | 0.0953 |
| STD. DEVIATIONS | 0.0789 | 0.0691 | 0.0769 | 0.0874 | 0.0751 | 0.0459 |
|                 | 0.0333 | 0.0234 | 0.0220 | 0.0612 | 0.0717 | 0.0749 |

PERCOLATION/LEAKAGE THROUGH LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.0200 | 0.0191 | 0.0189 | 0.0252 | 0.0279 | 0.0215 |
|                 | 0.0126 | 0.0061 | 0.0083 | 0.0152 | 0.0197 | 0.0226 |
| STD. DEVIATIONS | 0.0187 | 0.0178 | 0.0182 | 0.0214 | 0.0178 | 0.0112 |
|                 | 0.0079 | 0.0056 | 0.0054 | 0.0145 | 0.0175 | 0.0177 |

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 7

|                                         | INCHES  |            | CU. FEET   | PERCENT |
|-----------------------------------------|---------|------------|------------|---------|
| PRECIPITATION                           | 33.95   | ( 3.610)   | 3463147.5  | 100.00  |
| RUNOFF                                  | 10.923  | ( 2.5198)  | 1114135.75 | 32.171  |
| EVAPOTRANSPIRATION                      | 21.792  | ( 2.0850)  | 2222852.00 | 64.186  |
| LATERAL DRAINAGE COLLECTED FROM LAYER 3 | 0.89941 | ( 0.59344) | 91742.234  | 2.64910 |

|                                        |                    |          |         |
|----------------------------------------|--------------------|----------|---------|
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 5 | 0.00002 ( 0.00001) | 2.038    | 0.00006 |
| AVERAGE HEAD ON TOP<br>OF LAYER 4      | 0.018 ( 0.012)     |          |         |
| CHANGE IN WATER STORAGE                | 0.337 ( 1.3648)    | 34415.69 | 0.994   |

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| PEAK DAILY VALUES FOR YEARS                                  | 1 THROUGH | 7           |
|--------------------------------------------------------------|-----------|-------------|
|                                                              | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                | 2.60      | 265207.781  |
| RUNOFF                                                       | 1.896     | 193392.5780 |
| DRAINAGE COLLECTED FROM LAYER 3                              | 0.00787   | 802.88251   |
| PERCOLATION/LEAKAGE THROUGH LAYER 5                          | 0.000000  | 0.01516     |
| AVERAGE HEAD ON TOP OF LAYER 4                               | 0.058     |             |
| MAXIMUM HEAD ON TOP OF LAYER 4                               | 0.114     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 3<br>(DISTANCE FROM DRAIN) | 5.0 FEET  |             |
| SNOW WATER                                                   | 1.38      | 140819.5620 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.3792      |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.0470      |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 7

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 18.3273  | 0.2182    |
| 2          | 0.8886   | 0.0741    |
| 3          | 0.0246   | 0.0357    |
| 4          | 0.0000   | 0.0000    |
| 5          | 10.2480  | 0.4270    |
| SNOW WATER | 0.000    |           |

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## **Appendix O-5**

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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
**
**
*****
*****

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```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\IGE2R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\IGE2R003.OUT

```

TIME: 18: 4      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 30
THICKNESS           = 42.00 INCHES
POROSITY             = 0.5410 VOL/VOL
FIELD CAPACITY       = 0.1870 VOL/VOL
WILTING POINT       = 0.0470 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2199 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.499999987000E-04 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

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LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0528             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 3

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 0.69           | INCHES  |
| POROSITY                   | = | 0.8500         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0100         | VOL/VOL |
| WILTING POINT              | = | 0.0050         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0100         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 1.299999995000 | CM/SEC  |
| SLOPE                      | = | 33.33          | PERCENT |
| DRAINAGE LENGTH            | = | 60.0           | FEET    |

LAYER 4

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

# LAYER 5

-----

## TYPE 3 - BARRIER SOIL LINER MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

## GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #30 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 1.% AND  
A SLOPE LENGTH OF 60. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 97.00  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 3.300  | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 2.962  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.492  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 0.564  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 20.124 | INCHES      |
| TOTAL INITIAL WATER                | = | 20.124 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

## EVAPOTRANSPIRATION AND WEATHER DATA

-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |       |         |
|---------------------------------------|---|-------|---------|
| STATION LATITUDE                      | = | 38.70 | DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50  |         |
| START OF GROWING SEASON (JULIAN DATE) | = | 98    |         |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300   |         |
| EVAPORATIVE ZONE DEPTH                | = | 12.0  | INCHES  |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 | MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 | %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 | %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 | %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 | %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 7

|                 | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| -----           | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION   |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 1.71    | 2.08    | 3.24    | 3.42    | 3.42    | 5.13    |
|                 | 3.06    | 2.47    | 2.32    | 2.38    | 2.97    | 1.75    |
| STD. DEVIATIONS | 0.89    | 1.36    | 0.81    | 1.50    | 1.81    | 1.30    |
|                 | 1.58    | 1.66    | 1.35    | 1.37    | 1.62    | 1.07    |
| RUNOFF          |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 0.507   | 0.889   | 1.245   | 1.036   | 1.208   | 1.986   |
|                 | 1.093   | 0.720   | 0.766   | 0.767   | 1.194   | 0.312   |
| STD. DEVIATIONS | 0.257   | 0.773   | 0.878   | 0.747   | 1.195   | 0.629   |
|                 | 0.809   | 0.634   | 0.624   | 0.759   | 0.881   | 0.379   |

EVAPOTRANSPIRATION

|                 |       |       |       |       |       |       |
|-----------------|-------|-------|-------|-------|-------|-------|
| TOTALS          | 0.462 | 0.938 | 2.218 | 2.882 | 2.536 | 3.000 |
|                 | 2.134 | 1.840 | 1.360 | 1.107 | 1.207 | 0.759 |
| STD. DEVIATIONS | 0.168 | 0.481 | 0.305 | 0.650 | 0.941 | 0.921 |
|                 | 0.606 | 0.836 | 0.814 | 0.498 | 0.251 | 0.207 |

LATERAL DRAINAGE COLLECTED FROM LAYER 3

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.1049 | 0.1204 | 0.1589 | 0.1257 | 0.1343 | 0.1955 |
|                 | 0.2012 | 0.1718 | 0.1394 | 0.1282 | 0.1346 | 0.1299 |
| STD. DEVIATIONS | 0.0509 | 0.0786 | 0.0829 | 0.0604 | 0.1909 | 0.1581 |
|                 | 0.0932 | 0.0726 | 0.0467 | 0.0489 | 0.0539 | 0.0408 |

PERCOLATION/LEAKAGE THROUGH LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.0002 | 0.0002 | 0.0003 | 0.0002 | 0.0002 | 0.0003 |
|                 | 0.0003 | 0.0003 | 0.0002 | 0.0002 | 0.0002 | 0.0002 |
| STD. DEVIATIONS | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0003 | 0.0003 |
|                 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 |

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 7

|                                         | INCHES  |            | CU. FEET  | PERCENT |
|-----------------------------------------|---------|------------|-----------|---------|
| PRECIPITATION                           | 33.95   | ( 3.610)   | 406704.2  | 100.00  |
| RUNOFF                                  | 11.722  | ( 2.5523)  | 140417.73 | 34.526  |
| EVAPOTRANSPIRATION                      | 20.443  | ( 1.9893)  | 244887.45 | 60.213  |
| LATERAL DRAINAGE COLLECTED FROM LAYER 3 | 1.74498 | ( 0.72759) | 20903.158 | 5.13965 |

|                                        |                    |        |         |
|----------------------------------------|--------------------|--------|---------|
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 5 | 0.00000 ( 0.00000) | 0.013  | 0.00000 |
| AVERAGE HEAD ON TOP<br>OF LAYER 4      | 0.000 ( 0.000)     |        |         |
| CHANGE IN WATER STORAGE                | 0.041 ( 1.0396)    | 495.82 | 0.122   |

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| PEAK DAILY VALUES FOR YEARS                                  | 1 THROUGH | 7          |
|--------------------------------------------------------------|-----------|------------|
|                                                              | (INCHES)  | (CU. FT.)  |
| PRECIPITATION                                                | 2.60      | 31145.398  |
| RUNOFF                                                       | 1.940     | 23245.0449 |
| DRAINAGE COLLECTED FROM LAYER 3                              | 0.02107   | 252.41109  |
| PERCOLATION/LEAKAGE THROUGH LAYER 5                          | 0.000000  | 0.00008    |
| AVERAGE HEAD ON TOP OF LAYER 4                               | 0.001     |            |
| MAXIMUM HEAD ON TOP OF LAYER 4                               | 0.012     |            |
| LOCATION OF MAXIMUM HEAD IN LAYER 3<br>(DISTANCE FROM DRAIN) | 0.0 FEET  |            |
| SNOW WATER                                                   | 1.38      | 16537.5293 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.3556     |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.0470     |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 7

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 9.2876   | 0.2211    |
| 2          | 0.8712   | 0.0726    |
| 3          | 0.0072   | 0.0105    |
| 4          | 0.0000   | 0.0000    |
| 5          | 10.2480  | 0.4270    |
| SNOW WATER | 0.000    |           |

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## Appendix O-6

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**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
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*****
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```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\IGE3R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\IGE3R003.OUT

```

TIME: 18:17      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 30

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 84.00              | INCHES  |
| POROSITY                   | = | 0.5410             | VOL/VOL |
| FIELD CAPACITY             | = | 0.1870             | VOL/VOL |
| WILTING POINT              | = | 0.0470             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.1945             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.499999987000E-04 | CM/SEC  |

NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0498             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 3

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |               |         |
|----------------------------|---|---------------|---------|
| THICKNESS                  | = | 0.69          | INCHES  |
| POROSITY                   | = | 0.8500        | VOL/VOL |
| FIELD CAPACITY             | = | 0.0100        | VOL/VOL |
| WILTING POINT              | = | 0.0050        | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0114        | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 1.29999995000 | CM/SEC  |
| SLOPE                      | = | 1.00          | PERCENT |
| DRAINAGE LENGTH            | = | 712.0         | FEET    |

LAYER 4

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

# LAYER 5

-----

## TYPE 3 - BARRIER SOIL LINER MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

## GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #30 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 1.% AND  
A SLOPE LENGTH OF 712. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 96.60  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 31.400 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 2.864  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.492  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 0.564  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 27.194 | INCHES      |
| TOTAL INITIAL WATER                | = | 27.194 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

## EVAPOTRANSPIRATION AND WEATHER DATA

-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |       |         |
|---------------------------------------|---|-------|---------|
| STATION LATITUDE                      | = | 38.70 | DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50  |         |
| START OF GROWING SEASON (JULIAN DATE) | = | 98    |         |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300   |         |
| EVAPORATIVE ZONE DEPTH                | = | 12.0  | INCHES  |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 | MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 | %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 | %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 | %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 | %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| -----   | -----   | -----   | -----   | -----   | -----   |
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 7

|                 | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| -----           | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION   |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 1.71    | 2.08    | 3.24    | 3.42    | 3.42    | 5.13    |
|                 | 3.06    | 2.47    | 2.32    | 2.38    | 2.97    | 1.75    |
| STD. DEVIATIONS | 0.89    | 1.36    | 0.81    | 1.50    | 1.81    | 1.30    |
|                 | 1.58    | 1.66    | 1.35    | 1.37    | 1.62    | 1.07    |
| RUNOFF          |         |         |         |         |         |         |
| -----           |         |         |         |         |         |         |
| TOTALS          | 0.495   | 0.864   | 1.152   | 0.915   | 1.095   | 1.790   |
|                 | 0.968   | 0.641   | 0.689   | 0.706   | 1.099   | 0.283   |
| STD. DEVIATIONS | 0.241   | 0.742   | 0.889   | 0.683   | 1.148   | 0.601   |
|                 | 0.729   | 0.577   | 0.572   | 0.739   | 0.831   | 0.342   |

EVAPOTRANSPIRATION

|                 |       |       |       |       |       |       |
|-----------------|-------|-------|-------|-------|-------|-------|
| TOTALS          | 0.465 | 0.954 | 2.257 | 3.008 | 2.619 | 3.299 |
|                 | 2.410 | 2.152 | 1.455 | 1.242 | 1.312 | 0.784 |
| STD. DEVIATIONS | 0.171 | 0.495 | 0.292 | 0.675 | 1.015 | 0.980 |
|                 | 0.814 | 1.029 | 0.930 | 0.508 | 0.268 | 0.209 |

LATERAL DRAINAGE COLLECTED FROM LAYER 3

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0897 | 0.0802 | 0.0843 | 0.1100 | 0.1162 | 0.0843 |
|                 | 0.0532 | 0.0260 | 0.0403 | 0.0764 | 0.0909 | 0.1046 |
| STD. DEVIATIONS | 0.0829 | 0.0754 | 0.0793 | 0.0900 | 0.0818 | 0.0528 |
|                 | 0.0332 | 0.0216 | 0.0263 | 0.0730 | 0.0782 | 0.0795 |

PERCOLATION/LEAKAGE THROUGH LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| TOTALS          | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|                 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.0279 | 0.0274 | 0.0263 | 0.0354 | 0.0362 | 0.0272 |
|                 | 0.0166 | 0.0081 | 0.0130 | 0.0238 | 0.0293 | 0.0326 |
| STD. DEVIATIONS | 0.0258 | 0.0256 | 0.0247 | 0.0290 | 0.0255 | 0.0170 |
|                 | 0.0104 | 0.0067 | 0.0085 | 0.0228 | 0.0252 | 0.0248 |

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 7

|                                            | INCHES  |            | CU. FEET   | PERCENT |
|--------------------------------------------|---------|------------|------------|---------|
| PRECIPITATION                              | 33.95   | ( 3.610)   | 3869851.5  | 100.00  |
| RUNOFF                                     | 10.697  | ( 2.5448)  | 1219280.12 | 31.507  |
| EVAPOTRANSPIRATION                         | 21.957  | ( 2.0606)  | 2502747.50 | 64.673  |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 3 | 0.95610 | ( 0.63050) | 108978.195 | 2.81608 |

PERCOLATION/LEAKAGE THROUGH      0.00003 ( 0.00002)      2.975      0.00008  
LAYER 5

AVERAGE HEAD ON TOP      0.025 ( 0.017)  
OF LAYER 4

CHANGE IN WATER STORAGE      0.341 ( 1.3369)      38843.12      1.004

\*\*\*\*\*

\*\*\*\*\*

| PEAK DAILY VALUES FOR YEARS                                  | 1 THROUGH | 7           |
|--------------------------------------------------------------|-----------|-------------|
|                                                              | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                | 2.60      | 296353.187  |
| RUNOFF                                                       | 1.874     | 213547.0620 |
| DRAINAGE COLLECTED FROM LAYER 3                              | 0.00777   | 886.12292   |
| PERCOLATION/LEAKAGE THROUGH LAYER 5                          | 0.000000  | 0.02144     |
| AVERAGE HEAD ON TOP OF LAYER 4                               | 0.075     |             |
| MAXIMUM HEAD ON TOP OF LAYER 4                               | 0.149     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 3<br>(DISTANCE FROM DRAIN) | 5.8 FEET  |             |
| SNOW WATER                                                   | 1.38      | 157357.0940 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.3778      |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.0470      |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 7

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 18.3947  | 0.2190    |
| 2          | 0.9023   | 0.0752    |
| 3          | 0.0346   | 0.0502    |
| 4          | 0.0000   | 0.0000    |
| 5          | 10.2480  | 0.4270    |
| SNOW WATER | 0.000    |           |

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## Appendix O-7

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*****
*****
**
**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE          **
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)              **
**          DEVELOPED BY ENVIRONMENTAL LABORATORY                   **
**          USAE WATERWAYS EXPERIMENT STATION                      **
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY        **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\OAM1R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\OAM1R003.OUT

```

TIME: 19:29      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

          TYPE 1 - VERTICAL PERCOLATION LAYER
          MATERIAL TEXTURE NUMBER 9
THICKNESS           =      12.00  INCHES
POROSITY             =      0.5010 VOL/VOL
FIELD CAPACITY       =      0.2840 VOL/VOL
WILTING POINT       =      0.1350 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.3062 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.190000006000E-03 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 30

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 240.00             | INCHES  |
| POROSITY                   | = | 0.5410             | VOL/VOL |
| FIELD CAPACITY             | = | 0.1870             | VOL/VOL |
| WILTING POINT              | = | 0.0470             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.1947             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.499999987000E-04 | CM/SEC  |

LAYER 3

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0455             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 4

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 12.00          | INCHES  |
| POROSITY                   | = | 0.3970         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0320         | VOL/VOL |
| WILTING POINT              | = | 0.0130         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0321         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.250000000000 | CM/SEC  |
| SLOPE                      | = | 1.00           | PERCENT |
| DRAINAGE LENGTH            | = | 541.0          | FEET    |

LAYER 5

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

LAYER 6

-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE # 9 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 2.% AND  
A SLOPE LENGTH OF 720. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 91.30  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 28.100 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 3.675  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.012  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.620  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 61.577 | INCHES      |
| TOTAL INITIAL WATER                | = | 61.577 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

# EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |               |
|---------------------------------------|---|---------------|
| STATION LATITUDE                      | = | 38.70 DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50          |
| START OF GROWING SEASON (JULIAN DATE) | = | 98            |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300           |
| EVAPORATIVE ZONE DEPTH                | = | 12.0 INCHES   |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 25

|                                                   | JAN/JUL          | FEB/AUG          | MAR/SEP          | APR/OCT          | MAY/NOV          | JUN/DEC          |
|---------------------------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| -----                                             | -----            | -----            | -----            | -----            | -----            | -----            |
| PRECIPITATION                                     |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| TOTALS                                            | 1.48<br>3.36     | 2.08<br>2.45     | 3.12<br>2.96     | 3.53<br>2.30     | 3.24<br>2.13     | 4.61<br>2.18     |
| STD. DEVIATIONS                                   | 0.86<br>1.90     | 1.11<br>1.28     | 0.97<br>1.45     | 1.36<br>1.31     | 1.58<br>1.49     | 2.13<br>1.09     |
| RUNOFF                                            |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| TOTALS                                            | 0.391<br>0.392   | 0.787<br>0.109   | 0.587<br>0.234   | 0.212<br>0.151   | 0.265<br>0.218   | 0.654<br>0.161   |
| STD. DEVIATIONS                                   | 0.452<br>0.548   | 0.654<br>0.144   | 0.824<br>0.217   | 0.222<br>0.199   | 0.351<br>0.266   | 0.754<br>0.215   |
| EVAPOTRANSPIRATION                                |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| TOTALS                                            | 0.569<br>3.079   | 0.697<br>2.410   | 2.472<br>2.233   | 3.494<br>1.795   | 2.909<br>1.364   | 3.987<br>0.859   |
| STD. DEVIATIONS                                   | 0.318<br>1.345   | 0.474<br>1.087   | 0.492<br>1.145   | 0.953<br>0.670   | 1.133<br>0.512   | 1.415<br>0.255   |
| LATERAL DRAINAGE COLLECTED FROM LAYER 4           |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| TOTALS                                            | 0.2985<br>0.1469 | 0.2211<br>0.2314 | 0.2083<br>0.2721 | 0.2099<br>0.3079 | 0.1671<br>0.3115 | 0.1134<br>0.3273 |
| STD. DEVIATIONS                                   | 0.1400<br>0.1329 | 0.1112<br>0.1607 | 0.1310<br>0.1621 | 0.1158<br>0.1665 | 0.0888<br>0.1407 | 0.0735<br>0.1348 |
| PERCOLATION/LEAKAGE THROUGH LAYER 6               |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| TOTALS                                            | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 |
| STD. DEVIATIONS                                   | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 | 0.0000<br>0.0000 |
| -----                                             |                  |                  |                  |                  |                  |                  |
| AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES) |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| DAILY AVERAGE HEAD ON TOP OF LAYER 5              |                  |                  |                  |                  |                  |                  |
| -----                                             |                  |                  |                  |                  |                  |                  |
| AVERAGES                                          | 0.3676<br>0.1808 | 0.2981<br>0.2850 | 0.2565<br>0.3462 | 0.2670<br>0.3792 | 0.2058<br>0.3963 | 0.1443<br>0.4030 |
| STD. DEVIATIONS                                   | 0.1725<br>0.1637 | 0.1487<br>0.1979 | 0.1613<br>0.2063 | 0.1474<br>0.2051 | 0.1093<br>0.1790 | 0.0935<br>0.1660 |

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| AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS |         |            |            | 1 THROUGH | 25       |
|-----------------------------------------------------|---------|------------|------------|-----------|----------|
|                                                     |         |            |            | INCHES    | CU. FEET |
|                                                     |         |            |            |           | PERCENT  |
| PRECIPITATION                                       | 33.44   | ( 4.389)   | 3411429.2  | 100.00    |          |
| RUNOFF                                              | 4.161   | ( 1.6271)  | 424391.19  | 12.440    |          |
| EVAPOTRANSPIRATION                                  | 25.868  | ( 3.1274)  | 2638658.00 | 77.348    |          |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 4          | 2.81529 | ( 1.21086) | 287167.750 | 8.41781   |          |
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 6              | 0.00023 | ( 0.00009) | 23.651     | 0.00069   |          |
| AVERAGE HEAD ON TOP<br>OF LAYER 5                   | 0.294   | ( 0.126)   |            |           |          |
| CHANGE IN WATER STORAGE                             | 0.600   | ( 2.1564)  | 61188.54   | 1.794     |          |

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| PEAK DAILY VALUES FOR YEARS                                  |  |  | 1 THROUGH | 25          |
|--------------------------------------------------------------|--|--|-----------|-------------|
|                                                              |  |  | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                |  |  | 3.44      | 350890.344  |
| RUNOFF                                                       |  |  | 1.975     | 201463.1090 |
| DRAINAGE COLLECTED FROM LAYER 4                              |  |  | 0.02019   | 2059.21289  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6                          |  |  | 0.000002  | 0.15823     |
| AVERAGE HEAD ON TOP OF LAYER 5                               |  |  | 0.771     |             |
| MAXIMUM HEAD ON TOP OF LAYER 5                               |  |  | 1.437     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 4<br>(DISTANCE FROM DRAIN) |  |  | 36.4 FEET |             |
| SNOW WATER                                                   |  |  | 2.22      | 225988.4530 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |  |  |           | 0.4152      |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |  |  |           | 0.1350      |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 25

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 2.6733   | 0.2228    |
| 2          | 61.7891  | 0.2575    |
| 3          | 1.0614   | 0.0885    |
| 4          | 0.6015   | 0.0501    |
| 5          | 0.0000   | 0.0000    |
| 6          | 10.2480  | 0.4270    |
| SNOW WATER | 0.201    |           |

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## **Appendix O-8**

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**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY               **
**      USAE WATERWAYS EXPERIMENT STATION                  **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY     **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\OAM3R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\OAM3R003.OUT

```

TIME: 11:18      DATE: 10/31/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

          TYPE 1 - VERTICAL PERCOLATION LAYER
          MATERIAL TEXTURE NUMBER 9
THICKNESS           =      12.00  INCHES
POROSITY             =      0.5010 VOL/VOL
FIELD CAPACITY       =      0.2840 VOL/VOL
WILTING POINT       =      0.1350 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.3062 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.190000006000E-03 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 30

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 240.00             | INCHES  |
| POROSITY                   | = | 0.5410             | VOL/VOL |
| FIELD CAPACITY             | = | 0.1870             | VOL/VOL |
| WILTING POINT              | = | 0.0470             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.1947             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.499999987000E-04 | CM/SEC  |

LAYER 3

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0455             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 4

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                |         |
|----------------------------|---|----------------|---------|
| THICKNESS                  | = | 12.00          | INCHES  |
| POROSITY                   | = | 0.3970         | VOL/VOL |
| FIELD CAPACITY             | = | 0.0320         | VOL/VOL |
| WILTING POINT              | = | 0.0130         | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0321         | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.250000000000 | CM/SEC  |
| SLOPE                      | = | 1.00           | PERCENT |
| DRAINAGE LENGTH            | = | 637.0          | FEET    |

LAYER 5

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

LAYER 6

-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE # 9 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 2.% AND  
A SLOPE LENGTH OF 720. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 91.30  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 31.400 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 3.675  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.012  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.620  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 61.577 | INCHES      |
| TOTAL INITIAL WATER                | = | 61.577 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

# EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |               |
|---------------------------------------|---|---------------|
| STATION LATITUDE                      | = | 38.70 DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50          |
| START OF GROWING SEASON (JULIAN DATE) | = | 98            |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300           |
| EVAPORATIVE ZONE DEPTH                | = | 12.0 INCHES   |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 25

|                                         | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------------------------------|---------|---------|---------|---------|---------|---------|
| -----                                   | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION                           |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 1.48    | 2.08    | 3.12    | 3.53    | 3.24    | 4.61    |
|                                         | 3.36    | 2.45    | 2.96    | 2.30    | 2.13    | 2.18    |
| STD. DEVIATIONS                         | 0.86    | 1.11    | 0.97    | 1.36    | 1.58    | 2.13    |
|                                         | 1.90    | 1.28    | 1.45    | 1.31    | 1.49    | 1.09    |
| RUNOFF                                  |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.391   | 0.787   | 0.587   | 0.212   | 0.265   | 0.654   |
|                                         | 0.392   | 0.109   | 0.234   | 0.151   | 0.218   | 0.161   |
| STD. DEVIATIONS                         | 0.452   | 0.654   | 0.824   | 0.222   | 0.351   | 0.754   |
|                                         | 0.548   | 0.144   | 0.217   | 0.199   | 0.266   | 0.215   |
| EVAPOTRANSPIRATION                      |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.569   | 0.697   | 2.472   | 3.494   | 2.909   | 3.987   |
|                                         | 3.079   | 2.410   | 2.233   | 1.795   | 1.364   | 0.859   |
| STD. DEVIATIONS                         | 0.318   | 0.474   | 0.492   | 0.953   | 1.133   | 1.415   |
|                                         | 1.345   | 1.087   | 1.145   | 0.670   | 0.512   | 0.255   |
| LATERAL DRAINAGE COLLECTED FROM LAYER 4 |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.2996  | 0.2250  | 0.2109  | 0.2098  | 0.1710  | 0.1167  |
|                                         | 0.1446  | 0.2252  | 0.2684  | 0.3054  | 0.3103  | 0.3268  |
| STD. DEVIATIONS                         | 0.1396  | 0.1117  | 0.1294  | 0.1155  | 0.0896  | 0.0728  |
|                                         | 0.1266  | 0.1571  | 0.1604  | 0.1663  | 0.1416  | 0.1353  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6     |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
| STD. DEVIATIONS                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |

-----

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

-----

DAILY AVERAGE HEAD ON TOP OF LAYER 5

|                 |        |        |        |        |        |        |
|-----------------|--------|--------|--------|--------|--------|--------|
| AVERAGES        | 0.4344 | 0.3571 | 0.3057 | 0.3144 | 0.2480 | 0.1748 |
|                 | 0.2096 | 0.3265 | 0.4022 | 0.4429 | 0.4649 | 0.4739 |
| STD. DEVIATIONS | 0.2025 | 0.1759 | 0.1877 | 0.1730 | 0.1299 | 0.1091 |
|                 | 0.1836 | 0.2278 | 0.2403 | 0.2411 | 0.2122 | 0.1962 |

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| AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS |         |            |            | 1 THROUGH | 25 |
|-----------------------------------------------------|---------|------------|------------|-----------|----|
|                                                     | INCHES  |            | CU. FEET   | PERCENT   |    |
| PRECIPITATION                                       | 33.44   | ( 4.389)   | 3812059.7  | 100.00    |    |
| RUNOFF                                              | 4.161   | ( 1.6271)  | 474230.69  | 12.440    |    |
| EVAPOTRANSPIRATION                                  | 25.868  | ( 3.1274)  | 2948536.00 | 77.348    |    |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 4          | 2.81367 | ( 1.21238) | 320707.656 | 8.41298   |    |
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 6              | 0.00027 | ( 0.00011) | 30.642     | 0.00080   |    |
| AVERAGE HEAD ON TOP<br>OF LAYER 5                   | 0.346   | ( 0.149)   |            |           |    |
| CHANGE IN WATER STORAGE                             | 0.601   | ( 2.1597)  | 68554.64   | 1.798     |    |

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| PEAK DAILY VALUES FOR YEARS                                  |           |             | 1 THROUGH | 25 |
|--------------------------------------------------------------|-----------|-------------|-----------|----|
|                                                              | (INCHES)  | (CU. FT.)   |           |    |
| PRECIPITATION                                                | 3.44      | 392098.094  |           |    |
| RUNOFF                                                       | 1.975     | 225122.4840 |           |    |
| DRAINAGE COLLECTED FROM LAYER 4                              | 0.01977   | 2253.52466  |           |    |
| PERCOLATION/LEAKAGE THROUGH LAYER 6                          | 0.000002  | 0.20126     |           |    |
| AVERAGE HEAD ON TOP OF LAYER 5                               | 0.889     |             |           |    |
| MAXIMUM HEAD ON TOP OF LAYER 5                               | 1.659     |             |           |    |
| LOCATION OF MAXIMUM HEAD IN LAYER 4<br>(DISTANCE FROM DRAIN) | 42.3 FEET |             |           |    |
| SNOW WATER                                                   | 2.22      | 252528.0310 |           |    |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.4152      |           |    |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.1350      |           |    |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 25

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 2.6733   | 0.2228    |
| 2          | 61.7891  | 0.2575    |
| 3          | 1.0614   | 0.0885    |
| 4          | 0.6412   | 0.0534    |
| 5          | 0.0000   | 0.0000    |
| 6          | 10.2480  | 0.4270    |
| SNOW WATER | 0.201    |           |

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## **Appendix O-9**

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**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\OGE1R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\OGE1R003.OUT

```

TIME: 18:55      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 9
THICKNESS           = 12.00 INCHES
POROSITY             = 0.5010 VOL/VOL
FIELD CAPACITY       = 0.2840 VOL/VOL
WILTING POINT       = 0.1350 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.3062 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.190000006000E-03 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 30

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 240.00             | INCHES  |
| POROSITY                   | = | 0.5410             | VOL/VOL |
| FIELD CAPACITY             | = | 0.1870             | VOL/VOL |
| WILTING POINT              | = | 0.0470             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.1947             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.499999987000E-04 | CM/SEC  |

LAYER 3

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0455             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 4

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |               |         |
|----------------------------|---|---------------|---------|
| THICKNESS                  | = | 0.69          | INCHES  |
| POROSITY                   | = | 0.8500        | VOL/VOL |
| FIELD CAPACITY             | = | 0.0100        | VOL/VOL |
| WILTING POINT              | = | 0.0050        | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0102        | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 1.28999996000 | CM/SEC  |
| SLOPE                      | = | 1.00          | PERCENT |
| DRAINAGE LENGTH            | = | 541.0         | FEET    |

LAYER 5

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

LAYER 6

-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE # 9 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 2.% AND  
A SLOPE LENGTH OF 720. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 91.30  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 28.100 | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 3.675  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.012  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.620  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 61.200 | INCHES      |
| TOTAL INITIAL WATER                | = | 61.200 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

# EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |               |
|---------------------------------------|---|---------------|
| STATION LATITUDE                      | = | 38.70 DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50          |
| START OF GROWING SEASON (JULIAN DATE) | = | 98            |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300           |
| EVAPORATIVE ZONE DEPTH                | = | 12.0 INCHES   |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 25

|                                                   | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------------------------------------------------|---------|---------|---------|---------|---------|---------|
| -----                                             | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION                                     |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| TOTALS                                            | 1.48    | 2.08    | 3.12    | 3.53    | 3.24    | 4.61    |
|                                                   | 3.36    | 2.45    | 2.96    | 2.30    | 2.13    | 2.18    |
| STD. DEVIATIONS                                   | 0.86    | 1.11    | 0.97    | 1.36    | 1.58    | 2.13    |
|                                                   | 1.90    | 1.28    | 1.45    | 1.31    | 1.49    | 1.09    |
| RUNOFF                                            |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| TOTALS                                            | 0.391   | 0.787   | 0.587   | 0.212   | 0.265   | 0.654   |
|                                                   | 0.392   | 0.109   | 0.234   | 0.151   | 0.218   | 0.161   |
| STD. DEVIATIONS                                   | 0.452   | 0.654   | 0.824   | 0.222   | 0.351   | 0.754   |
|                                                   | 0.548   | 0.144   | 0.217   | 0.199   | 0.266   | 0.215   |
| EVAPOTRANSPIRATION                                |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| TOTALS                                            | 0.569   | 0.697   | 2.472   | 3.494   | 2.909   | 3.987   |
|                                                   | 3.079   | 2.410   | 2.233   | 1.795   | 1.364   | 0.859   |
| STD. DEVIATIONS                                   | 0.318   | 0.474   | 0.492   | 0.953   | 1.133   | 1.415   |
|                                                   | 1.345   | 1.087   | 1.145   | 0.670   | 0.512   | 0.255   |
| LATERAL DRAINAGE COLLECTED FROM LAYER 4           |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| TOTALS                                            | 0.2922  | 0.2075  | 0.2035  | 0.2098  | 0.1508  | 0.1063  |
|                                                   | 0.1599  | 0.2529  | 0.2804  | 0.3148  | 0.3142  | 0.3278  |
| STD. DEVIATIONS                                   | 0.1408  | 0.1104  | 0.1359  | 0.1175  | 0.0870  | 0.0816  |
|                                                   | 0.1536  | 0.1692  | 0.1658  | 0.1653  | 0.1374  | 0.1332  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6               |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| TOTALS                                            | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                                   | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
| STD. DEVIATIONS                                   | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                                   | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
| -----                                             |         |         |         |         |         |         |
| AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES) |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| DAILY AVERAGE HEAD ON TOP OF LAYER 5              |         |         |         |         |         |         |
| -----                                             |         |         |         |         |         |         |
| AVERAGES                                          | 0.0697  | 0.0542  | 0.0486  | 0.0517  | 0.0360  | 0.0262  |
|                                                   | 0.0382  | 0.0604  | 0.0691  | 0.0751  | 0.0775  | 0.0782  |
| STD. DEVIATIONS                                   | 0.0336  | 0.0287  | 0.0324  | 0.0290  | 0.0208  | 0.0201  |
|                                                   | 0.0367  | 0.0404  | 0.0409  | 0.0395  | 0.0339  | 0.0318  |

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| AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 25 |         |            |            |         |
|------------------------------------------------------------------|---------|------------|------------|---------|
|                                                                  | INCHES  |            | CU. FEET   | PERCENT |
| PRECIPITATION                                                    | 33.44   | ( 4.389)   | 3411429.2  | 100.00  |
| RUNOFF                                                           | 4.161   | ( 1.6271)  | 424391.19  | 12.440  |
| EVAPOTRANSPIRATION                                               | 25.868  | ( 3.1274)  | 2638658.00 | 77.348  |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 4                       | 2.82031 | ( 1.20619) | 287680.219 | 8.43284 |
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 6                           | 0.00005 | ( 0.00002) | 5.415      | 0.00016 |
| AVERAGE HEAD ON TOP<br>OF LAYER 5                                | 0.057   | ( 0.024)   |            |         |
| CHANGE IN WATER STORAGE                                          | 0.595   | ( 2.1461)  | 60694.28   | 1.779   |

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| PEAK DAILY VALUES FOR YEARS 1 THROUGH 25                     |           |             |
|--------------------------------------------------------------|-----------|-------------|
|                                                              | (INCHES)  | (CU. FT.)   |
| PRECIPITATION                                                | 3.44      | 350890.344  |
| RUNOFF                                                       | 1.975     | 201463.1090 |
| DRAINAGE COLLECTED FROM LAYER 4                              | 0.02321   | 2367.64014  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6                          | 0.000000  | 0.04056     |
| AVERAGE HEAD ON TOP OF LAYER 5                               | 0.172     |             |
| MAXIMUM HEAD ON TOP OF LAYER 5                               | 0.336     |             |
| LOCATION OF MAXIMUM HEAD IN LAYER 4<br>(DISTANCE FROM DRAIN) | 12.3 FEET |             |
| SNOW WATER                                                   | 2.22      | 225988.4530 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.4152      |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |           | 0.1350      |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 25

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 2.6733   | 0.2228    |
| 2          | 61.7891  | 0.2575    |
| 3          | 1.0614   | 0.0885    |
| 4          | 0.1028   | 0.1490    |
| 5          | 0.0000   | 0.0000    |
| 6          | 10.2480  | 0.4270    |
| SNOW WATER | 0.201    |           |

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## **Appendix O-10**

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**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE      **
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)          **
**      DEVELOPED BY ENVIRONMENTAL LABORATORY                **
**      USAE WATERWAYS EXPERIMENT STATION                   **
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY      **
**
**
*****
*****

```

```

PRECIPITATION DATA FILE:  C:\HELP\ALPPR612.D4
TEMPERATURE DATA FILE:   C:\HELP\ALPTE612.D7
SOLAR RADIATION DATA FILE: C:\HELP\ALPSR612.D13
EVAPOTRANSPIRATION DATA:  C:\HELP\ALPEV612.D11
SOIL AND DESIGN DATA FILE: C:\HELP\INPUTS\OGE2R003.D10
OUTPUT DATA FILE:         C:\HELP\OUT\OGE2R003.OUT

```

TIME: 19: 9      DATE: 10/30/2012

```

*****
TITLE:  Ameren Missouri Labadie Proposed Utility Waste Landfill
*****

```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

```

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 9
THICKNESS           = 12.00 INCHES
POROSITY             = 0.5010 VOL/VOL
FIELD CAPACITY       = 0.2840 VOL/VOL
WILTING POINT       = 0.1350 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.3111 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.190000006000E-03 CM/SEC
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.34
      FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

```

LAYER 2

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 30

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 120.00             | INCHES  |
| POROSITY                   | = | 0.5410             | VOL/VOL |
| FIELD CAPACITY             | = | 0.1870             | VOL/VOL |
| WILTING POINT              | = | 0.0470             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.2011             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.499999987000E-04 | CM/SEC  |

LAYER 3

-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 12.00              | INCHES  |
| POROSITY                   | = | 0.4170             | VOL/VOL |
| FIELD CAPACITY             | = | 0.0450             | VOL/VOL |
| WILTING POINT              | = | 0.0180             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0473             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.500000007000E-01 | CM/SEC  |

LAYER 4

-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

|                            |   |               |         |
|----------------------------|---|---------------|---------|
| THICKNESS                  | = | 0.69          | INCHES  |
| POROSITY                   | = | 0.8500        | VOL/VOL |
| FIELD CAPACITY             | = | 0.0100        | VOL/VOL |
| WILTING POINT              | = | 0.0050        | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0100        | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 1.28999996000 | CM/SEC  |
| SLOPE                      | = | 33.33         | PERCENT |
| DRAINAGE LENGTH            | = | 60.0          | FEET    |

LAYER 5

-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

|                            |   |                    |            |
|----------------------------|---|--------------------|------------|
| THICKNESS                  | = | 0.06               | INCHES     |
| POROSITY                   | = | 0.0000             | VOL/VOL    |
| FIELD CAPACITY             | = | 0.0000             | VOL/VOL    |
| WILTING POINT              | = | 0.0000             | VOL/VOL    |
| INITIAL SOIL WATER CONTENT | = | 0.0000             | VOL/VOL    |
| EFFECTIVE SAT. HYD. COND.  | = | 0.199999996000E-12 | CM/SEC     |
| FML PINHOLE DENSITY        | = | 2.00               | HOLES/ACRE |
| FML INSTALLATION DEFECTS   | = | 2.00               | HOLES/ACRE |
| FML PLACEMENT QUALITY      | = | 3                  | - GOOD     |

LAYER 6

-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

|                            |   |                    |         |
|----------------------------|---|--------------------|---------|
| THICKNESS                  | = | 24.00              | INCHES  |
| POROSITY                   | = | 0.4270             | VOL/VOL |
| FIELD CAPACITY             | = | 0.4180             | VOL/VOL |
| WILTING POINT              | = | 0.3670             | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.4270             | VOL/VOL |
| EFFECTIVE SAT. HYD. COND.  | = | 0.100000001000E-06 | CM/SEC  |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE # 9 WITH BARE  
GROUND CONDITIONS, A SURFACE SLOPE OF 2.% AND  
A SLOPE LENGTH OF 720. FEET.

|                                    |   |        |             |
|------------------------------------|---|--------|-------------|
| SCS RUNOFF CURVE NUMBER            | = | 91.30  |             |
| FRACTION OF AREA ALLOWING RUNOFF   | = | 100.0  | PERCENT     |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 3.300  | ACRES       |
| EVAPORATIVE ZONE DEPTH             | = | 12.0   | INCHES      |
| INITIAL WATER IN EVAPORATIVE ZONE  | = | 3.734  | INCHES      |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.012  | INCHES      |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.620  | INCHES      |
| INITIAL SNOW WATER                 | = | 0.000  | INCHES      |
| INITIAL WATER IN LAYER MATERIALS   | = | 38.694 | INCHES      |
| TOTAL INITIAL WATER                | = | 38.694 | INCHES      |
| TOTAL SUBSURFACE INFLOW            | = | 0.00   | INCHES/YEAR |

# EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
ST. LOUIS MISSOURI

|                                       |   |               |
|---------------------------------------|---|---------------|
| STATION LATITUDE                      | = | 38.70 DEGREES |
| MAXIMUM LEAF AREA INDEX               | = | 0.50          |
| START OF GROWING SEASON (JULIAN DATE) | = | 98            |
| END OF GROWING SEASON (JULIAN DATE)   | = | 300           |
| EVAPORATIVE ZONE DEPTH                | = | 12.0 INCHES   |
| AVERAGE ANNUAL WIND SPEED             | = | 10.40 MPH     |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 73.00 %       |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 67.00 %       |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 71.00 %       |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 74.00 %       |

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 1.72    | 2.14    | 3.28    | 3.55    | 3.54    | 3.73    |
| 3.63    | 2.55    | 2.70    | 2.32    | 2.53    | 2.22    |

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI

## NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

| JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|---------|---------|---------|---------|---------|---------|
| 28.60   | 33.80   | 43.20   | 56.10   | 65.60   | 74.80   |
| 78.90   | 77.00   | 69.70   | 57.90   | 44.60   | 34.20   |

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR ST. LOUIS MISSOURI  
AND STATION LATITUDE = 38.70 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 25

|                                         | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------------------------------|---------|---------|---------|---------|---------|---------|
| -----                                   | -----   | -----   | -----   | -----   | -----   | -----   |
| PRECIPITATION                           |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 1.48    | 2.08    | 3.12    | 3.53    | 3.24    | 4.61    |
|                                         | 3.36    | 2.45    | 2.96    | 2.30    | 2.13    | 2.18    |
| STD. DEVIATIONS                         | 0.86    | 1.11    | 0.97    | 1.36    | 1.58    | 2.13    |
|                                         | 1.90    | 1.28    | 1.45    | 1.31    | 1.49    | 1.09    |
| RUNOFF                                  |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.394   | 0.796   | 0.601   | 0.222   | 0.271   | 0.671   |
|                                         | 0.404   | 0.112   | 0.243   | 0.153   | 0.222   | 0.167   |
| STD. DEVIATIONS                         | 0.455   | 0.656   | 0.824   | 0.237   | 0.357   | 0.769   |
|                                         | 0.555   | 0.149   | 0.222   | 0.209   | 0.268   | 0.220   |
| EVAPOTRANSPIRATION                      |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.567   | 0.695   | 2.466   | 3.495   | 2.923   | 3.983   |
|                                         | 3.074   | 2.428   | 2.243   | 1.783   | 1.378   | 0.857   |
| STD. DEVIATIONS                         | 0.317   | 0.472   | 0.489   | 0.934   | 1.114   | 1.409   |
|                                         | 1.344   | 1.076   | 1.129   | 0.666   | 0.495   | 0.254   |
| LATERAL DRAINAGE COLLECTED FROM LAYER 4 |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.2596  | 0.1940  | 0.1951  | 0.2016  | 0.1607  | 0.1715  |
|                                         | 0.2941  | 0.3313  | 0.3130  | 0.3359  | 0.3121  | 0.3079  |
| STD. DEVIATIONS                         | 0.1270  | 0.0991  | 0.1028  | 0.1071  | 0.1131  | 0.1970  |
|                                         | 0.2319  | 0.2140  | 0.1787  | 0.1565  | 0.1247  | 0.1157  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6     |         |         |         |         |         |         |
| -----                                   |         |         |         |         |         |         |
| TOTALS                                  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
| STD. DEVIATIONS                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |
|                                         | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  | 0.0000  |

-----  
AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
-----

| DAILY AVERAGE HEAD ON TOP OF LAYER 5 |        |        |        |        |        |        |
|--------------------------------------|--------|--------|--------|--------|--------|--------|
| -----                                |        |        |        |        |        |        |
| AVERAGES                             | 0.0004 | 0.0003 | 0.0003 | 0.0003 | 0.0003 | 0.0003 |
|                                      | 0.0005 | 0.0005 | 0.0005 | 0.0005 | 0.0005 | 0.0005 |
| STD. DEVIATIONS                      | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0003 |
|                                      | 0.0004 | 0.0003 | 0.0003 | 0.0003 | 0.0002 | 0.0002 |

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| AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS |         |            |           | 1 THROUGH | 25       |
|-----------------------------------------------------|---------|------------|-----------|-----------|----------|
|                                                     |         |            |           | INCHES    | CU. FEET |
|                                                     |         |            |           | PERCENT   |          |
| PRECIPITATION                                       | 33.44   | ( 4.389)   | 400630.5  | 100.00    |          |
| RUNOFF                                              | 4.257   | ( 1.6530)  | 50989.73  | 12.727    |          |
| EVAPOTRANSPIRATION                                  | 25.892  | ( 3.1254)  | 310166.03 | 77.419    |          |
| LATERAL DRAINAGE COLLECTED<br>FROM LAYER 4          | 3.07670 | ( 1.26999) | 36855.824 | 9.19946   |          |
| PERCOLATION/LEAKAGE THROUGH<br>LAYER 6              | 0.00000 | ( 0.00000) | 0.015     | 0.00000   |          |
| AVERAGE HEAD ON TOP<br>OF LAYER 5                   | 0.000   | ( 0.000)   |           | .         |          |
| CHANGE IN WATER STORAGE                             | 0.219   | ( 1.7240)  | 2618.90   | 0.654     |          |

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| PEAK DAILY VALUES FOR YEARS                                  |  |  | 1 THROUGH | 25         |
|--------------------------------------------------------------|--|--|-----------|------------|
|                                                              |  |  | (INCHES)  | (CU. FT.)  |
| PRECIPITATION                                                |  |  | 3.44      | 41207.762  |
| RUNOFF                                                       |  |  | 2.008     | 24057.4727 |
| DRAINAGE COLLECTED FROM LAYER 4                              |  |  | 0.03123   | 374.08154  |
| PERCOLATION/LEAKAGE THROUGH LAYER 6                          |  |  | 0.000000  | 0.00009    |
| AVERAGE HEAD ON TOP OF LAYER 5                               |  |  | 0.002     |            |
| MAXIMUM HEAD ON TOP OF LAYER 5                               |  |  | 0.016     |            |
| LOCATION OF MAXIMUM HEAD IN LAYER 4<br>(DISTANCE FROM DRAIN) |  |  | 0.0 FEET  |            |
| SNOW WATER                                                   |  |  | 2.22      | 26539.5703 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL)                            |  |  |           | 0.4162     |
| MINIMUM VEG. SOIL WATER (VOL/VOL)                            |  |  |           | 0.1350     |

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
by Bruce M. McEnroe, University of Kansas  
ASCE Journal of Environmental Engineering  
Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 25

| LAYER      | (INCHES) | (VOL/VOL) |
|------------|----------|-----------|
| 1          | 2.6890   | 0.2241    |
| 2          | 29.9731  | 0.2498    |
| 3          | 1.0424   | 0.0869    |
| 4          | 0.0069   | 0.0100    |
| 5          | 0.0000   | 0.0000    |
| 6          | 10.2480  | 0.4270    |
| SNOW WATER | 0.201    |           |

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## **Appendix O-11**