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Volume 2: Commercial and Industrial Measures

MEEIA 2019-21 Plan Revision 4.0<u>5.0</u>

Ameren Missouri TRM - Volume 2: C&I Measures Revision Log

Revision	Date	Description
1.0	05/30/2018	Initial version filed for Commission approval.
1.1	06/19/2020	Updated version to include new measures and updates to existing measures
2.0	10/15/2020	Updated version to include updates to existing measures.
3.0	9/15/2021	Update "Deemed Tables" with PY2020 Evaluation results plus updates to existing measures (lighting, chiller, pool pump). Added EUL lookup table for lighting measures from PY19.
4.0	9/26/2022	Updated "Deemed Tables" with PY2021 Evaluation results and added two new measures: 2.2.2 Compressed Air Leak Repair (shifting Compressed Air Nozzle and VSD Air Compressor to 2.2.3 and 2.2.4, respectively) and 2.5.10 Chiller Tune-Up.
5.0	10/05/2023	Updated baselines to 2015 IECC (effective 1/1/2024) for 2.5.5, 2.5.6, and 2.5.8. Updated baseline table to include only 2015 IECC for 2.5.7 PTAC/PTHP. Added "exterior" to 24/7 lighting coincidence factor because 24/7 interior lighting (e.g., exit signs) are included in the indoor lighting coincidence factor. Retired measures 2.6.4 and 2.6.7 in response to the EISA backstop provision becoming effective 8/1/2023. Expanded measure 2.2.4 VSD Air Compressor description to include units up to 200-hp.
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MEEIA 2019-21 Plan

Revision 4.0<u>5.0</u>

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Volume 2: Commercial and Industrial Measures

2.1 Appliances

2.1.1 Clothes Washer

DESCRIPTION

This measure relates to the installation of a commercial-grade clothes washer meeting the ENERGY STAR® minimum qualifications. Note it is assumed the domestic hot water (DHW) and dryer fuels of the installations are known.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The commercial-grade clothes washer must meet the ENERGY STAR® minimum qualifications (provided in the table below), as required by the program. The current specification is effective as of February 5, 2018.

DEFINITION OF BASELINE EQUIPMENT

The baseline condition is a commercial-grade clothes washer meeting the minimum federal baseline as of January 2013.¹

Efficiency Level		Top loading	Front Loading
Baseline	Federal Standard	≥1.6 MEF, ≤8.5 WF	≥2.00 MEF, ≤5.5 WF
Efficient	ENERGY STAR®	N/A	≥2.2 MEF, ≤4.0 IWF

The Modified Energy Factor (MEF) includes unit operation, water heating, and drying energy use, with the higher the value the more efficient the unit; "The quotient of the capacity of the clothes container, divided by the total clothes washer energy consumption per cycle, with such energy consumption expressed as the sum of the machine electrical energy consumption, the hot water energy consumption, and the energy required for removal of the remaining moisture in the wash load."

The Water Factor (WF) indicates the total water consumption of the unit, with the lower the value the less water required; "The quotient of the total weighted per-cycle water consumption for cold wash, divided by the capacity of the clothes washer." 2

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 11 years.³

¹ See federal standard 10 CFR 431.152.

² Definitions provided on the Energy Star® website.

³ Appliance Magazine, September 2007 as referenced in ENERGY STAR® Commercial Clothes Washer Calculator.

DEEMED MEASURE COST

The incremental cost is assumed to be \$200.4

LOADSHAPE

Loadshape - Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = [(Capacity* \frac{1}{\textit{MEFbase}}*Ncycles)*(\%CWbase + (\%DHWbase * \%ElectricDHW) + (\%Dryerbase * \%ElectricDryer))] - [(Capacity* \frac{1}{\textit{MEFeff}}*Ncycles)*(\%CWeff + (\%DHWeff * \%ElectricDHW) + (\%Dryereff * \%ElectricDryer))]$

Where:

Capacity = Clothes washer capacity (cubic feet) = Actual - If capacity is unknown, assume 3.1 cubic feet ⁵ **MEFbase** = Modified Energy Factor of baseline unit = Actual. If unknown, assume average values provided below. MEFeff = Modified Energy Factor of efficient unit Ncycles = Number of Cycles per year $=2190^6$ %CW = Percentage of total energy consumption for clothes washer operation (different for baseline and efficient unit – see table below) %DHW = Percentage of total energy consumption used for water heating (different for baseline and efficient unit – see table below) %Dryer = Percentage of total energy consumption for dryer operation (different for baseline and efficient unit – see table below)

%Electric_{DHW} = Percentage of DHW savings assumed to be electric %Electric_{Dryer} = Percentage of dryer savings assumed to be electric

⁴ Based on Industry Data 2007 as referenced in ENERGY STAR® Commercial Clothes Washer Calculator.

⁵ Based on the average clothes washer volume of all units that pass the federal standard on the California Energy Commission (CEC) database of commercial clothes washer products (accessed on 11/26/2015).

⁶ Based on DOE Technical Support Document, 2009; Chapter 8 Life-Cycle Cost and Payback Period Analysis, p 8-15.

Efficiency Level	MEFbase and MEFee			
Efficiency Level	Top loading	Front Loading	Weighted Average ⁷	
Federal Standard	1.6	2.0	1.7	
ENERGY STAR®	N/A	2.2	2.2	

Ecc.:II	Percentage of Total Energy Consumption 8			
Efficiency Level	%CW	%DHW	%Dryer	
Federal Standard	6.5%	25.9%	67.6%	
ENERGY STAR®	3.5%	14.1%	82.4%	

DHW fuel	%Electric _{DHW}	
Electric	100%	
Natural Gas	0%	

Dryer fuel	%Electric _{Dryer}	
Electric	100%	
Natural Gas	0%	

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below.9

•	ΔkWh			
Efficiency Level	Electric DHW Electric Dryer	Gas DHW Electric Dryer	Electric DHW Gas Dryer	Gas DHW Gas Dryer
ENERGY STAR®	808.2	229.3	725.3	146.5

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

⁷ Weighted average MEF of federal standard rating for front- loading and top- loading units. Baseline weighting is based upon the relative top front loading percentage of available non-ENERGY STAR[®] commercial products in the CEC database (accessed 11/26/2015) and ENERGY STAR[®] weighting is based on eligible products as of 11/26/2015. The relative weightings are as follows, see more information in "Commercial Clothes Washer Analysis.xlsx":

Efficiency Level	Front	Top
Baseline	37%	63%
ENERGY STAR®	99%	1%

⁸ The percentage of total energy consumption that is used for the machine, heating the hot water, or by the dryer is different depending on the efficiency of the unit. Values are based on a data provided in the ENERGY STAR® Calculator for Commercial Clothes Washers.

Clothes Washers.

Note that the baseline savings is based on the weighted average baseline MEF (as opposed to assuming front baseline for front-efficient unit and top baseline for top- efficient unit). The reasoning is that the support of the program of more efficient units (which are predominately front loading) will result in some participants switching from planned purchase of a top loader to a front loader.

Where:

 ΔkWh = Energy Savings as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $=0.0001379439^{10}$

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below.

	ΔkW			
Efficiency Level	Electric DHW Electric Dryer	Gas DHW Electric Dryer	Electric DHW Gas Dryer	Gas DHW Gas Dryer
ENERGY STAR®	0.1115	0.0316	0.1001	0.0202

NATURAL GAS SAVINGS

$$\Delta Therms = [[(Capacity*\frac{1}{\textit{MEFbase}}*Ncycles)*((\%DHWbase*\%Natural GasDHW*R_eff) + (\%Dryerbase*\%GasDryer\%Gas_Dryer))] - [(Capacity*\frac{1}{\textit{MEFeff}}*Ncycles)*((\%DHWeff*\%GasDHW\%Natural Gas_DHW*R_eff) + (\%Dryereff*MGasDryer\%Gas_Dryer))]]*Therm_convert$$

Where:

%Gas_{DHW} = Percentage of DHW savings assumed to be Natural Gas

R eff = Recovery efficiency factor

 $=1.26^{11}$

%Gas_{Dryer} = Percentage of dryer savings assumed to be Natural Gas

Therm convert = Conversion factor from kWh to Therm

= 0.03412

Other factors as defined above.

DHW fuel	%Gas _{DHW}	
Electric	0%	
Natural Gas	100%	

Therefore a factor of 0.98/0.78 (1.26) is applied.

¹⁰ Based on Ameren Missouri 2016 Loadshape for Business Miscellaneous End-Use. Upon inspection and comparison to the residential clothes washer coincidence factor, this is a reasonable assumption until data becomes available to inform a technology specific coincidence factor. Given that business laundry schedules are likely more variable compared to residential, it follows that less overlap with the system peak hour is possible.

¹¹ To account for the different efficiency of electric and natural gas hot water heaters (gas water heater: recovery efficiencies ranging from 0.74 to 0.85 (0.78 used), and electric water heater with 0.98 recovery efficiency (http://www.energystar.gov/ia/partners/bldrs_lenders_raters/downloads/Waste_Water_Heat_Recovery_Guidelines.pdf).

Dryer fuel	%Gas _{Dryer}
Electric	0%
Natural Gas	100%

Using the default assumptions provided above, the prescriptive savings for each configuration are presented below:

	ΔTherms			
Efficiency Level	Electric DHW	Gas DHW	Electric DHW	Gas DHW
Efficiency Level	Electric Dryer	Electric Dryer	Gas Dryer	Gas Dryer
ENERGY STAR®	0.0	24.9	2.8	27.7

WATER IMPACT DESCRIPTIONS AND CALCULATION

 $\Delta Water(gallons) = Capacity * (IWFbase - IWFeff) * Ncycles$

Where:

WFbase = Water Factor of baseline clothes washer WFeff = Water Factor of efficient clothes washer

= Actual - If unknown assume average values provided below

Using the default assumptions provided above, the prescriptive water savings for each efficiency level are presented below.

	WF			∆Water (gallons per year)
Efficiency Level	Top Loaders	Front Loaders	Weighted Average	Weighted Average
Federal Standard 12	8.5	5.5	7.4	n/a
ENERGY STAR®		4.5		19,874

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

¹² Weighted average MEF of federal standard rating for frontloading and top- loading units. Baseline weighting is based upon the relative top v front loading percentage of available non-ENERGY STAR® commercial product in the CEC database (accessed 11/26/2015) and ENERGY STAR® weighting is based on eligible products as of 11/26/2015. The relative weightings are as follows, see more information in "Commercial Clothes Washer Analysis.xlsx":

Efficiency Level	Front	Top
Baseline	37%	63%
ENERGY STAR®	99%	1%

2.1.2 Clothes Dryer

DESCRIPTION

This measure is for the installation of a residential clothes dryer, utilized in a commercial setting, meeting the ENERGY STAR® criteria. ENERGY STAR® qualified clothes dryers save energy through a combination of more efficient drying and reduced runtime of the drying cycle. More efficient drying is achieved through increased insulation, modifying operating conditions (such as air flow and/or heat input rate) improving air circulation through better drum design or booster fans, and improving efficiency of motors. Reducing the runtime of dryers through automatic termination by temperature and moisture sensors is believed to have the greatest potential for reducing energy use in clothes dryers.¹³ ENERGY STAR® provides criteria for both gas and electric clothes dryers.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

Clothes dryer must meet the ENERGY STAR® criteria, as required by the program.

Definition of Baseline Equipment

The baseline condition is a clothes dryer meeting the minimum federal requirements for units manufactured on or after January 1, 2015.

Deemed Lifetime of Efficient Equipment

The expected measure life is assumed to be 14 years. 14

Deemed Measure Cost

Dryer Size	Incremental Cost 15
Standard	\$75
Compact	\$105

LOADSHAPE

Loadshape - Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

 $\underline{https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx}$

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¹³ ENERGY STAR® Market & Industry Scoping Report. Residential Clothes Dryers. Table 8. November 2011. http://www.energystar.gov/ia/products/downloads/ENERGY STAR Scoping Report Residential Clothes Dryers.pdf

14 Based on an average estimated range of 12-16 years. ENERGY STAR® Market & Industry Scoping Report. Residential Clothes Dryers. November 2011.

http://www.energystar.gov/ia/products/downloads/ENERGY_STAR_Scoping_Report_Residential_Clothes_Dryers.pdf

15 Cost based on ENERGY STAR® Savings Calculator for ENERGY STAR® Qualified Appliances.

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = (Load/CEFbase - Load/CEFeff) * Ncycles * \%Electric$

Where:

= The average total weight (lbs.) of clothes per drying cycle. If dryer Load

size is unknown, assume standard.

CEFbase = Combined energy factor (CEF) (lbs./kWh) of the baseline unit is

based on existing federal standards energy factor and adjusted to CEF as performed in the ENERGY STAR® analysis. 16 If product class

unknown, assume electric, standard.

= CEF (lbs./kWh) of the ENERGY STAR® unit based on ENERGY CEFeff

STAR® requirements. ¹⁷ If product class unknown, assume electric,

Ncycles = Number of dryer cycles per year. Use actual data if available. If

unknown, refer to the table below.¹⁸

= 100% for electric dryers, 5% for gas dryers¹⁹ %Electric

Dryer Size	Load (lbs.) ²⁰
Standard	8.45
Compact	3

Product Class	CEFbase (lbs./kWh)
Vented Electric, Standard (≥ 4.4 ft ³)	3.11
Vented Electric, Compact (120V) (< 4.4 ft ³)	3.01
Vented Electric, Compact (240V) (<4.4 ft ³)	2.73
Ventless Electric, Compact (240V) (<4.4 ft ³)	2.13
Vented Gas	2.84 ²¹

¹⁶ ENERGY STAR® Draft 2 Version 1.0 Clothes Dryers Data and Analysis

¹⁷ ENERGY STAR® Clothes Dryers Key Product Criteria.
https://www.energystar.gov/index.cfm?e=clothesdry.pr_crit_clothes_dryers

18 NOPR analysis for DOE Commercial Clothes Washer standard. Annual use cycles of 1,074 and 1,483 for multifamily and laundromat applications, respectively. https://www.regulations.gov/document?D=EERE-2012-BT-STD-0020-0021. On-premise laundromat cycle average value for dryer cycles in healthcare facility, hotels, drycleaners and laundromats from tests conducted in Nicor Gas Emerging Technology Program's Commercial Dryer Modulation Retrofit Public Project Report.

^{19 %}Electric accounts for the fact that some of the savings on gas dryers comes from electricity (motors, controls, etc.). 5% was determined using a ratio of the electric to total savings from gas dryers given by ENERGY STAR® Draft 2 Version 1.0 Clothes Dryers Data and Analysis. Value reported in 2015 EPA EnergySTAR $^{\tiny{\circledR}}$ appliance calculator.

²⁰ Based on ENERGY STAR® teprocedures. https://www.energystar.gov/index.cfm?c=clothesdry.pr_crit_clothes_dryers

²¹ Federal standards report CEF for gas clothes dryers in terms of lbs/kWh. To determine gas savings, this number is later converted

to therms.

Product Class	CEFeff (lbs./kWh)
Vented or Ventless Electric, Standard (≥ 4.4 ft3)	3.93
Vented or Ventless Electric, Compact (120V) (<4.4 ft3)	3.80
Vented Electric, Compact (240V) (< 4.4 ft3)	3.45
Ventless Electric, Compact (240V) (< 4.4 ft3)	2.68
Vented Gas	3.48 ²²

Application	Cycles per Year
Multi-family	1,074
Laundromat	1,483
On-Premise Laundromat	3,607

Using defaults provided above:

	ΔkWh		
Product Class	Multifamily	Laundromat	On-Premise Laundromat
Vented Electric, Standard (≥ 4.4 ft³)	608.9	840.7	2044.9
Vented Electric, Compact (120V) (< 4.4 ft ³)	222.5	307.3	747.4
Vented Electric, Compact (240V) (<4.4 ft ³)	246.3	340.1	827.2
Ventless Electric, Compact (240V) (<4.4 ft ³)	310.4	428.7	1042.6
Vented Gas	29.4	40.6	98.7

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = h * CF$

Where:

 ΔkWh = Energy savings as calculated above.

= Summer peak coincidence demand (kW) to annual energy (kWh) CF

factor

 $= 0.0001379439^{23}$

Using defaults provided above:

 $^{^{22}\} Federal\ standards\ report\ CEF\ for\ gas\ clothes\ dryers\ in\ terms\ of\ lbs/kWh.\ To\ determine\ gas\ savings,\ this\ number\ is\ later\ converted$

to therms.

23 Based on Ameren Missouri 2016 Loadshape for Business Miscellaneous End-Use. Upon inspection and comparison to the Residential clothes washer coincidence factor, this is a reasonable assumption until data becomes available to inform a technology specific coincidence factor. Given that business laundry schedules are likely more variable compared to residential, it follows that less overlap with the system peak hour is possible.

	ΔkW		
Product Class	Multifamily	Laundromat	On-Premise Laundromat
Vented Electric, Standard (≥ 4.4 ft³)	0.0840	0.1160	0.2821
Vented Electric, Compact (120V) (<4.4 ft ³)	0.0307	0.0424	0.1031
Vented Electric, Compact (240V) (<4.4 ft ³)	0.0340	0.0469	0.1141
Ventless Electric, Compact (240V) (<4.4 ft ³)	0.0428	0.0591	0.1438
Vented Gas	0.0041	0.0056	0.0136

NATURAL GAS ENERGY SAVINGS

Natural gas savings only apply to ENERGY STAR® vented gas clothes dryers.

$$\Delta Therm = \left(\frac{Load}{CEFbase} - \frac{Load}{CEFeff}\right) * Ncycles * Therm_convert * \%Gas$$

Where:

Therm_convert = Conversion factor from kWh to Therm

=0.03413

%Gas = Percent of overall savings coming from gas

= 0% for electric units and 84% for gas units²⁴

Using defaults provided above:

$$\Delta$$
Therms = $(8.45/2.84 - 8.45/3.48) * Ncycles * 0.03413 * 0.84$

		ΔTherms	
Product Class	Multi-family	Laundromat	On-Premise
	Multi-laminy	Laundromat	
Vented Gas	16.8	23.3	56.6

PEAK GAS SAVINGS

Savings for this measure is assumed to be evenly spread across the year. The Peak Gas Savings is therefore assumed to be:

$$\Delta PeakTherms = \underline{\hspace{1cm}}$$
 365.25

Where:

$$\Delta$$
Therms = Therm impact calculated above = Days per year

²⁴ % Gas accounts for the fact that some of the savings on gas dryers comes from electricity (motors, controls, etc.). 84% was determined using a ratio of the gas to total savings from gas dryers given by ENERGY STAR® Draft 2 Version 1.0 Clothes Dryers Data and Analysis.

Using defaults provided above:

	ΔPeakTherms			
Product Class	Multi-family	Laundromat	On-Premise Laundromat	
Vented Gas	0.0461	0.0637	0.1549	

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.2 Compressed Air

2.2.1 Compressed Air No Loss Condensate Drain

DESCRIPTION

No-loss condensate drains remove condensate as needed without venting compressed air, resulting in less air demand and better efficiency. Replacement or upgrades of existing no-loss drains are not eligible for this measure.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment is a no-loss condensate drain.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a standard condensate drain (open valve, timer, or both).

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The lifetime of a no-loss condensate drain is assumed to be 13 years.²⁵

DEEMED MEASURE COST

The measure cost is \$700 per drain.²⁶

LOADSHAPE

Air Comp BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = CFM_{reduced} * kW_{CFM} * Hours$

Where:

 $CFM_{reduced}$ = Reduced air consumption (CFM) per drain = 3 CFM^{27}

²⁵ "Measure Life Study," Energy & Resource Solutions (prepared for the Massachusetts Joint Utilities): Table 1-1, 2005.

²⁶ Based on empirical project data from ComEd Comprehensive Compressed Air Study program and VEIC review of pricing data found in CAS Cost Data.xls.

²⁷ Reduced CFM consumption is based on a timer drain opening for 10 seconds every 300 seconds as the baseline. See "Industrial System Standard Deemed Saving Analysis.xls."

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kW_{CFM} = System power demand reduction per reduced air consumption

(kw/CFM), depending on the type of compressor control, see table

below²⁸

Hours = Compressed air system pressurized hours

= Use actual hours if known, otherwise assume values in table below

Compressor Control Type	kW _{CFM}
Reciprocating - On/off Control	0.184
Reciprocating - Load/Unload	0.136
Screw - Load/Unload	0.152
Screw - Inlet Modulation	0.055
Screw - Inlet Modulation w/ Unloading	0.055
Screw - Variable Displacement	0.153
Screw - VFD	0.178

Shift	Hours	
Simple shift (9/5)	1976 hours: 7 AM – 3 PM, weekdays, minus some holidays and	
Single shift (8/5)	scheduled down time	
2 abift (16/5)	3952 hours: 7AM – 11 PM, weekdays, minus some holidays and	
2-shift (16/5)	scheduled down time	
2 abift (24/5)	5928 hours: 24 hours per day, weekdays, minus some holidays and	
3-shift (24/5)	scheduled down time	
4-shift (24/7)	8320 hours: 24 hours per day, 7 days a week minus some holidays	
	and scheduled down time	

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 Δ kWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001379439^{29}$

MEASURE CODE:

²⁸ Calculated based on the type of compressor control. This assumes the compressor will be between 40% and 100% capacity before and after the changes to the system demand. See "Industrial System Standard Deemed Saving Analysis.xls."

²⁹ 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Compressed Air. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

2.2.2 Compressed Air Leak Repair

DESCRIPTION

This measure applies to an installed air compressor that has developed leaks. Leaks in a compressed air system lead to an increase in energy use to maintain the necessary pressure in the system.

Savings are calculated by using information collected through survey and measurement of the compressed air system, including the cubic feet per minute (CFM) of the airflow of each leak using ultrasonic leak detection equipment.

DEFINITION OF EFFICIENT EQUIPMENT

Efficient Equipment is defined as the state of the air compressor system after leaks have been repaired. It is not necessarily the air compressor with no leaks left as some leaks may be impossible to reach or have substantial difficulty in fixing, therefore the efficient equipment is one that has all leaks repaired that have been stated to be repaired.

DEFINITION OF BASELINE EQUIPMENT

Baseline equipment is characterized by the condition of the compressed air system at the time of inspection before the leaks are repaired.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The effective useful life is 2 years. 30

DEEMED MEASURE COST

Measure cost should include the inspection and repair cost.

LOADSHAPE

Air Comp BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = CFM_{\text{leak}} * kW_{CFM} * Hours$

Where:

 CFM_{leak} = CFM leaving the air compressor system through leaks

= Use actual value if known, otherwise approximate value can be found

using dB and psig reading and the table below³¹

³⁰ 2022 WI TRM. PA Consulting Group. Focus on Energy, Business Programs: Measure Life Study Final Report. August 25, 2009. https://focusonenergy.com/sites/default/files/bpmeasurelifestudyfinal_evaluationreport.pdf

³¹ Values extrapolated from "Compressed Air Ultrasonic Leak Detection Guide" from UE Systems. Readings compensated for atmospheric pressure and taken at 40 kHz.

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 kW_{CFM} = System power demand reduction per reduced air consumption

(kw/CFM), depending on the type of compressor control, see table below 32

= Compressed air system pressurized hours Hours

= Use actual hours if known, otherwise assume values in table below,

based on business operating schedule

Digital Reading	10 PSIG	25 PSIG	50 PSIG	75 PSIG	100 PSIG
10 dB	0.05	0.1	0.2	0.3	0.5
20 dB	0.15	0.3	0.5	0.9	0.8
30 dB	0.4	0.5	0.8	1.1	1.4
40 dB	0.5	0.8	1.1	1.4	1.7
50 dB	1.9	2	2.2	1.8	2
60 dB	2.3	2.6	2.8	3	3.6
70 dB	3	3.4	3.9	4.9	5.2
80 dB	3.6	5.1	5.6	6.8	7.7
90 dB	5.3	6.8	7.1	7.7	8.4
100 dB	6	7.3	9.6	10	10.6

Compressor Control Type	kW _{CFM}
Reciprocating - On/off Control	0.184
Reciprocating - Load/Unload	0.136
Screw - Load/Unload	0.152
Screw - Inlet Modulation	0.055
Screw - Inlet Modulation w/ Unloading	0.055
Screw - Variable Displacement	0.153
Screw - VFD	0.178

Shift	Hours
Single shift (8/5)	1976 hours: 7 AM – 3 PM, weekdays, minus some holidays and
Single sint (6/3)	scheduled down time
2-shift (16/5)	3952 hours: 7AM – 11 PM, weekdays, minus some holidays and
2-81111 (10/3)	scheduled down time
3-shift (24/5)	5928 hours: 24 hours per day, weekdays, minus some holidays and
3-SIIII (24/3)	scheduled down time
4 -1-:0 (24/7)	8320 hours: 24 hours per day, 7 days a week minus some holidays
4-shift (24/7)	and scheduled down time

³² Calculated based on the type of compressor control. This assumes the compressor will be between 40% and 100% capacity before and after the changes to the system demand. See "Industrial System Standard Deemed Saving Analysis.xls."

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 $\Delta kWh \\$ = Electric energy savings, calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor = 0.0001379439³³ CF

MEASURE CODE:

³³ 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Compressed Air. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

2.2.3 Compressed Air Nozzle

DESCRIPTION

This measure applies to the replacement of a standard air nozzle with high-efficiency air nozzle used in a compressed air system. High-efficiency air nozzles use the Coandă effect to pull in free air and use significantly less compressed air for blowing off parts or for drying. These nozzles have the added benefits of noise reduction and improved safety in systems with greater than 30 psig.

This measure was developed to be applicable to the following program types: DI and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment is a compressed air nozzle meeting program requirements.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a standard air nozzle.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The measure life is 15 years.³⁴

DEEMED MEASURE COST

Incremental measure costs are presented in the following table.³⁵

Nozzle Diameter	Measure Cost
1/8"	\$42
1/4"	\$57
5/16"	\$87
1/2"	\$121

LOADSHAPE

Air Comp BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS

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^{34 &}quot;Focus on Energy Evaluation - Business Programs: Measure Life Study," prepared for State of Wisconsin Public Service Commission by PA Consulting Group, August 25, 2009.

³⁵ Costs are from EXAIR's website and are an average of nozzles that meet the flow requirements. Models include Atto Super, Pico Super, Nano Super, Micro Super, Mini Super, Super and Large Super nozzles. www.exair.com. Accessed March 20, 2014.

 $\Delta kWh = (SCFM * SCFM\%Reduced) * kW/CFM * \%Use * Hours$

Where:

SCFM = Air flow through standard nozzle.

= Actual rated flow at 80 psi, if known. If unknown, use CFM by

orifice diameter from table below. 36, 37

SCFM%Reduced = Percent reduction in air loss per nozzle.

= Estimated at 50%³⁸

kW/CFM = System power reduction per air demand (kW/CFM), depending on

the type of air compressor; see table below³⁹

%USE = Percent of the compressor total operating hours that the nozzle is in

use

= Custom, or if unknown, assume 5%⁴⁰

Hours = Compressed air system pressurized hours

= Use actual hours if known, otherwise assume values in table below.

Orifice Diameter	SCFM
1/8"	21
1/4"	58
5/16"	113
1/2"	280

Air Compressor Type	ΔkW/CFM
Reciprocating - On/off Control	0.18
Reciprocating – Load/Unload	0.14
Screw - Load/Unload	0.15
Screw – Inlet Modulation	0.06
Screw – Inlet Modulation w/	0.06
UnloadingScrew - Variable Displacement	0.15
Screw - VFD	0.18

³⁶ Review of manufacturer's information

³⁷ Technical Reference Manual (TRM) for Ohio Senate Bill 221,"Energy Efficiency and Conservation Program" and 09-512-GEUNC, October 15, 2009, Pgs 170-171.

³⁸ Conservative estimate based on average values provided by the Compressed Air Challenge Training Program, Machinery's

Handbook 25th Edition, and manufacturers' catalog. .

39 Calculated based on the type of compressor control. This assumes the compressor will be between 40% and 100% capacity before and after the changes to the system demand. See "Industrial System Standard Deemed Saving Analysis.xls."

40 Assumes 50% handheld air guns and 50% stationary air nozzles. Manual air guns tend to be used less than stationary air nozzles,

⁴⁰ Assumes 50% handheld air guns and 50% stationary air nozzles. Manual air guns tend to be used less than stationary air nozzles, and a conservative estimate of 1 second of blow-off per minute of compressor run time is assumed. Stationary air nozzles are commonly more wasteful as they are often mounted on machine tools and can be manually operated resulting in the possibility of a long term open blow situation. An assumption of 5 seconds of blow-off per minute of compressor run time is used.

Shift	Hours
Single shift (8/5)	1976 hours: 7 AM – 3 PM, weekdays, minus some holidays and scheduled
Single sinit (6/3)	down time
2 -1:0 (16/5)	3952 hours: 7AM – 11 PM, weekdays, minus some holidays and scheduled
2-shift (16/5)	down time
5928 hours: 24 hours per day, weekdays, minus some holidays and scl	
3-shift (24/5)	down time
4-shift (24/7)	8320 hours: 24 hours per day, 7 days a week minus some holidays and
	scheduled down time

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001379439^{41}$

NATURAL GAS SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

⁴¹ 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Compressed Air. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

2.2.4 VSD Air Compressor

DESCRIPTION

This measure relates to the installation of an air compressor with a variable frequency drive, load/no load controls, or variable displacement control. A baseline modulating compressor regulates output by choking off the inlet air, which is not efficient. Efficient compressors use a variable speed drive on the motor to match output to the load. Savings are calculated using representative baseline and efficient demand numbers for compressor capacities according to the facility's load shape, and the number of hours the compressor runs at that capacity. Demand curves are as per US Department of Energy (DOE) data for a Variable Speed compressor versus a Modulating compressor. This measure applies only to an individual compressor ≤ 40-200 hp. Only one compressor per compressed air distribution system is eligible.

This measure was developed to be applicable to the following program type: TOS. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The high efficiency equipment is a compressor 5-40-200 hp with variable speed control.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a modulating compressor with blow down 5-40-200 hp

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

10 years.42

DEEMED MEASURE COST⁴³

```
Incremental Cost ($) = (127 \text{ x hp}_{compressor}) + 1446) \times 1.2444
```

Where:

hpcompressor = compressor motor nominal horsepower = compressor motor nominal hp to incremental cost conversion factor and offset⁴⁵

LOADSHAPE

Air Comp BUS

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⁴² Based on data provided by vendors, reference file "VSD compressor lifetime and costs.xls."

⁴³ Based on data provided by vendors, reference file "VSD compressor lifetime and costs.xls."

⁴⁴ Adjustment for inflation since incremental cost study is in \$2008. The U.S. Bureau of Labor Statistic CPI Inflation Calculator was used to adjust \$2008 (January) to \$2021 (January). The resulting factor was 1.24. This adjustment was evaluated against current pricing of compressors (2021) and found to be a reasonable and appropriate. **was used to adjust \$2008 (January) to \$2021 (January). The resulting factor was 1.24. This adjustment was evaluated against current pricing of compressors (2021) and found to be a reasonable and appropriate.

⁴⁵ Conversion factor and offset based on a linear regression analysis of the relationship between air compressor motor nomine horsepower and incremental cost, as sourced from the Efficiency Vermont Technical Reference Manual (TRM). Several Vermon vendors were surveyed to determine the cost of equipment.

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 ΔkWh = 0.9 x hp_{compressor} x HOURS x (CF_b - CF_e)

Where:

 ΔkWh = gross customer annual kWh savings for the measure

hp_{compressor} = compressor motor nominal horsepower

0.9 = compressor motor nominal horsepower to full load kW conversion

factor46

HOURS = compressor total annual hours of operation. Custom input, if unknown use

the defaults based on shift structure below.

CF_b = baseline compressor factor, refer to table below-47

=0.890

 CF_e = efficient compressor ⁴⁸

 $=0.705 \text{ for units} \le 40 \text{ hp}$

=0.701 for units > 40 hp and < 50 hp =0.658 for units 50 - 200 hp

⁴⁶⁻Conversion factor based on a linear regression analysis of the relationship between air compressor motor nominal horsepower and full load kW from power measurements of 72 compressors at 50 facilities on Long Island. See "VSD Air Compressor – Supporting Information_with40to50hpbucket.xlsx" for more information.See "BHP Weighted Compressed Air Load Profiles

⁴⁷ Compressor factors were developed using DOE part load data for different compressor control types as well as load profiles from 50 facilities employing air compressors less than or equal to 40 hp. "See "BHP Weighted Compressed Air Load Profiles v3.xls" for source data and calculations:

⁴⁸ Compressor factors were developed using DOE part load data for different compressor control types as well as load profiles from 50 facilities employing air compressors less than or equal to 40 hp. "See "BHP Weighted Compressed Air Load Profiles v3.xls" for source data and calculations. The "variable speed drive" compressor factor has been adjusted up from the 0.675 presented in the analysis to 0.705 to account for the additional power draw of the VSD. See "VSD Air Compressor – Supporting Information with 40 to 50 hpbucket.xlsx" for more information.

Baseline Compressor	Compressor Factor (≤ 40 hp) ⁴⁹	$\frac{\text{Compressor Factor}}{(>40 - < 50\text{hp})^{50}}$	$\frac{\text{Compressor Factor}}{(50-200 \text{ hp})^{51}}$
Modulating w/ Blowdown	0.890	0.886	0.863
Load/No-Load w/ 1 Gallon/CFM	0.909	0.905	<u>0.887</u>
Load/No-Load w/ 3 Gallon/CFM	0.831	0.827	<u>0.811</u>
Load/No-Load w/ 5 Gallon/CFM	0.806	0.802	<u>0.786</u>

Shift	Hours
Single shift (8/5)	1976 hours: 7 AM – 3 PM, weekdays, minus some holidays and scheduled down
Single shift (8/3)	time
2-shift (16/5)	3952 hours: 7AM – 11 PM, weekdays, minus some holidays and scheduled
2-Sillit (10/3)	down time
2 shift (24/5)	5928 hours: 24 hours per day, weekdays, minus some holidays and scheduled
3-shift (24/5)	down time
4 shift (24/7)	8320 hours: 24 hours per day, 7 days a week minus some holidays and scheduled
4-shift (24/7)	down time
<u>Unknown /</u>	5702 hours: Weighting of 16% single shift, 23% two shift, 25% three shift and
Weighted average ⁵²	36% continual
weighted average ³²	30% CONUNUAL

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor = 0.0001379439

MEASURE CODE:

⁴⁹ Compressor factors were developed using DOE part load data for different compressor control types as well as load profiles from 50 facilities employing air compressors less than or equal to 40 hp. See "VSD Air Compressor – Supporting Information with 40 to 50 hpb ucket.xlsx" for more information.

⁵⁰ Compressor factors for the size range between 40 and 50 hp were interpolated from data used to derive the compressor factor for the other size ranges. See "VSD Air Compressor – Supporting Information with 40to 50 hpbucket.xlsx" for more information.

⁵¹ Compressor factors for this size range were developed using DOE part-load data for different compressor control types as we as load profiles from 45 compressors and 20 facilities. This data comes from ComEd Custom and Indsustrial Systems programs. The compressors were filtered to reflect only rotary screw compressors, between 50 and 200 hp, and operating a minimum of hours per day, Additionally, compressors with clear and consistent baseload profiles were excluded from this analysis. See "VSD Air Compressor – Supporting Information with 40to 50 hpbucket.xlsx" for more information.

⁵² Weighting based on DOE evaluation of the Compressed Air Challenge, section 2.1.5 Facility Operating Schedules.

⁵³ Ameren Missouri Coincident Peak Demand Factor for Commercial Compressed Air. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

2.3 Food Service

2.3.1 Combination Oven

DESCRIPTION

This measure applies to full or half-sized electric ENERGY STAR® combination ovens with a pan capacity ≥ 5 and ≤ 20 and to full or half-sized natural gas fired ENERGY STAR® combination ovens with a pan capacity ≥ 6 installed in a commercial kitchen. Combination ovens combine the function of hot air convection (convection mode), saturated and superheated steam heating (steam mode), and combination convection/steam mode for moist heating, to perform steaming, baking, roasting, re-thermalizing, and proofing of various food products. ENERGY STAR® certified combination ovens are approximately 20% more efficient than standard ovens.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be an ENERGY STAR® certified combination oven meeting idle energy rate (kW or Btu/hr) and cooking efficiency (%) limits, as determined by fuel type, operation mode (steam or convection), and pan capacity.

ENERGY STAR® Requirements (Version 2.2, Effective October 7, 2015)

Fuel Type	Operation	Idle Rate (Btu/hr for Gas, kW for Electric)	Cooking-Energy Efficiency (%)
Natural Gas	Steam Mode	≤ 200P+6,511	≥ 41
Natural Gas	Convection Mode	$\leq 150P+5,425$	≥ 56
Electric	Steam Mode	≤ 0.133P+0.6400	≥ 55
Elecuic	Convection Mode	$\leq 0.080P + 0.4989$	≥ 76

Note: P = Pan capacity as defined in Section 1.T of the Commercial Ovens Program Requirements Version 2.2.54

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric or natural gas combination oven that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years. 55

DEEMED MEASURE COST

⁵⁴ Pan capacity is defined as the number of steam table pans the combination oven is able to accommodate as per the ASTM F1495-05 standard specification.

https://www.energystar.gov/sites/default/files/asset/document/commercial_kitchen_equipment_calculator.xlsx

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https://www.energystar.gov/sites/default/files/Commercial%20Ovens%20Final%20Version%202.2%20Specification.pdf
https://www.energystar.gov/sites/default/files/asset/document/commercial_kitchen_equipment_calculator.xlsx

55 Lifetime from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "ESTC resear

⁵⁵ Lifetime from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "FSTC research on available models, 2009."

The incremental capital cost for this measure is \$4,300.56

LOADSHAPE

Cooking BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation for an electric combination oven below. 57

 $\Delta kWh = (\Delta CookingEnergy_{ConvElec} + \Delta CookingEnergy_{SteamElec} + \Delta IdleEnergy_{ConvElec} + \Delta IdleEnergy_{SteamElec}) * Days/1,000$

Where:

Days

ΔCookingEnergy_{ConvElec} = Difference in cooking energy between baseline and efficient

combination oven in convection mode

= FoodCooked_{Elec} * (EFOOD_{ConvElec} / ElecEFF_{ConvBase} -

EFOODConvElec / ElecEFFConvEE) * %Conv

ΔCookingEnergy_{SteamElec} = Difference in cooking energy between baseline and efficient

combination oven in steam mode

= FoodCooked_{Elec} * (EFOOD_{SteamElec} / ElecEFF_{SteamBase} -

EFOODSteamElec / ElecEFFSteamEE) * %Steam

 Δ IdleEnergyConvElec = Difference in idle energy between baseline and efficient

combination oven in convection mode

 $= ((ElecIDLE_{ConvBase} * ((Hours - FoodCooked_{Elec} / ElecPC_{ConvBase})))$

* %Conv)) - (ElecIDLEConvEE * ((Hours - FoodCookedElec

/ElecPCconvEE) * %Conv)))

ΔIdleEnergy_{SteamElec} = Difference in idle energy between baseline and efficient

combination oven in steam mode

= [(ElecIDLEsteamBase * ((Hours – FoodCookedElec / ElecPCsteamBase)

* %Steam)) - (ElecIDLESteamEE * ((Hours - FoodCookedElec /

ElecPC_{SteamEE}) * %_{Steam}))] = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor

FoodCooked_{Elec} = Food cooked per day for electric combination oven

= Custom, or, if unknown, use 200 lbs if P <15 or 250 lbs if P \geq 15

EFOOD_{convElec} = ASTM energy to food for electric combination oven in

convection mode

ElecEff = 73.2 Wh/lb

⁵⁶ Nicor Gas Energy Efficiency Plan 2011-2014. Revised Plan Filed Pursuant to Order Docket 10-0562, May 27, 2011.

⁵⁷ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

%Conv

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= Cooking energy efficiency of electric combination oven

= Custom or if unknown, use values from table below

= Percentage of time in convection mode = Custom or, if unknown, use 50%

EFOOD_{SteamElec} = ASTM energy to food for electric combination oven in steam

mode

=30.8 Wh/lb

%steam = Percentage of time in steam mode

= 1 - %conv

 $\label{eq:elecIDLE} \mbox{ElecIDLE}_{\mbox{\footnotesize Base}} \qquad = \mbox{Idle energy rate (W) of baseline electric combination oven}$

= Custom or, if unknown, use values from table below

Hours = Average daily hours of operation

= Custom or, if unknown, use 12 hours per day

ElecPC_{Base} = Production capacity (lbs/hr) of baseline electric combination

oven

= Custom or, if unknown, use values from table below

ElecIDLE_{ConvEE} = Idle energy rate of ENERGY STAR® electric combination oven

in convection mode

= (0.08 *P + 0.4989) *1,000

ElecPC_{EE} = Production capacity (lbs/hr) of ENERGY STAR® electric

combination oven

= Custom or, if unknown, use values from table below

ElecIDLE_{SteamEE} = Idle energy rate of ENERGY STAR® electric combination oven

in steam mode

=(0.133*P+0.64)*1,000

	Base	EE
ElecEFF _{Conv}	72%	76%
ElecEFF _{Steam}	49%	55%

Pan Capacity	Convection Mode (ElecIDLE _{ConvBase)}	Steam Mode (ElecIDLE _{SteamBase)}
< 15	1,320	5,260
≥ 15	2,280	8,710

Pan Capacity	Convection Mode (ElecPC _{ConvBase)}	Steam Mode (ElecPC _{SteamBase)}	
< 15	79	126	
>15	166	295	

Pan Capacity	Convection Mode (ElecPC _{ConvEE})	Steam Mode (ElecPC _{SteamEE)}	
< 15	119	177	
≥ 15	201	349	

SUMMER COINCIDENT PEAK DEMAND SAVINGS

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 $\Delta k = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001998949^{58}$

Other variables as defined above.

NATURAL GAS ENERGY SAVINGS

Custom calculation for a gas combination oven below:59

 $\Delta Therms = (\Delta Cooking Energy_{ConvGas} + \Delta Cooking Energy_{SteamGas} + \Delta Idle Energy_{ConvGa} + \Delta Idle Energy_{SteamGas}) * Days/100,000$

Where:

nere.	
$\Delta Cooking Energy_{ConvGas}$	= Difference in cooking energy between baseline and efficient combination oven in convection mode = FoodCooked _{Gas} * (EFOOD _{ConvGas} / GasEFF _{ConvBase} EFOOD _{ConvGas} / GasEFF _{ConvEE}) * %Conv
$\Delta Cooking Energy_{SteamGas}$	= Difference in cooking energy between baseline and efficient combination oven in steam mode = FoodCooked _{Gas} * (EFOOD _{SteamGas} / GasEFF _{SteamBase} -
$\Delta Idle Energy {\tt ConvGas}$	EFOOD _{SteamGas} / GasEFF _{SteamEE}) * % _{Steam} = Difference in idle energy between baseline and efficient combination oven in convection mode = ((GasIDLE _{ConvBase} * ((Hours - FoodCooked _{Gas} /GasPC _{ConvBase}) * % _{Conv})) - (GasIDLE _{ConvEE} * ((Hours - FoodCooked _{Gas} /GasPC _{ConvEE}) * //GasPC _{ConvEE}) * % _{Conv})))
$\Delta Idle Energy {\it Steam Gas}$	= Difference in idle energy between baseline and efficient combination oven in steam mode = [(GasIDLE _{SteamBase} * ((Hours – FoodCooked _{Gas} / GasPC _{SteamBase}) * % _{Steam})) - (GasIDLE _{SteamEE} * ((Hours - FoodCooked _{Gas} / GasPC _{SteamEE}) * % _{Steam}))]
100,000 FoodCooked _{Gas}	= Btu to therms conversion factor = Food cooked per day for gas combination oven = Custom, or, if unknown, use 200 lbs if $P < 15$, 250 lbs if $15 \le P$ 30, or 400 lbs if $P \ge 30$
EFOODConvGas	= ASTM energy to food for gas combination oven in convection mode = 250 Btu/lb

^{58 2016} Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

⁵⁹ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

GasPCEE

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GasEff = Cooking energy efficiency of gas combination oven

= Custom or, if unknown, use values from table below

EFOOD_{SteamGas} = ASTM energy to food for gas combination oven in steam mode

= 105 Btu/lb

GasIDLE_{Base} = Idle energy rate (Btu/hr) of baseline gas combination oven

= Custom or, if unknown, use values from table below

GasPC_{Base} = Production capacity (lbs/hr) of baseline gas combination oven

= Custom or, if unknown, use values from table below

GasIDLE_{ConvEE} = Idle energy rate of ENERGY STAR® gas combination oven in

convection mode

= 150*P + 5,425 = Production capacity (lbs/hr) of ENERGY STAR® gas

combination oven

= Custom or, if unknown, use values from table below

GasIDLE_{SteamEE} = Idle energy rate of ENERGY STAR® gas combination oven in

steam mode = 200*P +6,511

Other variables as defined above.

	Base	EE
GasEFF _{Conv}	52%	56%
GasEFF _{Steam}	39%	41%

Dan Canasity	Convection Mode	Steam Mode
Pan Capacity	(GasIDLE _{ConvBase)}	(GasIDLE _{SteamBase)}
< 15	8,747	18,656
15 ≤ P 30	10,788	24,562
≥30	13,000	43,300

Pan Capacity	Convection Mode	Steam Mode
I an Capacity	(GasPC _{ConvBase)}	(GasPC _{SteamBase)}
< 15	125	195
$15 \le P \ 30$	176	211
≥30	392	579

Pan Capacity	Convection Mode (GasPC _{ConvEE)}	Steam Mode (GasPC _{SteamEE)}	
< 15	124	172	
15 ≤ P 30	210	277	
≥30	394	640	

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.3.2 Commercial Steam Cooker

DESCRIPTION

This measure applies to electric or natural gas fired ENERGY STAR® steam cookers installed in a commercial kitchen. Commercial steam cookers contain compartments where steam energy is transferred to food by direct contact. ENERGY STAR® certified steam cookers have shorter cook times, higher production rates, and reduced heat loss due to better insulation and more efficient steam delivery.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be an ENERGY STAR® certified steam cooker meeting idle energy rate (W or Btu/hr) and cooking efficiency (%) limits, as determined by fuel type and pan capacity.

ENERGY STAR® Requirements (Version 1.2, Effective August 1, 2003)

Electric Efficienc		cy Requirements	Natural Gas Efficiency	
Pan Capacity	Idle Energy Rate	Cooking	Idle Energy Rate	Cooking
	Idle Energy Rate	Efficiency		Efficiency
3-pan	≤ 400 W		≤ 6,250 Btu/hr	
4-pan	≤ 530 W	> 500/	≤ 8,350 Btu/hr	> 200/ NI/A
5-pan	≤ 670 W	≥ 50%	≤ 10,400 Btu/hr	≥ 38% N/A
6-pan and larger	≤ 800 W		≤ 12,500 Btu/hr	

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric or natural gas steam cooker that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years.60

DEEMED MEASURE COST

Actual incremental cost for this measure should be used. If actuals are unavailable use \$4,150.61

⁶⁰ Lifetime from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "FSTC research on available models, 2009."

http://www.energystar.gov/buildings/sites/default/uploads/files/commercial_kitchen_equipment_calculator.xlsx 61 Ameren Missouri Technical Resource Manual – Effective January 1, 2018.

LOADSHAPE

Cooking BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation for an electric steam cooker below; otherwise use deemed value from the table that follows.⁶²

 $\Delta kWh = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/1,000$

Where:

ΔIdleEnergy = Difference in idle energy between baseline and efficient steam cooker

 $= [(1-SteamMode)*(IdleRate_{Base} + SteamMode* Production_{Base}* Pans *EFOOD/Eff_{Base})* (Hours - FoodCooked/(Production_{Base}* Pans))] \\ - [(1-SteamMode)*(IdleRate_{ESTAR} + SteamMode* Production_{ESTAR}* Pans* EFOOD/Eff_{ESTAR})* (Hours - FoodCooked/(Production_{ESTAR}*)* (Ho$

Pans))]

ΔCookingEnergy = Difference in cooking energy between baseline and efficient steam

cooker

= (FoodCooked * EFOOD/ EffBase) – (FoodCooked * EFOOD/

Effestar)

Days = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor SteamMode = Time (%) in constant steam mode = Custom or, if unknown, use 40%

IdleRateBase = Idle energy rate (W) of baseline electric steam cooker

 $= 1,100 \text{ W}^{63}$

IdleRate_{ESTAR} = Idle energy rate (W) of ENERGY STAR® electric steam cooker

= Custom or, if unknown, use value from table below as determined by

pan capacity

Production_{Base} = Production capacity (lb/hr) per pan of baseline electric steam cooker

= 23.3 lb/hr

Production_{ESTAR} = Production capacity (lb/hr) per pan of ENERGY STAR[®] electric

steam cooker

= Custom or, if unknown, use 16.7 lb/hr

Pans = Pan capacity of steam cooker

= Custom or, if unknown, use 6 pans

EFOOD = ASTM energy to food

⁶² Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

⁶³ Idle energy rate for baseline steam cookers is the average of rates provided by ENERGY STAR® for steam generator and boiler-based cookers.

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= 30.8 Wh/lb

 Eff_{Base} = Cooking efficiency (%) of baseline electric steam cooker⁶⁴

= Cooking efficiency (%) of ENERGY STAR® electric steam cooker Effestar

= Custom or, if unknown, use 50%

Hours = Average daily hours of operation

= Custom or, if unknown, use 12 hours per day

FoodCooked = Food cooked per day (lbs)

= Custom or, if unknown, use 100 pounds

Pan Capacity	IdleRate _{ESTAR}
3	400
4	530
5	670
6	800
10	800

Savings for all pan capacities are presented in the table below.

Energy Consumption of Electric Steam Cookers							
Pan Capacity	kWh _{Base}	kWh _{ESTAR}	Savings (kWh)				
3	18,438.9	7,637.6	10,801.3				
4	23,018.6	9,784.1	13,234.5				
5	27,563.8	11,953.8	15,609.9				
6	32,091.7	14,100.1	17,991.6				
10	50,134.5	21,384.3	28,750.1				
Average	30,249.5	12,972.0	17,277.5				

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $=0.0001998949^{65}$

Other variables as defined above.

NATURAL GAS ENERGY SAVINGS

⁶⁴ Cooking efficiency for baseline steam cookers is the average of efficiencies provided by ENERGY STAR® Commercial Kitchen Equipment Savings Calculator for steam generator and boiler-based cookers.

65 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri

²⁰¹⁶ Appendix E - End Use Shapes and Coincident Factors.pdf."

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Custom calculation for a natural gas steam cooker below; otherwise use deemed value from the table that follows.⁶⁶

 $\Delta Therms = (\Delta IdleEnergy + \Delta CookingEnergy)*Days/100,000$

Where:

 Δ IdleEnergy = [(1 - SteamMode) *(IdleRate_{Base} + SteamMode * Production_{Base} *

Pans *EFOOD/Eff_{Base})* (Hours – FoodCooked/(Production_{Base} * Pans))] – [(1 – SteamMode) *(IdleRateestar + SteamMode * Productionestar * Pans * EFOOD/Eff_{ESTAR})* (Hours – FoodCooked/Productionestar *

Pans)]

 Δ CookingEnergy = (FoodCooked * EFOOD/ Eff_{Base}) – (FoodCooked * EFOOD /

Effestar)

100,000 = Btu to therms conversion factor

IdleRate_{Base} = Idle energy rate (Btu/hr) of baseline gas steam cooker

 $= 16,500 \text{ Btu/hr}^{67}$

IdleRate_{ESTAR} = Idle energy rate (Btu/hr) of ENERGY STAR® gas steam cooker

= Custom or, if unknown, use value from table below as determined by

pan capacity

Production_{Base} = Production capacity (lb/hr) per pan of baseline gas steam cooker

= 23.3 lb/hr

Production_{ESTAR} = Production capacity (lb/hr) per pan of ENERGY STAR® gas steam

cooker

= Custom or, if unknown, use 20 lb/hr

EFOOD = ASTM energy to food

= 105 Btu/lb

Eff_{Base} = Cooking efficiency (%) of baseline gas steam cooker⁶⁸

= 16.5%

= Cooking efficiency (%) of ENERGY STAR® gas steam cooker

Effestar = Custom or if unknown, use 38%

Other variables as defined above.

Pan Capacity	IdleRate _{ESTAR}		
3	6,250		
5	10,400		
6	12,500		
10	12,500		

Savings for all pan capacities are presented in the table below.

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⁶⁶ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

⁶⁷ Idle energy rate for baseline steam cookers is the average of rates provided by ENERGY STAR® for steam generator and boiler-based cookers.

⁶⁸ Cooking efficiency for baseline steam cookers is the average of efficiencies provided by ENERGY STAR® for steam generator and boiler-based cookers.

Energy Consumption of Gas Steam Cookers						
Pan Capacity	Therms _{Base}	Therms _{ESTAR}	Savings (Therms)			
3	1,301.5	492.8	808.7			
5	1,842.1	795.7	1,046.4			
6	2,107.2	947.8	1,159.4			
10	3,157.4	1,344.5	1,812.9			
Average	1,996.0	845.0	1,150.0			

WATER IMPACT DESCRIPTIONS AND CALCULATION

Custom calculation below; otherwise use deemed value of 134,412.0 gallons per year.⁶⁹ Savings are the same for electric and gas steam cookers.

 $\Delta Water = (WaterUse_{Base} - WaterUse_{ESTAR}) * Hours * Days$

Where:

WaterUse_{Base} = Water use (gal/hr) of baseline steam cooker

=40 gal/hr

WaterUse_{ESTAR} = Water use (gal/hr) of ENERGY STAR[®] steam cooker⁷⁰

= Custom or, if unknown, use 9.3 gal/hr

Other variables as defined above

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

 $^{^{69}}$ Algorithms and assumptions derived from ENERGY STAR $^{\circledR}$ Commercial Kitchen Equipment Savings Calculator.

⁷⁰ Water use for ENERGY STAR® steam cookers is the average of water use values provided by ENERGY STAR® for steam generator, boiler-based, and boiler-less cookers.

2.3.3 Fryer

DESCRIPTION

This measure applies to electric or natural gas fired ENERGY STAR® certified fryers installed in a commercial kitchen. ENERGY STAR® fryers offer shorter cook times and higher production rates through advanced burner and heat exchanger designs. Fry pot insulation reduces standby losses, resulting in lower idle energy rates. Standard-sized ENERGY STAR® fryers are up to 30% more efficient, and large-vat ENERGY STAR® fryers are up to 35% more efficient, than standard fryers.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be an ENERGY STAR® certified fryer meeting idle energy rate (W or Btu/hr) and cooking efficiency (%) limits, as determined by both fuel type and fryer capacity (standard versus large vat).

ENERGY STAR® Requirements (Version 2.0, Effective April 22, 2011)

Entertain itequirements	, ersion 200, 2010001, 6 11pm 22, 2011)				
	Electric Efficiency Requirements		Natural Gas Efficiency Requirements		
Fryer Capacity	Idle Energy Rate	Cooking Efficiency Consumption	Idle Energy Rate	Cooking Efficiency Consumption	
Standard Open Deep-Fat Fryer	≤ 1,000 W	≥ 80%	≤ 9,000 Btu/hr	> 50%	
Large Vat Open Deep-Fat Fryer	≤1,100 W		≤ 12,000 Btu/hr	≥ 30%	

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric or natural gas fryer that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years.71

DEEMED MEASURE COST

The incremental capital cost for this measure is \$210 for standard electric, \$0 for large vat electric, \$0 for standard gas, and \$1,120 for large vat gas fryers.⁷²

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 $^{^{71}}$ Lifetime from ENERGY STAR* Commercial Kitchen Equipment Savings Calculator, which cites reference as "FSTC research on available models, 2009."

 $[\]underline{https://www.energystar.gov/sites/default/files/asset/document/commercial_kitchen_equipment_calculator.xlsx.}$

⁷² Measure costs from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "EPA research using AutoQuotes, 2012."

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation for an electric fryer below; otherwise use deemed value of 952.3 kWh for standard fryers and 2,537.9 kWh for large vat fryers.⁷³

 $\Delta kWh = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/1,000$

Where:

ΔIdleEnergy = Difference in idle energy between baseline and efficient fryer

= (ElecIdleBase* (Hours – FoodCooked/ElecPCBase)) –

ElecIdleESTAR * (Hours – FoodCooked/ElecPCESTAR))

ΔCookingEnergy = Difference in cooking energy between baseline and efficient fryer

= (FoodCooked * EFOOD_{Elec}/ ElecEff_{Base}) – (FoodCooked *

EFOODElec/ElecEffestar)

Days = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor

ElecIdle_{Base} = Idle energy rate of baseline electric fryer

= 1,050 W for standard fryers and 1,350 W for large vat fryers

ElecIdle_{ESTAR} = Idle energy rate of ENERGY STAR® electric fryer

= Custom or, if unknown, use 1,000 W for standard fryers and 1,100 for

large vat fryers

Hours = Average daily hours of operation

= Custom or, if unknown, use 16 hours per day for a standard fryer and

12 hours per day for a large vat fryer

FoodCooked = Food cooked per day

= Custom or, if unknown, use 150 pounds

ElecPC_{Base} = Production capacity of baseline electric fryer

= 65 lb/hr for standard fryers and 100 lb/hr for large vat fryers

ElecPC_{ESTAR} = Production capacity of ENERGY STAR[®] electric fryer

= Custom or, if unknown, use 70 lb/hr for standard fryers and 110 lb/hr

for large vat fryers

 $EFOOD_{Elec}$ = ASTM energy to food

= 167 Wh/lb

ElecEff_{Base} = Cooking efficiency of baseline electric fryer

= 75% for standard fryers and 70% for large vat fryers = Cooking efficiency of ENERGY STAR[®] electric fryer

ElecEffestar = Custom or, if unknown, use 80% for both standard and large vat fryers

Other variables as defined above

⁷³ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001998949^{74}$

Other variables as defined above.

NATURAL GAS ENERGY SAVINGS

Custom calculation for a natural gas fryer below; otherwise use deemed value of 507.9 therms/yr for standard fryers and 415.1 therms/yr for large vat fryers.⁷⁵

 $\Delta Therms = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/100,000$

Where:

 $\Delta Idle Energy = (GasIdle_{Base}^* (Hours - FoodCooked/GasPC_{Base})) - (GasIdle_{ESTAR}^*)$

(Hours - FoodCooked/GasPC_{ESTAR}))

 Δ CookingEnergy = (FoodCooked * EFOOD_{Gas}/ GasEff_{Base}) – (FoodCooked *

EFOODGas/GasEffestar)

100,000 = Btu to therms conversion factor GasIdle_{Base} = Idle energy rate of baseline gas fryer

= 14,000 Btu/hr for standard fryers and 16,000 Btu/hr for large vat

fryers

GasIdle_{ESTAR} = Idle energy rate of ENERGY STAR® gas fryer

= Custom or, if unknown, use 9,000 Btu/hr for standard fryers and

12,000 Btu/hr for large vat fryers

GasPc_{Base} = Production capacity of baseline gas fryer

= 60 lb/hr for standard fryers and 100 lb/hr for large vat fryers

= Production capacity of ENERGY STAR® gas fryer

= Custom or, if unknown, use 65 lb/hr for standard fryers and 110 lb/hr

GasPcestar for large vat fryers

 $EFOOD_{Gas}$ = ASTM energy to food

= 570 Btu/lb

 $GasEff_{Base}$ = Cooking efficiency of baseline gas fryer

= 35% for both standard and large vat fryers

= Cooking efficiency of ENERGY STAR® gas fryer

GasEff_{ESTAR} = Custom or, if unknown, use 50% for both standard and large vat fryers

⁷⁴ 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

⁷⁵ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

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Other variables as defined above

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.3.4 Convection Oven

DESCRIPTION

This measure applies to either full or half-sized electric ENERGY STAR® convection ovens and to half sized natural gas fired ENERGY STAR® convection ovens installed in a commercial kitchen. Convection ovens are general purpose ovens that use fans to circulate hot, dry air over the food surface. ENERGY STAR® certified convection ovens are approximately 20% more efficient than standard ovens.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be an ENERGY STAR® certified convection oven meeting idle energy rate (kW or Btu/hr) and cooking efficiency (%) limits, as determined by both fuel type and oven capacity (full size versus half size).

ENERGY STAR® Requirements (Version 2.2, Effective October 7, 2015)

Oven Capacity Electric Efficiency Requi		Electric Efficiency Requirements		Efficiency nents
Oven Capacity	Idle Energy Rate	Cooking Efficiency	Idle Energy Rate	Cooking Efficiency
Full Size	≤1.60 kW	> 71%	≤ 12,000 Btu/hr	≥ 46%
Half Size	≤ 1.00 kW	≥ /170	N/A	N/A

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric or natural gas convection oven that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years.76

DEEMED MEASURE COST

The incremental capital cost for this measure is \$0.77

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Cooking BUS

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⁷⁶ Lifetime from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "FSTC research on available models, 2009."

https://www.energystar.gov/sites/default/files/asset/document/commercial_kitchen_equipment_calculator.xlsx.

⁷⁷ Measure cost from ENERGY STAR® which cites reference as "EPA research on available models using AutoQuotes, 2013."

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation for an electric convection oven below; otherwise use 1,938.5 kWh for fullsize ovens and 192.1 kWh for half-size ovens.78

 $\Delta kWh = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/1,000$

Where:

ΔIdleEnergy = Difference in idle energy between baseline and efficient convection

= (ElecIdle_{Base}* (Hours - FoodCooked/ElecPC_{Base})) - (ElecIdle_{ESTAR} *

(Hours -FoodCooked/ElecPCESTAR))

ΔCookingEnergy = Difference in cooking energy between baseline and efficient

convection oven

= (FoodCooked * EFOODElec/ ElecEffBase) - (FoodCooked *

EFOOD_{Elec}/ ElecEff_{ESTAR})

Days = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor

 $ElecIdle_{Base}$ = Idle energy rate of baseline electric convection oven

= 2,000 W for full-size ovens and 1,030 W for half-size ovens = Idle energy rate of ENERGY STAR® electric convection oven

ElecIdleESTAR = Custom or, if unknown, use 1,600 W for full-size ovens and 1,000

W for half-size ovens

Hours = Average daily hours of operation

= Custom or, if unknown, use 12 hours per day

FoodCooked = Food cooked per day

= Custom or, if unknown, use 100 pounds

= Production capacity of baseline electric convection oven = 90 lb/hr for full-size ovens and 45 lb/hr for half-size ovens

= Production capacity of ENERGY STAR® electric convection oven **ElecPC**ESTAR

= Custom or, if unknown, use 90 lb/hr for full-size ovens and 50 lb/hr

for half-size ovens

 $EFOOD_{Elec} \\$ = ASTM energy to food for electric convection oven

=73.2 Wh/lb

ElecEff_{Base} = Cooking efficiency of baseline electric convection oven

= 65% for full-size ovens and 68% for half-size ovens

ElecPC_{Base}

⁷⁸ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

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 $ElecEff_{ESTAR} \\$

- = Cooking efficiency of ENERGY STAR® electric convection oven = Custom or, if unknown, use 71% for full-size and half-size ovens

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SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $=0.0001998949^{79}$

Other variables as defined above.

NATURAL GAS ENERGY SAVINGS

Custom calculation for a natural gas convection oven below, otherwise use deemed value of 129.4 therms/yr.⁸⁰

 $\Delta Therms = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/100,000$

Where:

 $\Delta IdleEnergy = (GasIdle_{Base}* (Hours - FoodCooked/GasPC_{Base})) - (GasIdle_{ESTAR})$

* (Hours -FoodCooked/GasPC_{ESTAR}))

= (FoodCooked * EFOODGas/ GasEffBase) - (FoodCooked *

 $\Delta Cooking Energy$ EFOOD_{Gas}/ GasEff_{ESTAR}) 100,000 = Btu to therms conversion factor

GasIdle_{Base} = Idle energy rate of baseline gas convection oven

= 15,100 Btu/hr

GasIdle_{ESTAR} = Idle energy rate of ENERGY STAR® gas convection oven

= Custom or, if unknown, use 12,000 Btu/hr

GasPC_{Base} = Production capacity of baseline gas convection oven

=83 lb/hr

GasPC_{ESTAR} = Production capacity of ENERGY STAR[®] gas convection oven

= Custom or, if unknown, use 86 lb/hr

EFOOD_{Gas} = ASTM energy to food for gas convection oven

= 250 Btu/lb

GasEff_{Base} = Cooking efficiency of baseline gas convection oven

=44%

= Cooking efficiency of ENERGY STAR® gas convection oven

GasEffestar = Custom or, if unknown, use 46%

Other variables as defined above.

^{79 2016} Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

⁸⁰ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

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WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.3.5 Griddle

DESCRIPTION

This measure applies to electric or natural gas fired ENERGY STAR® certified griddles installed in a commercial kitchen. ENERGY STAR® commercial griddles achieve approximately 10% higher efficiency than standard griddles with strategies such as highly conductive or reflective plate materials and improved thermostatic controls.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure the installed equipment must be a new ENERGY STAR® electric or natural gas fired griddle meeting idle energy rate limits as determined by fuel type.

ENERGY STAR® Requirements (Version 1.2, Effective May 8, 2009 for natural gas and January 1, 2011 for electric griddles)

Electric Effici	ency Requirements	Natural Gas Eff	iciency Requirements
Idle Energy Rate	Cooking Efficiency Consumption	Idle Energy Rate	Cooking Efficiency Consumption
≤ 320 W/ft ² ≤ 1.00 kW	Reported	\leq 2,650 Btu/hr/ft ² N/A	Reported

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric or natural gas fired griddle that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years.81

DEEMED MEASURE COST

The incremental capital cost for this measure is 0 for an electric griddle and 360 for a gas griddle.

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Cooking BUS

Algorithm

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⁸¹ Lifetime from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "FSTC research on available models, 2009."

http://www.energystar.gov/buildings/sites/default/uploads/files/commercial_kitchen_equipment_calculator.xlsx

⁸² Measure costs from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator, which cites reference as "EPA research on available models using AutoQuotes, 2012."

http://www.energystar.gov/index.cfm?fuseaction=find_a_product.showProductGroup&pgw_code=COG.

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation for an electric griddle below; otherwise use deemed value of 1,910.4 kWh.83

 $\Delta kWh = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/1,000$

Where:

Hours

ΔIdleEnergy = Difference in idle energy between baseline and efficient griddle

= [(ElecIdle_{Base}* Width * Depth) * (Hours –

FoodCooked/ElecPC_{Base})] - [(ElecIdle_{ESTAR} * Width * Depth) *

(Hours – FoodCooked/ElecPC_{ESTAR}))

ΔCookingEnergy = Difference in cooking energy between baseline and efficient

griddle

= (FoodCooked * EFOOD_{Elec} / ElecEff_{Base}) – (FoodCooked *

Days = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor

 $ElecIdle_{Base}$ = Idle energy rate of baseline electric griddle

EFOOD_{Elec} / ElecEff_{ESTAR})

 $= 400 \text{ W/ft}^2$

= Idle energy rate of ENERGY STAR® electric griddle ElecRateestar

= Custom or, if unknown, use 320 W/ft²

Width = Griddle width

= Custom or, if unknown, use 3 feet

Depth = Griddle depth

> = Custom or, if unknown, use 2 feet = Average daily hours of operation

= Custom or, if unknown, use 12 hours per day

FoodCooked = Food cooked per day

= Custom or, if unknown, use 100 pounds

ElecPC_{Base} = Production capacity of baseline electric griddle

=35 lb/hr

ElecPCESTAR = Production capacity of ENERGY STAR® electric griddle

= Custom or, if unknown, use 40 lb/hr

 $EFOOD_{Elec} \\$ = ASTM energy to food

= 139 Wh/lb

ElecEff_{Base} = Cooking efficiency of baseline electric griddle

= Cooking efficiency of ENERGY STAR® electric griddle ElecEffestar

= Custom or, if unknown, use 70%

Other variables as defined above.

⁸³ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.000199894984

Other variables as defined above.

NATURAL GAS ENERGY SAVINGS

Custom calculation for a natural gas griddle below; otherwise use deemed value of 131.4 therms.⁸⁵

 $\Delta Therms = (\Delta IdleEnergy + \Delta CookingEnergy) * Days/100,000$

Where:

 Δ IdleEnergy = [GasIdle_{Base}* (Width * Depth) * (Hours –

FoodCooked/GasPC_{Base})] - [GasIdle_{ESTAR} * (Width * Depth) *

 $(Hours-FoodCooked/GasPC_{ESTAR})) \\$

 $\Delta CookingEnergy = (FoodCooked * EFOOD_{Gas}/ GasEff_{Base}) - (FoodCooked * FOOD_{Gas}/ GasEff_{Gas}) - (FoodCooked * FOOD_{Gas}/ GasEff_{Gas}/ GasEff_{Gas}) - (FoodCooked * FOOD_{Gas}/ GasEff_{Gas}/ GasEff_{Ga$

EFOOD_{Gas}/ GasEff_{ESTAR})

100,000 = Btu to therms conversion factor

GasIdle_{Base} = Idle energy rate of baseline gas griddle

 $= 3,500 \text{ Btu/hr/ft}^2$

GasIdle_{ESTAR} = Idle energy rate of ENERGY STAR® gas griddle

= Custom or, if unknown, use 2,650 Btu/hr/ft²

 $GasPC_{Base}$ = Production capacity of baseline gas griddle

=25 lb/hr

GasPC_{ESTAR} = Production capacity of ENERGY STAR® gas griddle

= Custom or, if unknown, use 45 lb/hr

 $EFOOD_{Gas}$ = ASTM energy to food

= 475 Btu/lb

GasEff_{Base} = Cooking efficiency of baseline gas griddle

= 32%

= Cooking efficiency of ENERGY STAR® gas griddle

GasEff_{ESTAR} = Custom or, if unknown, use 38%

Other variables as defined above.

^{84 2016} Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

⁸⁵ Algorithms and assumptions derived from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator.

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WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.3.6 Kitchen Demand Ventilation Controls

DESCRIPTION

Installation of commercial kitchen demand ventilation controls that vary the ventilation based on cooking load and/or time of day. This measure applies to the following program types: RF, NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure the installed equipment must be a control system that varies the exhaust rate of kitchen ventilation (exhaust and/or makeup air fans) based on the energy and effluent output from the cooking appliances (i.e., the more heat and smoke/vapors generated, the more ventilation needed). This involves installing a new temperature sensor in the hood exhaust collar and/or an optic sensor on the end of the hood that sense cooking conditions which allows the system to automatically vary the rate of exhaust to what is needed by adjusting the fan speed accordingly.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is kitchen ventilation that has constant speed ventilation motor.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT⁸⁶

The expected measure life is assumed to be 15 years.

MEASURE COST8680

The incremental capital cost for this measure is:

Measure Category	Incremental Cost (\$/HP)
DVC Control Retrofit	\$1,991
DVC Control New	\$1,991

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Cooking BUS

Algorithm

Calculation of Savings

Annual energy use was based on monitoring results from five different types of sites, as summarized in PG&E Food Service Equipment work paper.

Electric Energy Savings 8680

Measure Name	Annual Energy Savings per Unit (kWh/HP)
DVC Control Retrofit	4,197
DVC Control New	4,197

⁸⁶ Pacific Gas & Electric Company Work Paper PGECOFST116 Demand Ventilation Controls Revision # 4.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = kWh_{savings} * CF$$

Where:

= Electric energy savings, calculated above ΔkWh

= Summer peak coincidence demand (kW) to annual energy (kWh) factor CF

 $= 0.0001998949^{87}$

NATURAL GAS SAVINGS

 Δ Therms = CFM * HP* Annual Heating Load /(Eff(heat) * 100,000)

Where:

CFM = the average airflow reduction with ventilation controls per hood

=430 cfm/HP

HP = actual if known, otherwise assume 7.75 HP88

Annual Heating = Annual heating energy required to heat fan exhaust make-up air

Load dependent on location = Heating Efficiency Eff(heat)

= actual if known, otherwise assume 80%89

100,000 = conversion from Btu to Therm

Zone	Annual Heating Load (BTU/cfm)
Missouri Average90	137,000

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

Measure Code:

⁸⁷ See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

^{88 &}quot;Illinois Statewide Technical Reference Manual for Energy Efficiency Version 6.0, Volume 2: Commercial and Industrial Measures," Section 4.2.16, Kitchen Demand Ventilation Controls; https://s3.amazonaws.com/ilsag/IL-

TRM Effective 010118 v6.0 Vol 2 C and I 020817 Final.pdf

89 "Illinois Statewide Technical Reference Manual for Energy Efficiency Version 6.0, Volume 2: Commercial and Industrial Measures", Section 4.2.16, Kitchen Demand Ventilation Controls; https://s3.amazonaws.com/ilsag/IL-

TRM Effective 010118 v6.0 Vol 2 C and I 020817 Final.pdf

90 Used https://s3.amazonaws.com/ilsag/2020 IL-TRM Version 8.0 dated October-17-2019 Final Volumes 1
4 Compiled.pdf to compare savings values by weather zone from the IL TRM to zone-specific HDD values, and determined a linear relationship between Heating Load and HDD, then applied that linear relationship to HDD values (using base 60) for MO weather stations to estimate Heating Load values for zones in Ameren Missouri territory

2.3.7 Hot Food Holding Cabinet

DESCRIPTION

This measure applies to electric ENERGY STAR® certified hot food holding cabinets (HFHCs) installed in a commercial kitchen. ENERGY STAR® HFHCs achieve approximately 70% higher efficiency than standard models by incorporating better insulation which reduces heat loss, offers better temperature uniformity within the cabinet from top to bottom, and keeps the external cabinet cooler. In addition, many certified HFHCs may include additional energy saving devices such as magnetic door gaskets, auto-door closures, or dutch doors.

This measure was developed to be applicable to the following program type: TOS.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new ENERGY STAR® electric HFHC meeting idle energy rate limits as determined by product interior volume.

ENERGY STAR® Requirements (Version 2.0, Effective October 1, 2011)

Interior Volume (ft ³)	Idle Energy Consumption Rate (W)
0 < V < 13	≤ 21.5 V
$13 \le V < 28$	≤ 2.0 V + 254.0
28 ≤ V	≤ 3.8 V + 203.5

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new electric HFHC that is not ENERGY STAR® certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years.91

DEEMED MEASURE COST

Actual incremental costs should be used if available. If actual costs are unknown, assume \$1,783.

LOADSHAPE

Cooking BUS

Algorithm

CALCULATION OF SAVINGS

⁹¹ Lifetime from ENERGY STAR® Commercial Kitchen Equipment Calculator, which cites reference as "FSTC research on available models, 2009."

⁹² Ameren Missouri Technical Resource Manual – Effective January 1, 2018.

ELECTRIC ENERGY SAVINGS93

 $\Delta kWh = (IdleRate_{Base} - IdleRate_{EE}) * Hours * Days/1,000$

Where:

IdleRate_{Base} = Idle energy rate (W) of baseline HFHC

=40 * V

V = Interior volume (ft^3) of new HFHC

= Custom

IdleRate_{ESTAR} = Idle energy rate (W) of ENERGY STAR® HFHC

= See table below for idle energy rates based on interior volume

Hours = Average daily hours of operation

= Custom or, if unknown, use 15 hours per day

Days = Annual days of operation

= Custom or, if unknown, use 365.25 days per year

1,000 = Wh to kWh conversion factor

Interior Volume (ft ³)	Idle Energy Consumption Rate (W)
0 < V < 13	21.5 * V
13 ≤ V < 28	(2.0 * V) + 254.0
28 ≤ V	(3.8 * V) + 203.5

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

 Δ kWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001998949^{94}$

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

 $^{^{93}}$ Algorithms and assumptions derived from Commercial Kitchen Equipment Calculator.

⁹⁴ 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

MEASURE CODE:

2.3.8 Pre-Rinse Spray Valve

DESCRIPTION

Pre-rinse valves use a spray of water to remove food waste from dishes prior to cleaning in a dishwasher. More efficient spray valves use less water, thereby reducing water consumption, water heating cost, and waste water (sewer) charges. Pre-rinse spray valves include a nozzle, squeeze lever, and dish guard bumper. The primary impacts of this measure are water savings. Reduced hot water consumption saves either natural gas or electricity, depending on the type of energy the hot water heater uses.

This measure was developed to be applicable to the following program types: TOS, RF, and DI.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the new or replacement pre-rinse spray nozzle must use less than 1.6 gallons per minute.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment will vary based on the delivery method and is defined below:

Time of Sale	Retrofit, Direct Install
The baseline equipment is	Actual existing flow rates should be used when possible. If
assumed to be 1.6 gallons per	unknown, baseline can be assumed to be 2.23 gallons per minute. ⁹⁵
minute. The Energy Policy Act of	If existing pre-rinse spray valve flow rate is unknown, then existing
2005 sets the maximum flow rate	pre-rinse spray valve must have been installed prior to 2006. The
for pre-rinse spray valves at 1.6	Energy Policy Act of 2005 sets the maximum flow rate for pre-rinse
gallons per minute at 60 pounds	spray valves at 1.6 gallons per minute at 60 pounds per square inch
per square inch of water pressure	of water pressure when tested in accordance with ASTM F2324-03.
when tested in accordance with	This performance standard went into effect January 1, 2006.
ASTM F2324-03. This	However, field data shows that not all nozzles in use have been
performance standard went into	replaced with the newer flow rate nozzle. Products predating this
effect January 1, 2006.	standard can use up to five gallons per minute.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 5 years.⁹⁶

DEEMED MEASURE COST

MEEIA 2019-21 Plan

⁹⁵ Verification measurements taken at 195 installations showed average pre flowrates of 2.23 gallons per minute. IMPACT AND PROCESS EVALUATION FINAL REPORT for CALIFORNIA URBAN WATER CONSERVATION COUNCIL 2004-5 PRERINSE SPRAY VALVE INSTALLATION PROGRAM (PHASE 2) (PG&E Program # 1198-04; SoCalGas Program 1200-04) ("CUWCC Report," Feb 2007).

⁹⁶ Consistent with Ameren Missouri MEEIA 2016-18 and KCPL TRM assumptions.

When available, the actual cost of the measure should be used. If unknown, a default value of $$92.90^{97}$ may be assumed.

LOADSHAPE

Cooking BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS (NOTE WATER SAVINGS MUST FIRST BE CALCULATED)

```
\Delta kWH = \Delta Gallons * 8.33 * 1 * (T_{out} - T_{in}) * (1/EFF_{Elec}) / 3,413
```

Where:

 Δ Gallons = amount of water saved as calculated below in Water Impact Calculation

8.33 = specific mass in pounds of one gallon of water (lbm/gal)

 $\begin{array}{ll} 1 & = Specific \ heat \ of \ water: \ 1 \ Btu/lbm/^\circ F \\ T_{out} & = Water \ Heater \ Outlet \ Water \ Temperature \\ \end{array}$

= Custom, otherwise assume Tin + 70°F temperature rise from Tin⁹⁸

 T_{in} = Inlet Water Temperature

= Custom, otherwise assume 57.9F99

EFF_{Elec} = Efficiency of electric water heater supplying hot water to pre-rinse spray

valve

=Custom, otherwise assume 97%¹⁰⁰

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001998949^{101}$

NATURAL GAS ENERGY SAVINGS

⁹⁷Average of costs recognized by Ameren Missouri (\$85.8) and KCPL (\$100).

⁹⁸ If unknown, assume a 70 degree temperature rise from Tin per Food Service Technology Center calculator assumptions to account for variations in mixing and water heater efficiencies.

⁹⁹ Using 40" deep soil temp as a proxy at Powell Gardens SCAN site. Average by month of available data from 3/28/02–10/11/14: 12 month average is 57.898. http://www.wcc.nrcs.usda.gov/nwcc/site?sitenum=2061.

¹⁰⁰ This efficiency value is based on IECC 2012/2015 performance requirement for electric resistant water heaters rounded without the slight adjustment allowing for reduction based on size of storage tank.

^{101 2016} Ameren Missouri Coincident Peak Demand Factor for Commercial Electric Cooking. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

$$\Delta$$
Therms = Δ Gallons * 8.33 * 1 * (T_{out} - T_{in}) * (1/EFF_{Gas}) / 100,000

Where:

EFF_{Gas} = Efficiency of gas water heater supplying hot water to pre-rinse

spray valve

= Custom, otherwise assume 80%¹⁰²

Other variables as described above.

WATER IMPACT CALCULATION

FLOeff

$$\Delta Gallons = (FLO_{base} - FLO_{eff}) * 60 * HOURS_{day} * DAYS_{year}$$

Where:

FLO_{base} = Base case flow in gallons per minute (gal/min). Use actual when

appropriate if available, otherwise use values in table below. = Efficient case flow in gallons per minute (gal/min). Use actual

flow rate if known, otherwise use values in table below.

60 = Minutes per hour

 $HOURS_{day}$ = Hours per day that the pre-rinse spray valve is used at the site,

custom, otherwise use values in the table below. 103

DAYS_{year} = Days per year pre-rinse spray valve is used at the site, custom,

otherwise 312 days/yr based on assumed 6 days/wk x 52 wk/yr =

312 day/yr.

Parameter	Time of Sale	Retrofit, Direct Install
FLO _{base}	1.6 gal/min ¹⁰⁴	2.23 gal/min ¹⁰⁵
FLO _{eff}	1.06 gal/min ¹⁰⁶	1.06 gal/min

Application	HOURS _{day}
Small, quick- service restaurants	1
Medium-sized casual dining restaurants	1.5
Large institutional establishments with cafeteria	3

¹⁰² IECC 2012/2015, Table C404.2, Minimum Performance of Water-Heating Equipment.

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¹⁰³ Hours primarily based on PG& E savings estimates, algorithms, sources (2005), Food Service Pre-Rinse Spray Valves.

¹⁰⁴ The baseline equipment is assumed to be 1.6 gallons per minute. The Energy Policy Act (EPAct) of 2005 sets the maximum flow rate for pre-rinse spray valves at 1.6 gallons per minute at 60 pounds per square inch of water pressure when tested in accordance with ASTM F2324-03. This performance standard went into effect January 1, 2006.

www1.eere.energy.gov/femp/pdfs/spec_prerinsesprayvavles.pdf.

105 Verification measurements taken at 195 installations showed average pre flowrates of 2.23 gallons per minute. IMPACT AND PROCESS EVALUATION FINAL REPORT for CALIFORNIA URBAN WATER CONSERVATION COUNCIL 2004-5 PRERINSE SPRAY VALVE INSTALLATION PROGRAM (PHASE 2) (PG&E Program # 1198-04; SoCalGas Program 1200-04) ("CUWCC Report," Feb 2007).

^{106 1.6} gallons per minute used to be the high efficiency flow, but more efficient spray valves are available ranging down to 0.64 gallons per minute per Federal Energy Management Program which references the Food Services Technology Center web site with the added note that even more efficient models may be available since publishing the data. The average of the nozzles listed on the FSTC website is 1.06.

MEASURE CODE:

2.4 Hot Water

2.4.1 Low Flow Faucet Aerator

DESCRIPTION

This measure relates to the direct installation of a low flow faucet aerator in a commercial building. Expected applications include small business, office, restaurant, or motel. For multifamily or senior housing, the residential low flow faucet aerator should be used.

This measure was developed to be applicable to the following program type: DI.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure the installed equipment must be an energy efficient faucet aerator, for bathrooms rated at 1.5 gallons per minute (GPM) or less, or for kitchens rated at 2.2 GPM or less. Savings are calculated on an average savings per faucet fixture basis.

DEFINITION OF BASELINE EQUIPMENT

The baseline condition is assumed to be a standard bathroom faucet aerator rated at 2.25 GPM or more, or a standard kitchen faucet aerator rated at 2.75 GPM or more.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 9 years.¹⁰⁷

DEEMED MEASURE COST

The incremental cost for this measure is \$8.00¹⁰⁸ or program actual.

LOADSHAPE

Water Heating BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 ¹⁰⁷ Table C-6, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates,
 June 2007. "http://neep.org/uploads/EMV%20Forum/EMV%20Studies/measure_life_GDS%5B1%5D.pdf."
 108 Direct-install price per faucet assumes cost of aerator and install time. (2011, Market research average of \$3 and assess and install time of \$5 (20min @ \$15/hr).

Note these savings are per faucet retrofitted. 109

 $\Delta kWh \ = \%ElectricDHW * ((GPM_{base} - GPM_{low}) / GPM_{base}) * Usage * EPG_{electric} * ISR$

Where:

%ElectricDHW = proportion of water heating supplied by electric resistance heating

(see values in table below)

GPM_{base} = Average flow rate, in gallons per minute, of the baseline faucet

"as-used"

= 1.2¹¹⁰ or custom based on metering studies¹¹¹

GPM_{low} = Average flow rate, in gallons per minute, of the low-flow faucet

erator "as-used"

= 0.94¹¹² or custom based on metering studies¹¹³

Usage = Estimated usage of mixed water (mixture of hot water from water

heater line and cold-water line) per faucet (gallons per year)

= If data is available to provide a reasonable custom estimate it should be used, if not use the defaults in the table below (or

substitute custom information into the calculation):

EPG_{electric} = Energy per gallon of mixed water used by faucet (electric water

heater)

= $(8.33 * 1.0 * (WaterTemp - SupplyTemp)) / (RE_{electric} * 3412)$ = (8.33 * 1.0 * (90 - 57.9)) / (0.98 * 3412) = 0.0800 kWh/gal

8.33 = Specific weight of water (lbs/gallon)
1.0 = Heat Capacity of water (btu/lb-F)
WaterTemp = Assumed temperature of mixed water

¹⁰⁹ This algorithm calculates the amount of energy saved per aerator by determining the fraction of water consumption savings for the upgraded fixture. Due to the distribution of water consumption by fixture type, as well as the different number of fixtures in a building, several variables must be incorporated.

¹¹⁰ Representative baseline flow rate for kitchen and bathroom faucet aerators from sources 1, 2, 3, and 4. This accounts for all throttling and differences from rated flow rates. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use.

¹¹¹ Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow.

¹¹² Average retrofit flow rate for kitchen and bathroom faucet aerators from sources 1, 2, 3, and 4. This accounts for all throttling and differences from rated flow rates. Assumes all kitchen aerators at 2.2 gpm or less and all bathroom aerators at 1.5 gpm or less. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use. It is possible that programs installing low-flow aerators lower than the 2.2 gpm for kitchens and 1.5 gpm for bathrooms will see a lower overall average retrofit flow rate.

¹¹³ Measurement should be based on actual average flow consumed over a period of time rather than a onetime spot measurement for maximum flow. Studies have shown maximum flow rates do not correspond well to average flow rate due to occupant behavior which does not always use maximum flow.

= 90 F 114

SupplyTemp = Assumed temperature of water entering building

 $= 57.9 F^{115}$

RE_{electric} = Recovery efficiency of electric water heater

=98% 116

3412 = Converts Btu to kWh (Btu/kWh) ISR = In service rate of faucet aerators

= Assumed to be 1.0

DHW fuel	%Electric_DHW
Electric	100%
Fossil Fuel	0%
Unknown	43%117

Building Type	Gallons HW per unit per day ¹¹⁸ (A)	Unit	Estimated % HW from Faucets ¹¹⁹ (B)	Multiplier 120 (C)	Unit	Days per year (D)	Annual gallons mixed water per faucet (A*B*C*D)
Small Office	1	person	100%	10	employees per faucet	250	2,500
Large Office	1	person	100%	45	employees per faucet	250	11,250
Fast Food Restaurant	0.7	meal/day	50%	75	meals per faucet	365	9,581
Sit-Down Restaurant	2.4	meal/day	50%	36	meals per faucet	365	15,768
Retail	2	employee	100%	5	employees per faucet	365	3,650

¹¹⁴ Temperature cited from SBW Consulting, Evaluation for the Bonneville Power Authority, 1994, http://www.bpa.gov/energy/n/reports/evaluation/residential/faucet_aerator.cfm. This is a variable that would benefit from further conduction.

¹¹⁵ Using 40" deep soil temp as a proxy at Powell Gardens SCAN site. Average by month of available data from 3/28/02–

^{10/11/14: 12} month average is 57.898. http://www.wcc.nrcs.usda.gov/nwcc/site?sitenum=2061

¹¹⁶ Electric water heater have recovery efficiency of 98%: http://www.ahrinet.org/ARI/util/showdoc.aspx?doc=576

¹¹⁷ Default assumption for unknown fuel is based on EIA Commercial Building Energy Consumption Survey (CBECS) 2012 for Midwest North Central Region (see 'HC8.9 Water Heating in Midwest Region.xls'). If utilities have specific evaluation results providing a more appropriate assumption for buildings in a particular market or geographical area, then they should be used. ¹⁰⁴ Representative baseline flow rate for kitchen and bathroom faucet aerators from sources 1, 2, 3, and 4. This accounts for all throttling and differences from rated flow rates. The most comprehensive available studies did not disaggregate kitchen use from bathroom use, but instead looked at total flow and length of use for all faucets. This makes it difficult to reliably separate kitchen water use from bathroom water use.

Table 2-45 Chapter 49, Service Water Heating, 2007 ASHRAE Handbook, HVAC Applications.

¹¹⁹ Estimated based on data provided in Appendix E, "Waste Not, Want Not: The Potential for Urban Water Conservation in California," http://www.pacinst.org/reports/urban_usage/appendix_e.pdf.

 $^{^{120}}$ Based on review of the Illinois plumbing code (Employees and students per faucet). Retail, grocery, warehouse and health are estimates. Meals per faucet estimated as 4 bathroom and 3 kitchen faucets and average meals per day of 250 (based on California study above) -250/7 = 36. Fast food assumption estimated.

Grocery	2	employee	100%	5	employees per faucet	365	3,650
Warehouse	2	employee	100%	5	employees per faucet	250	2,500
Elementary School	0.6	person	50%	50	students per faucet	200	3,000
Jr High/High School	1.8	person	50%	50	students per faucet	200	9,000
Health	90	patient	25%	2	Patients per faucet	365	16,425
Motel	20	room	25%	1	faucet per room	365	1,825
Hotel	14	room	25%	1	faucet per room	365	1,278
Other	1	employee	100%	20	employees per faucet	250	5,000

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = calculated value above on a per faucet basis

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

=0.0001811545

FOSSIL FUEL IMPACT DESCRIPTIONS AND CALCULATION

 $\Delta Therms = \%FossilDHW*((GPM_{base} - GPM_{low}) / GPM_{base})*Usage*EPG_{gas}*ISR$

Where:

%FossilDHW = proportion of water heating supplied by fossil fuel heating (see

table below)

EPG_gas = Energy per gallon of mixed water used by faucet (gas water

heater)

= (8.33 * 1.0 * (WaterTemp - SupplyTemp)) / (RE_gas * 100,000)

= 0.00772 Therm/gal

RE_gas = Recovery efficiency of gas water heater

 $=67\%^{115}$

100,000 = Converts Btus to Therms (Btu/Therm)

Other variables as defined above.

DHW fuel	%Fossil_DHW	
Electric	0%	
Fossil Fuel	100%	

Unknown	57%121

WATER IMPACT DESCRIPTIONS AND CALCULATION

 Δ gallons = $((GPM_{base} - GPM_{low}) / GPM_{base}) * Usage * ISR$

Variables as defined above

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

SOURCES USED FOR GPM ASSUMPTIONS

Source ID	Reference
1	2000, Mayer, Peter, William DeOreo, and David Lewis. Seattle Home Water Conservation
	Study. December 2000.
	2003, Mayer, Peter, William DeOreo. Residential Indoor Water Conservation Study.
2	Aquacraft, Inc. Water Engineering and Management. Prepared for East Bay Municipal Utility
	District and the US EPA. July 2003.
3	2011, DeOreo, William. Analysis of Water Use in New Single Family Homes. By Aquacraft.
3	For Salt Lake City Corporation and US EPA. July 20, 2011.
	2008, Schultdt, Marc, and Debra Tachibana. Energy related Water Fixture Measurements:
4	Securing the Baseline for Northwest Single Family Homes. 2008 ACEEE Summer Study on
	Energy Efficiency in Buildings.

MEASURE CODE:

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¹²¹ Default assumption for unknown fuel is based on EIA Commercial Building Energy Consumption Survey (CBECS) 2012 for Midwest North Central Region (see 'HC8.9 Water Heating in Midwest Region.xls'). If utilities have specific evaluation results providing a more appropriate assumption for buildings in a particular market or geographical area, then they should be used. ¹¹⁵ Review of AHRI Directory suggests range of recovery efficiency ratings for new Gas DHW units of 70-87%. Average of existing units is estimated at 75%. Commercial properties are more similar to MF homes than SF homes. MF hot water is often provided by a larger commercial boiler. This suggests that the average recovery efficiency is somewhere between a typical central boiler efficiency of .59 and the .75 for single family home. An average is used for this analysis by default.

2.4.2 Circulator Pump

DESCRIPTION

Demand control recirculation pumps seek to reduce inefficiency by combining control via temperature and demand inputs, whereby the controller will not activate the recirculation pump unless both (a) the recirculation loop return water has dropped below a prescribed temperature (e.g. 100°F) and (b) a CDHW demand is sensed as water flow through the CDHW system.

This measure was developed to be applicable to the following program types: TOS, RF, and NC.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

Re-circulating pump shall cycle on based on (a) the recirculation loop return water dropping below a prescribed temperature (e.g. 100°F) and (b) a CDHW demand is sensed as water flow through the CDHW system.

DEFINITION OF BASELINE EQUIPMENT

The base case for this measure category is an existing, un-controlled recirculation pump on a gasfired Central Domestic Hot Water System.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The effective useful life is 15 years. 122

DEEMED MEASURE COST

The assumed measure cost is \$1,200 per pump. 123

LOADSHAPE

Miscellaneous BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

Savings shown are per pump.

ELECTRIC ENERGY SAVINGS

Deemed at 651 kWh.124

SUMMER COINCIDENT PEAK DEMAND SAVINGS

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¹²² Benningfield Group. (2009). PY 2009 Monitoring Report: Demand Control for Multifamily Central Domestic Hot Water. Folsom, CA: Prepared for Southern California Gas Company, October 30, 2009.

¹²³ Gas Technology Institute. (2014). 1003: Demand-based domestic hot water recirculation Public project report. Des Plaines, IL: Prepared for Nicor Gas, January 7, 2014.

¹²⁴ Based on results from the Nicor Gas Emerging Technology Program study, this value is the average kWh saved per pump. Note this value does not reflect savings from electric units but electrical savings from gas-fired units.

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = calculated value above on a per faucet basis

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor =0.0001379439

NATURAL GAS SAVINGS

 Δ Therms = 55.9 * number of dwelling units¹²⁵

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

¹²⁵ Based on results from the Nicor Gas Emerging Technology Program study, this value is the average therms saved per dwelling unit.

2.4.3 Heat Pump Water Heater

DESCRIPTION

This measure applies to the installation of a heat pump water heater (HPWH) in place of a standard electric water heater in a commercial building. Savings are presented dependent on the heating system installed in the building due to the impact of the heat pump water heater on the heating and cooling loads.

This measure was developed to be applicable to the following program types: TOSNC.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a heat pump water heater meeting program efficiency requirements.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is assumed to be a new, electric storage water heater meeting federal minimum efficiency standards. 126

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 13 years. 127

DEEMED MEASURE COST

Actual costs should be used where available. Incremental capital costs are presented in the table below for heat pump water heaters with energy factors (EF) of 2.0 and 2.4 and rated volumes of 40 gallons and 50 gallons, respectively.¹²⁸

EF	Rated Volume (gal)	Incremental Cost
2.0	40	\$1,340.30
2.4	50	\$1,187.58

For larger HPWHs, incremental capital costs are presented below based on heating capacity. 129

Heating Capacity (MBtu/hr)	Incremental Cost
10-50	\$4,000.00
>50-100	\$7,000.00
>100-300	\$10,000.00
>300-500	\$14,000.00

 $^{^{126}}$ Federal standards for ≤55 gallon and ≤12 kW storage water heaters are from 10 CFR §430.32(d). Federal standards for >120 gallon and>12 kW storage water heaters are from 10 CFR §431.110. Since the federal standard effectively requires a heat pump water heater for residential electric storage water heaters >55 gallons and ≤120 gallons, this measure excludes those units.

127 2010 Residential Heating Products Final Rule Technical Support Document, U.S. DOE, Table 8.7.2.

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¹²⁸ Cost information is based upon data from "2010-2012 WA017 Ex Ante Measure Cost Study Draft Report," Itron, February

 $^{28, 2014. \} See \ ``NR \ HW \ Heater_WA017_MCS \ Results \ Matrix - Volume \ I_August 2016.xls" \ for \ more \ information.$

 $^{^{129}}$ Costs for larger heat pump water heaters are from 2017 Michigan Energy Measures Database.xlsx and are based on heat pump water heaters with a COP \geq 3.0.

>500	\$18,000.00
	4-0,0000

LOADSHAPE

Water Heating BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = ((1/EF_{BASE} - 1/EF_{EE})*HWU_{GAL}*\gamma Water*(T_{out} - T_{in})*1.0*3,412) + kWh_{COOL} - kWh_{HEAT}$

 $kWh_{COOL} = ((1-1/EF_{EE})*HWU_{GAL}*\gamma Water*(T_{out} - T_{in})*1.0*LF*53\%*LM) / (COP_{COOL}*3,412)*\%Cool$

kWh $_{\rm HEAT}$ = ((1-1/EF $_{\rm EE}$) * HWU $_{\rm GAL}$ * γ Water * (T $_{\rm out}$ - T $_{\rm in}$) * 1.0) * LF * 43%) / (COP $_{\rm HEAT}$ * 3,412) * %ElectricHeat

Where:

kWh_cool = Cooling savings from conversion of heat in building to water heat | kWh heat = Heating cost from conversion of heat in building to water heat

(dependent on heating fuel)

EF_{BASE} = Efficiency of baseline water heater according to federal standards,

expressed as Energy Factor (EF) or Thermal Efficiency (Et)

= See table below

 EF_{EE} = EF of heat pump water heater

= Actual

HWU_{GAL} = Estimated annual hot water consumption (gallons)

= Actual if possible to provide reasonable custom estimate. If not, two

methodologies are provided below to develop an estimate.

γWater = Specific weight of water

= 8.33 pounds per gallon

 T_{OUT} = Tank temperature

= Actual, if unknown assume 125 °F 131

T_{IN} = Incoming water temperature from well or municipal system

¹³⁰ This algorithm calculates the heat removed from the air by subtracting the heat pump water heater electric consumption from the total water heating energy delivered. This is then adjusted to account for location of the heat pump unit and the coincidence of the waste heat with cooling requirements, the efficiency of the central cooling, and latent cooling demands.

¹³¹ Ideally, the actual set point of the water heater should be used. If not available, 125 degrees is provided as an estimate of unmixed output temperature. While plumbing code generally limits temperatures at the end use, it typically does not limit the water heater system, which can be anywhere in the range 120-201 degrees. For applications such as laundry and dishwashing, health and safety regulations may require water to be initially heated to higher temperatures. Since temperature set points can vary widely, market, program, or site-specific data should be used whenever possible.

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Appendix H - TRM - Vol. 2: C&I Measures

= 57.898 °F ¹³²
= Heat capacity of water (1 Btu/lb*°F)
= Conversion factor from Btu to kWh
= Location Factor
= 1.0 for HPWH installation in a conditioned space
= 0.5 for HPWH installation in an unknown location ¹³³
= 0.0 for installation in an unconditioned space
= Portion of reduced waste heat that results in cooling savings ¹³⁴
= Portion of reduced waste heat that results in increased heating load ¹³⁵
= Latent multiplier to account for latent cooling demand ¹³⁶
= 3.0 for St. Louis, MO
= COP of central air conditioner
= Actual
= Actual. Note: electric resistance heating and heat pumps will have an
efficiency greater than or equal to 100%
= Percentage of buildings with central cooling
= 100% for cooling in the home and 0% for no cooling in the home
= Percentage of buildings with electric heat
= 100% for electric heating fuel and 0% for gas heating fuel

Equipment Type	Size Category	Federal Standard Minimum Efficiency
HPWH ≤12 kW	≤55 gallon	EF: 0.96 – (0.0003 * rated volume in gallons)
HPWH >12 kW	>120 gallon	Et: 98% ¹³⁷

Method 1 to estimate HWU_{GAL} – Consumption per water heater capacity

HWU_{GAL} = Consumption/cap * Capacity

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¹³² Using 40" deep soil temp as a proxy at Powell Gardens SCAN site. Average by month of available data from 3/28/02–10/11/14:

¹² month average is 57.898. http://www.wcc.nrcs.usda.gov/nwcc/site?sitenum=2061.

¹³³ Professional judgment.

¹³⁴ Based on 193 days where CDD 65>0, divided by 365.25. CDD days determined from TMY data with a base temp of 65°F.
135 Based on 157 days where HDD 60>0, divided by 365.25. HDD days determined from TMY data with a base temp of 60°F.

¹³⁶ The Latent Multiplier is used to convert the sensible cooling savings calculated to a value representing sensible and latent cooling loads. The values are derived from the methodology outlined in Infiltration Factor Calculation Methodology by Bruce Harley, Senior Manager, Applied Building Science, CLEAResult 11/18/2015 and is based upon an 8760 analysis of sensible and total heat loads using hourly climate data.

137 Efficiency of baseline water heaters >120 gallons based on search of electric storage water heaters >120 gallons available on

AHRI directory.

Where:

Consumption/cap = Estimate of consumption per gallon of tank capacity, dependent

on Building Type (see table below)¹³⁸

= Capacity of hot water heater in gallons Capacity

= Actual

Building Type	Consumption/cap				
Grocery, Convenience Store, and Restaurant	803				
Lodging, Hospital, and Multifamily	630				
Health Clinic, Church, Warehouse	433				
Education, Office, and Retail	594				
Industrial	558				
Agriculture	558				
Average Non Residential	558				

Method 2 to estimate HWUGAL – Consumption by facility size¹³⁹

Building Type	Gallons HW per unit per day	Unit	Units/1000 ft ²	Days per year	Gallons / 1000 ft² floor area
Small Office	1	person	2.3	250	575
Large Office	1	person	2.3	250	575
Fast Food Restaurant	0.7	meal/day	784.6	365	200,458
Sit-Down Restaurant	2.4	meal/day	340	365	297,840
Retail	2	employee	1	365	730
Grocery	2	employee	1.1	365	803
Warehouse	2	employee	0.5	250	250
Elementary School	0.6	person	9.5	200	1,140
Jr High/High School	1.8	person	9.5	200	3,420
Health	90	patient	3.8	365	124,830
Motel	20	room	5	365	36,500
Hotel	14	room	2.2	365	11,242
Other	1	employee	0.7	250	175

SUMMER COINCIDENT PEAK DEMAND SAVINGS

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 $^{^{138} \} Based \ on \ Cadmus \ analysis. \ Annual \ hot \ water \ usage \ in \ gallons \ based \ on \ CBECS \ (2003) \ consumption \ data \ for \ West \ North \ Central$ $(removed\ outliers\ of\ 1,000\ kBtu/hr\ or\ less)\ to\ calculate\ hot\ water\ usage.\ Annual\ hot\ water\ gallons\ per\ tank\ size\ gallons\ based\ on$ the tank sizing methodology found in ASHRAE 2011 HVAC Applications. Chapter 50 Service Water Heating. Demand assumptions (gallons per day) for each Building Type based on ASHRAE Chapter 50 and "Technology Data Characterizing Water Heating in Commercial Buildings: Application to End Use Forecasting," Lawrence Berkeley National Library, December 1995. VEIC considers these values to be relatively conservative estimates that may benefit from future evaluation.

139 Technology Data Characterizing Water Heating in Commercial Buildings: Application to End Use Forecasting,"

Berkeley National Library, December 1995.

 $\Delta kW = \Delta kWh * CF$

Where:

ΔkWh = Electric energy savings, as calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001811545^{140}$

NATURAL GAS SAVINGS

$$\Delta therms = \left[\;\left((1\text{-}1/EF_{EE}) * HWU_{GAL} * \gamma Water * T_{out} - T_{in}\right) * 1.0\right) * LF * 53\% \right] / \left(\eta Heat * 100,000\right) * \% GasHeat$$

Where:

 Δ Therms = Heating cost from conversion of heat in building to water heat

for buildings with natural gas heat141

100,000 = Conversion factor from Btu to therms

ηHeat = Efficiency of heating system

= Actual

%GasHeat = Percentage of buildings with gas heat

= 0% for Electric Heating Fuel =100% for Gas Heating Fuel

Other variables as defined above.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

140 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Water Heating. See reference "Ameren Missouri 2016

Appendix E - End Use Shapes and Coincident Factors.pdf."

141 This is the additional energy consumption required to replace the heat removed from the building during the heating season by the heat pump water heater. The variable kWh_heating (electric resistance) is that additional heating energy for a building with electric resistance heat (COP 1.0). This formula converts the additional heating kWh for an electric resistance building to the MMBtu required in a natural gas heated building, applying the relative efficiencies.

2.5 HVAC

Table: Effective Full Load Heating and Cooling Hours, by Building Type

		ıan AFB vg)		ln, NE W)		dison, IA (E)		iser W)		irardeau E)	St Louis	s Metro	Kansa	s City
Building Type	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH	Heating EFLH	Cooling EFLH
Large Office	1039	1846	1141	1756	1088	1539	997	1918	861	1784	988	1869	1056	1792
Medium Office	649	1350	740	1245	728	1146	567	1412	528	1323	645	1386	708	1325
Small Office	946	1114	1030	1041	1029	975	926	1165	769	1082	893	1159	989	1097
Warehouse	991	415	1201	380	1227	357	1189	457	851	391	1059	433	1207	400
Stand-alone Retail	1012	1000	1125	903	1139	808	968	1076	891	965	994	986	1036	946
Strip Mall	1030	970	1124	884	1148	794	984	1044	905	944	1001	956	1039	916
Primary School	806	1019	892	958	898	852	798	1155	666	1016	785	1195	840	971
Secondary School	719	812	803	724	867	677	754	911	603	800	712	873	779	779
Supermarket	1279	875	1367	800	1405	672	1330	902	1120	837	1248	846	1344	820
Quick Service Restaurant	1233	1013	1414	916	1513	819	1316	1127	1025	973	1262	1035	1387	970
Full Service Restaurant	1367	1119	1499	1014	1655	952	1442	1234	1156	1114	1380	1124	1473	1059
Hospital	3388	3318	3205	3055	3467	2733	3891	3448	2913	3312	3170	3413	3372	3215
Outpatient Health Care	3203	3113	3261	2834	3150	2627	3128	3217	3001	3109	3013	3265	3164	2994
Small Hotel - Building	602	2247	697	2097	760	1914	620	2386	436	2304	575	2277	669	2207
Large Hotel - Building	1656	2148	1472	2016	1980	1916	1943	2369	1202	2186	1551	2363	1692	2155
Midrise Apartment - Building	1462	1132	1599	1028	1710	901	1590	1214	1208	1085	1433	1171	1580	1090
C&I Average ¹⁴²	1067	1018	1196	937	1217	865	1118	1085	910	996	1060	1053	1164	986

¹⁴² See Volume 1 for details on modeling calculations and assumptions.

2.5.1 Small Commercial Learning Thermostats

DESCRIPTION

This measure characterizes the energy savings from the installation of a new programmable thermostat for reduced cooling and heating energy consumption through temperature set-back during unoccupied or reduced demand times as well as automatic adjustments based on occupancy patterns and various independent variables such as weather. This measure is limited to small businesses as defined by programs, ¹⁴³ as they have smaller HVAC systems that are similar to residential HVAC systems and may be controlled by a simple manual adjustment thermostat. Midto large-sized businesses will typically have a building automation system or some other form of automated HVAC controls. This measure is only appropriate for single zone heating systems. Custom calculations are required for savings for learning thermostats installed in multi-zone systems.

This measure was developed to be applicable to the following program types: RF, DI, and TOS.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The criteria for this measure are established by replacement of a manual-only temperature control with one that has the capability to adjust temperature set-points according to various independent variables without manual intervention.

DEFINITION OF BASELINE EQUIPMENT

For new thermostats the baseline is a non-programmable thermostat requiring manual intervention to change the temperature set-point.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life of a learning thermostat is assumed to be 10 years 144 based upon equipment life only. 145

DEEMED MEASURE COST

Actual material and labor costs should be used if the implementation method allows. If unknown, the capital cost for this measure is assumed to be \$224. 146

LOADSHAPE

Cooling BUS Heating BUS

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 $^{^{143}}$ The square footage of the small office prototype building modeled in is 7,500 sf.

¹⁴⁴ Table 1, HVAC Controls, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007.

¹⁴⁵ Future evaluation is strongly encouraged to inform the persistence of savings to further refine measure life assumption. As this characterization depends heavily upon a large scale but only 2-year study of the energy impacts of programmable thermostats, the longer-term impacts should be assessed.

¹⁴⁶ Ameren Missouri Technical Resource Manual – Effective January 1, 2018. This current value was reviewed and confirmed using PY20 program data.

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

△kWh = 1/eff * EFLHCOOL * BtuhCOOL / 1000 * ESFCOOL

Where:

eff = Efficiency of HVAC unit

= Actual; If not available, assume 10 SEER

EFLH_{COOL} = Effective Full Load Cooling Hours

= Actual; If not available, refer to section 2.7 HVAC

Btuhcool = Cooling System Capacity

= Actual

ESFCOOL = Cooling energy savings factor

= Assume 0.139^{147}

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kW * CF$

Where:

 ΔkWh = Electric energy savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0009106840

NATURAL GAS ENERGY SAVINGS

△Therms = SQFT * SavingsFactor * PF / (100 * AFUE_{EXIST})

Where:

SOFT = Square footage of building controlled by thermostat

SavingsFactor = $9.940 \text{ kBtu/sf-yr}^{148}$

= Efficiency rating of existing heating equipment (AFUE), in decimal form. **AFUE**_{EXIST}

100 = Converts kBtu to therms, 1 therm = 100 kBtu

¹⁴⁷ Cadmus (Aarish, C., M. Perussi, A. Rietz, and D. Korn). Evaluation of the 2013-2014 Programmable and Smart Thermostat

Program. Prepared for Northern Indiana Public Service Company and Vectren Corporation. 2015.
 Heating Savings Factors for the programmable thermostat are calculated as the savings in annual building load divided by the square footage of the prototype building (5,500 sf) and converted to kBtu.

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Appendix H - TRM - Vol. 2: C&I Measures

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.5.2 Small Commercial Programmable Thermostats

DESCRIPTION

This measure characterizes the energy savings from the installation of a new programmable thermostat for reduced heating and cooling energy consumption through temperature set-back during unoccupied or reduced demand times. This measure is limited to small businesses as defined by programs, ¹⁴⁹ as they have smaller HVAC systems that are similar to residential HVAC systems and may be controlled by a simple manual adjustment thermostat. Mid- to large-sized businesses will typically have a building automation system or some other form of automated HVAC controls. This measure is only appropriate for single zone heating systems. Custom calculations are required for savings for programmable thermostats installed in multi-zone systems.

This measure was developed to be applicable to the following program types: RF and DI.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The criteria for this measure are established by replacement of a manual-only temperature control with one that has the capability to adjust temperature set-points according to a schedule without manual intervention.

DEFINITION OF BASELINE EQUIPMENT

For new thermostats the baseline is a non-programmable thermostat requiring manual intervention to change the temperature set-point.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life of a programmable thermostat is assumed to be 8 years¹⁵⁰ based upon equipment life only.¹⁵¹

DEEMED MEASURE COST

Actual material and labor costs should be used if the implementation method allows. If unknown, the capital cost for this measure is assumed to be \$181.152

LOADSHAPE

Cooling BUS

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 $^{^{\}rm 149}$ The square footage of the small office prototype building modeled in is 7,500 sf.

¹⁵⁰ Table 1, HVAC Controls, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007.

¹⁵¹ Future evaluation is strongly encouraged to inform the persistence of savings to further refine measure life assumption. As this characterization depends heavily upon a large scale but only 2-year study of the energy impacts of programmable thermostats, the longer-term impacts should be assessed.

¹⁵² Based upon Nicor, Illinois Rider 30 Business EER Program Database, Paid Rebates with Programmable Thermostat Installation Costs, Program to Date as of January 11, 2013. If Missouri average costs are available, they should be used.

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 Δ kWh = SQFT * SavingsFactor * PF / EER_{EXIST}

Where:

Sqft = Square footage of building controlled by thermostat

SavingsFactor = $0.578 \text{ kWh/sf-yr}^{153}$

PF = Persistence Factor to account for thermostat being placed on hold,

reset or bypassed.

= Actual if provided in program evaluation, else assume 50%154

EER_{EXIST} = Efficiency rating of existing cooling equipment EER (btu hr/W)

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kW * CF$

Where:

ΔkWh = Electric energy savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0009106840

NATURAL GAS ENERGY SAVINGS

 Δ Therms = SQFT * SavingsFactor * PF / (100 * AFUE_{EXIST})

Where:

SQFT = Square footage of building controlled by thermostat

Savings Factor = $9.940 \text{ kBtu/sf-yr}^{155}$

 ¹⁵³ Cooling savings factors for the programmable thermostat are calculated as the savings in annual building load divided by the square footage of the small office prototype building (5,500 sf).
 154 This factor is based on consideration of the findings from a number of evaluations, including Sachs et al, "Field Evaluation of

Programmable Thermostats," US DOE Building Technologies Program, December 2012, p35; "low proportion of households that ended up using thermostat-enabled energy saving settings"

http://apps1.eere.energy.gov/buildings/publications/pdfs/building_america/field_eval_thermostats.pdf%20, and Meier et al., "Usability of residential thermostats: Preliminary investigations," Lawrence Berkeley National Laboratory, March 2011, p1;

[&]quot;The majority of occupants operated thermostats manually, rather than relying on their programmable features and almost 90% of respondents reported that they rarely or never adjusted the thermostat to set a weekend or weekday program. Photographs of thermostats were collected in one on-line survey, which revealed that about 20% of the thermostats displayed the wrong time and that about 50% of the respondents set their programmable thermostats on "long term hold" (or its equivalent)." http://eec.ucdavis.edu/files/Usability of residential thermostats.pdf.

¹⁵⁵ Heating Savings Factors for the programmable thermostat are calculated as the savings in annual building load divided by the square footage of the prototype building (5,500 sf) and converted to kBtu.

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100 = Converts kBtu to therms, 1 therm = 100 kBtu

AFUE_{EXIST} = Efficiency rating of existing heating equipment (AFUE), in decimal form.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.5.3 Demand Controlled Ventilation

DESCRIPTION

Demand control ventilation (DCV) automatically adjusts building ventilation rates based on occupancy. DCV is part of a building's ventilation system control strategy. It may include hardware, software, and controls as an integral part of a building's ventilation design. Active control of the ventilation system provides the opportunity to reduce heating and cooling energy use.

The primary component is a control sensor to communicate either directly with the economizer or with a central computer. The component is most typically a carbon dioxide (CO₂) sensor, occupancy sensor, or turnstile counter. This measure is modeled to assume night time set backs are in operation and minimum outside air is being used when the building is unoccupied.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment condition is defined by new CO₂ sensors installed on return air systems where no other sensors were previously installed. Additionally, commissioned control logic and installed hardware must be capable of reducing ventilation rates based on sensor input. For heating savings, this measure does not apply to any system with terminal reheat (constant volume or variable air volume). For terminal reheat system a custom savings calculation should be used.

DEFINITION OF BASELINE EQUIPMENT

The base case for this measure is a space with no demand control capability. The current code minimum for outside air (OA) is 17 CFM per occupant (ASHRAE 62.1) which is the value assumed in this measure.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The deemed measure life is 10 years. 156

DEEMED MEASURE COST

As a retrofit measure, the actual cost of installation should be used for screening. Costs should include the hardware and labor costs to install the sensors. Additional purchase and installation costs for any other component of the DCV system that was not previously existing should also be included.

LOADSHAPE

Cooling BUS

Algorithm

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¹⁵⁶ Based on CO₂ sensor estimated life, determined through conversations with contractors to have a minimum lifetime of 10 years. It is recommended that they are part of a normal preventive maintenance program, as calibration is an important part of extending useful life. Although they are not subject to mechanical failure, they can fall out of tolerance over time.

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS

For facilities heated by natural gas, cooling savings are:

$$\Delta kWh = SQFT_{cond} / 1000 * SF_{cooling}$$

For facilities heated by heat pumps, heating and cooling savings are:

$$\Delta kWh = SQFT_{cond} / 1000 * SF_{cooling} + SQFT_{cond} / 1000 * SF_{Heat HP}$$

For facilities heated by electric resistance heating and cooling savings are:

$$\Delta kWh = SQFT_{cond} \: / \: 1000 \: * \: SF_{cooling} + SQFT_{cond} \: / 1000 \: * \: SF_{Heat \: ER}$$

Where:

 $\begin{array}{ll} SQFT_{cond} & = Square \ footage \ of \ conditioned \ space \ commissioned \ with \ DCV \\ SF_{cooling} & = Cooling \ Savings \ Factor, \ including \ cooling \ and \ fan \ energy \ savings \\ SF_{Heat \ HP} & = Heating \ Savings \ factor \ for \ facilities \ heated \ by \ Electric \ Resistance \ (ER) \\ \end{array}$

Savings factors are based on Building Type and weather zone – see tables below. 157

	SFcooling (kWh/1000 SqFt)						
	North East	North	South East	South	St	Kansa	Average/
Building Type	(Fort	West	(Cape	West	Louis		Unknown
	Madison,	(Lincol	Girardeau,	(Kaiser,	Metro,	City,	(Knob
	IA)	n, NE)	MO)	MO)	MO	MO	Noster, MO)
Office - Low-rise	475	533	535	634	649	555	579
Office - Mid-rise	448	502	504	597	611	523	545
Office - High-rise	468	525	527	624	639	547	570
Religious Building	567	635	639	756	774	662	690
Restaurant	561	629	632	748	765	655	683
Retail - Department Store	654	734	737	873	893	764	797
Retail - Strip Mall	399	447	449	532	544	466	486
Convenience Store	631	708	711	842	862	737	769
Elementary School	353	395	397	470	481	412	430
High School	340	382	384	454	465	398	415
College/University	442	495	498	589	603	516	538
Healthcare Clinic	384	431	433	513	525	449	468
Lodging	605	679	682	808	827	707	738
Manufacturing	500	560	563	666	682	584	609

¹⁵⁷ Energy savings factors were calculated using weather data and methodology consistent with ASHRAE standards. Savings are calculated on an annual basis for each given weather zone in Missouri. Original energy savings for DCV were developed for Illinois utilizing standards, inputs and approaches as set forth by ASHRAE 62.1and 90.1. These savings factors were then translated into Missouri-specific values using adjustment factors based on differences in heating and cooling degree hours. See DCV savings factors v1.xlsx for derivation.

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Appendix H - TRM - Vol. 2: C&I Measures

Special Assembly Auditorium	476	534	536	635	650	556	580
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	SF Heat HP (kWh/1000 SqFt)							
Building Type	North East (Fort Madison, IA)	North West (Lincoln, NE)	South East (Cape Girardeau, MO)	South West (Kaiser, MO)	St Louis Metro, MO	Kansas City, MO	Average/ Unknown (Knob Noster, MO)	
Office - Low-rise	171	191	145	151	156	176	159	
Office - Mid-rise	114	128	97	100	104	117	106	
Office - High-rise	154	172	130	135	140	158	143	
Religious Building	1,118	1,248	945	983	1,018	1,149	1,036	
Restaurant	799	892	675	702	727	821	740	
Retail - Department Store	277	310	234	244	252	285	257	
Retail - Strip Mall	184	205	155	161	167	189	170	
Convenience Store	134	150	114	118	122	138	125	
Elementary School	475	531	402	418	433	488	440	
High School	465	519	393	409	423	478	431	
College/University	923	1,031	780	812	840	949	856	
Healthcare Clinic	331	370	280	291	301	340	307	
Lodging	157	175	132	138	143	161	145	
Manufacturing	122	136	103	107	111	125	113	
Special Assembly Auditorium	1,335	1,490	1,128	1,173	1,215	1,371	1,236	

	SF Heat ER (kWh/1000 SqFt)						
Building Type	North East (Fort Madison, IA)	North West (Lincoln, NE)	South East (Cape Girardeau, MO)	South West (Kaiser, MO)	St Louis <u>Metro</u> , MO	Kansas City, MO	Average/ Unknown (Knob Noster, MO)
Office - Low-rise	514	574	434	452	468	528	476
Office - Mid-rise	343	383	290	301	312	352	318
Office - High-rise	461	515	390	406	420	474	428
Religious Building	3,354	3,744	2,835	2,948	3,053	3,446	3,108
Restaurant	2,396	2,675	2,025	2,106	2,181	2,462	2,220
Retail - Department Store	832	929	703	731	757	855	771
Retail - Strip Mall	551	615	465	484	501	566	510
Convenience Store	403	450	341	354	367	414	374
Elementary School	1,426	1,592	1,205	1,253	1,298	1,465	1,321
High School	1,395	1,557	1,179	1,226	1,270	1,433	1,292
College/University	2,770	3,093	2,341	2,435	2,521	2,846	2,567
Healthcare Clinic	993	1,109	839	873	904	1,020	920
lodging	470	525	397	413	428	483	436
Manufacturing	365	408	309	321	332	375	338

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Special Assembly Auditorium	4,004	4,470	3,384	3,519	3,644	4,114	3,709
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SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kW h_{cooling} * CF$

Where:

 Δ kWh_{cooling} = Electric energy savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0009106840

NATURAL GAS SAVINGS

 $\Delta Therms = SQFT_{cond} / 1000 * SF_{Heat Gas}$

Where:

SF Heat Gas Savings factor for facilities heated by natural gas – see table below

	SF _{Heat Gas} (Therm/1000 sq ft)							
Building Type	North East (Fort Madison, IA)	North West (Lincoln, NE)	South East (Cape Girardeau, MO)	South West (Kaiser, MO)	St Louis <u>Metro</u> , MO	Kansas City, MO	Average/ Unknown (Knob Noster, MO)	
Office - Low-rise	22	24	19	19	20	23	20	
Office - Mid-rise	15	16	12	13	13	15	14	
Office - High-rise	20	22	17	17	18	20	18	
Religious Building	143	160	121	126	130	147	133	
Restaurant	102	114	86	90	93	105	95	
Retail - Department Store	35	40	30	31	32	36	33	
Retail - Strip Mall	23	26	20	21	21	24	22	
Convenience Store	17	19	15	15	16	18	16	
Elementary School	61	68	51	53	55	62	56	
High School	60	66	50	52	54	61	55	
College/University	118	132	100	104	108	121	109	
Healthcare Clinic	42	47	36	37	39	44	39	
lodging	20	22	17	18	18	21	19	
Manufacturing	16	17	13	14	14	16	14	
Special Assembly Auditorium	171	191	144	150	155	175	158	

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.5.4 Advanced Roof Top Unit (RTU) Controls

DESCRIPTION

A traditional packaged HVAC rooftop unit uses a zone thermostat to control the operation of the compressor or the gas furnace, depending on whether the zone thermostat is calling for cooling or heating. Under a conventional control scheme, the compressor or furnace is cycled on or off to maintain the zone thermostat set point with the supply fan operating continuously (when the building is occupied) to provide sufficient ventilation air and provide comfort heating and cooling for the space. The supply-fan speed is typically not capable of modulation, so it supplies constant air volume under all modes of operations.

Modulating the supply fan in conjunction with demand-controlled ventilation (DCV) can reduce both heating/cooling energy and fan energy requirements. This measure describes the energy savings realized by retrofitting traditional RTUs with advanced controllers that enable integrated air-side economization, supply-fan speed control (by installing a variable speed drive), and demand-controlled ventilation.

This measure is applicable to the following program type: RF.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

A traditional RTU retrofitted and commissioned with advanced controls that allow for modulation of supply fan speed in conjunction with demand-controlled ventilation (DCV).

DEFINITION OF BASELINE EQUIPMENT

Packaged heating and cooling equipment with constant speed supply fans providing ventilation at the design rate at all times when the fan is operating and when the building is occupied.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life for HVAC application is 15 years.¹⁵⁸

DEEMED MEASURE COST

As a retrofit measure, actual costs should be specified when available. Default measure costs are listed below based on RTU supply fan horsepower rating: 159

Supply Fan Size ¹⁶⁰ (hp)	Controller	Installation Labor	Total Retrofit Cost
1	\$2,200	\$750	\$2,950
2	\$2,600	\$750	\$3,350

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¹⁵⁸ Consistent with other HVAC variable speed drive lifetimes.

¹⁵⁹ Advanced Rooftop Control (ARC) Retrofit: Field-Test Results, PNNL-22656. U.S. Department of Energy, July 2013.

¹⁶⁰ Interpolation may be used to estimate controller cost for motor sizes not listed.

3	\$3,500	\$750	\$4,250
5	\$4,000	\$750	\$4,750
7.5	\$4,142	\$750	\$4,892

LOADSHAPE

HVAC BUS

Algorithm

CALCULATION OF SAVINGS

Although advanced RTUs controls can enable operating strategies that result in heating and cooling savings, field testing has shown variable results (in some instances increased heating/cooling energy consumption has been observed). Field testing has suggested that upwards of 90% of total energy savings can be attributed to reduced fan energy requirements, and therefore the following savings estimates are limited to those relating to fan energy consumption.

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = P_{sf} * SF * Hours_{fan}$

Where:

 P_{sf} = Nominal horsepower of supply fan motor

SF = Fan energy savings factor¹⁶¹ (kWh/hour/horsepower)

= 0.558

Hours_{fan} = Annual operating hours for fan motor based on Building Type. Default hours

are provided for HVAC applications by Building Type. 162 When available, actual hours should be used, especially in instances where RTU operation is seasonal.

Building Type	Total Fan Run Hours
Large Office	6753
Medium Office	6968
Small Office	6626
Warehouse	6263
Stand-alone Retail	6679
Strip Mall	6687
Primary School	5906
Secondary School	6702
Supermarket	6900

¹⁶¹ Based on average field testing results outlined in Advanced Rooftop Control (ARC) Retrofit: Field-Test Results, PNNL-22656. U.S. Department of Energy, July 2013. Savings factors were consistent across the capacity range. See "RTU Control Savings.xlsx" for additional details.

¹⁶² Hours per year are estimated using the modeling results and represent the total number of hours the fans are operating for heating, cooling and ventilation for each Building Type.

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Quick Service Restaurant	7679
Full Service Restaurant	7664
Hospital	8760
Outpatient Health Care	8760
Small Hotel - Building	8760
Large Hotel - Building	8760
Midrise Apartment Building	8728
Nonresidential Average	6773

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = As calculated above.

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0004439830

NATURAL GAS ENERGY SAVINGS

If fossil fuel impacts are expected, a custom analysis should be used to support them.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.5.5 Electric Chiller

DESCRIPTION

This measure involves the installation of a new electric chiller meeting the efficiency standards presented below. This measure could relate to the replacement of an existing unit at the end of its useful life or the installation of a new system in an existing building (i.e., time of sale). Only singlechiller applications should be assessed with this methodology. For multiple chiller projects, a custom analysis should be used to establish savings.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to exceed the efficiency requirements defined by the program.

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline equipment is assumed to meet the 2015 IECC energy efficiency requirements, effective January 1, 2024.

Prior to January 1, 2024, the applicable baseline is assumed to meet the efficiency requirements set forth by local jurisdictions. When local code does not exist, use of IECC 2012 is defined as the building code baseline. In most cases, this will be some version of International Energy Conservation Code (IECC). Depending on the version, this will correspond to the requirements defined within Table 503.2.3(7) in the case of IECC 2009, Table 403.2.3(7) in the case of either IECC 2012 or the IECC 2015, or Table C403.3.2(7) in the case of IECC 2018.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 20 years.¹⁶³

DEEMED MEASURE COST

The incremental capital cost for this measure is \$106.23 per ton. 164

Water cooled, electrically operated, positive displacement (rotary screw and scroll) (\$/ton)							
Capacity (tons)	> 0.72 kW/ton	< 0.72 and	< 0.68 and	0.64 kW/ton and			
		> 0.68 kW/ton	> 0.64 kW/ton	less			
< 50	\$76	\$126	n/a	n/a			
>= 50 and <100	\$38	\$63	n/a	n/a			
>= 100 and <150	\$25	\$42	n/a	n/a			
>= 150 and <200	\$0	\$61	\$122	\$183			
>= 200	\$0	\$31	\$61	\$92			

¹⁶⁴ Ameren Missouri Technical Resource Manual Effective January 1, 2018.

^{163 2008} Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, "Effective/Remaining Useful Life Values," California Public Utilities Commission, December 16, 2008.

Water cooled, electrically operated, positive displacement (reciprocating) (\$/ton)							
Capacity (tons)	> 0.60 kW/ton	< 0.60 and > 0.58 kW/ton	0.58 kw/ton and less				
< 100	\$73	\$110	\$183				
>= 100 and <150	\$49	\$73	\$122				
>= 150 and <200	\$37	\$55	\$92				
>= 200 and <300	\$61	\$91	\$152				
>= 300	\$30	\$46	\$76				

LOADSHAPE

Cooling BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = TONS * (IPLV_{BASE} - IPLV_{EE}) * EFLH$

Where:

TONS = Chiller nominal cooling capacity in tons (note: 1 ton = 12,000 Btu/hr)

= Actual installed

IPLV_{BASE} =Efficiency of baseline equipment expressed as Integrated Part Load Value

(kW/ton). Chiller units are dependent on chiller type. See 'Chiller Units, Conversion Values' and 'Baseline Efficiency Values by Chiller Type' and

Capacity in the Reference Tables section.

IPLV_{EE}¹⁶⁵ = Efficiency of high efficiency equipment expressed as Integrated Part Load

Value (kW/ton)166

= Actual installed

EFLH = Equivalent Full Load Hours for cooling are provided in section 2.7 HVAC

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWH * CF$

Where:

 ΔkWh = Annual electricity savings, as calculated above

¹⁶⁵ Integrated Part Load Value is a seasonal average efficiency rating calculated in accordance with ARI Standard 550/590. It may be calculated using any measure of efficiency (EER, kW/ton, COP), but for consistency, it is expressed in terms of IPLV here.

¹⁶⁶ Can determine IPLV from standard testing or looking at engineering specs for design conditions. Standard data is available from AHRnetLorg. http://www.ahrinet.org/.

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CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor for Cooling = 0.0009106840

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

REFERENCE TABLES

Chillers Ratings - Chillers are rated with different units based on equipment type as shown below

Equipment Type	Unit
Air cooled, electrically operated	EER
Water cooled, electrically operated, positive displacement (reciprocating)	kW/ton
Water cooled, electrically operated, positive displacement (rotary screw and scroll)	kW/ton

In order to convert chiller equipment ratings to IPLV the following relationships are provided

kW/ton = 12 / EER kW/ton = 12 / (COP x 3.412) COP = EER / 3.412 COP = 12 / (kW/ton) / 3.412 EER = 12 / kW/ton EER = COP x 3.412

Baseline Efficiency Values by Chiller Type and Capacity:

Note: Efficiency requirements depend on the path (Path A or Path B) that the building owner has chosen to meet compliance requirements. For air cooled and absorption chillers, Path A should be assumed. For water cooled chillers, the building owner should be consulted and the relevant path used for calculations. When unknown, Path A should be used.

TABLE 503.2.3(7) WATER CHILLING PACKAGES, EFFICIENCY REQUIREMENTS²

			BEFORE	1/1/2010		AS OF 1/1/2	010				
					PAT	на	PAT	нв			
EQUIPMENT TYPE	SIZE CATEGORY		UNITS	FULL LOAD	IPLV	FULL LOAD	IPLV	FULL LOAD	IPLV	TEST PROCEDURE	
	< 150 tons	EER			≥ 9.562	≥ 12.500	NAd	NAd			
Air-cooled chillers	≥ 150 tons	EER	≥ 9.562	≥ 10.416	≥ 9.562	≥ 12.750	NAd	NAd			
Air cooled without condenser, electrical operated	All capacities	EER	≥ 10.586 ≥ 11.782 b		be rated with matching condensers and		comply with the air-cooled chiller efficiency				
Water cooled, electrically operated, reciprocating	All capacities	kW/ton	≤ 0.837	≤ 0.696	Reciprocating cooled positive requirements	ve displaceme					
Water cooled, electrically operated, positive displacement	< 75 tons	kW/ton			≤ 0.780	≤ 0.630	≤0.800	≤ 0.600			
	≥ 75 tons and < 150 tons	kW/ton	≤ 0.790	≤ 0.676	≤ 0.775	≤ 0.615	≤ 0.790	≤ 0.586	AHRI		
	≥ 150 tons and < 300 tons	kW/ton	≤ 0.717	≤ 0.627	≤ 0.680	≤ 0.580	≤0.718	≤ 0.540	550/590		
	≥ 300 tons	kW/ton	≤ 0.639	≤ 0.571	≤ 0.620	≤ 0.540	≤ 0.639	≤ 0.490			
	< 150 tons	kW/ton	≤ 0.703	≤ 0.669							
Water cooled,	≥ 150 tons and < 300 tons	kW/ton	≤ 0.634	≤ 0.596	≤ 0.634	≤ 0.596	≤ 0.639	≤ 0.450			
electrically operated, centrifugal	≥ 300 tons and < 600 tons	kW/ton	≤ 0.576	≤ 0.549	≤ 0.576	≤ 0.549	≤0.600	≤ 0.400			
	≥ 600 tons	kW/ton	≤ 0.576	≤ 0.549	≤ 0.570	≤ 0.539	≤ 0.590	≤ 0.400			
Air cooled, absorption single effect	All capacities	COP	≥ 0.600	NRe	≥ 0.600	NRe	NAd	NAd			
Water-cooled, absorption single effect	All capacities	COP	≥ 0.700	NRe	≥ 0.700	NRe	NAd	NAd	AHRI560		
Absorption double effect, indirect-fired	All capacities	COP	≥ 1.000	≥ 1.050	≥ 1.000	≥ 1.050	NAd	NAd			
Absorption double effect, direct fired	All capacities	COP	≥ 1.000	≥ 1,000	≥ 1.000	≥ 1,000	NAd	NAd			

For SI: 1 ton = 907 kg, 1 British thermal unit per hour = 0.2931 W

a. The chiller equipment requirements do not apply for chillers used in ICMT-temperature applications where the design leaving fluid temperature is < 40°F,
b. Section 12 contains a complete specification of the referenced test procedure, including the referenced year WESiON of the test procedure.
c. Compliance with this standard can be obtained by meeting the minimum requirements of Path A or B. However, both the full load and IPLV must be met to fulfill the requirements of Path A or B.
d. NA means that this requirement is not applicable and cannot be used for compliance.

TABLE C403.2.3(7) MINIMUM EFFICIENCY REQUIREMENTS: WATER CHILLING PACKAGES*

			BEFORE	1/1/2010		AS OF 1	/1/2010 ^b	ences to		
	***		1111111		PAT	TH A	PAT	нв	1	
EQUIPMENT TYPE	SIZE CATEGORY	UNITS	FULL	IPLV	FULL	IPLV	FULL LOAD	IPLV	TEST PROCEDURE ^c	
Air-cooled chillers	< 150 tons	EER	≥ 9.562	≥10.4	≥ 9.562	≥ 12.500	NA	NA		
All-cooled cilliers	≥ 150 tons	EER	2 9.302	16	≥ 9.562	≥ 12.750	NA	NA	1	
Air cooled without condenser, electrical operated	All capacities	EER	≥ 10.586	≥ 11.782	Air-cooled chillers without condens- ers shall be rated with matching con- densers and comply with the air-cooled chiller efficiency requirements		rated with matching co comply with the air-co			
Water cooled, electrically operated, reciprocating	All capacities	kW/ton	≤ 0.837	≤ 0.696	water coo	ating units oled positiv y requirem	ve displac			
	< 75 tons	kW/ton			≤ 0.780	≤ 0.630	≤ 0.800	≤ 0.600		
Water cooled, electrically operated, posi- tive displacement	≥ 75 tons and < 150 tons	kW/ton	≤ 0.790	≤ 0.676	≤ 0.775	≤ 0.615	≤ 0.790	≤ 0.586	AHRI 550/590	
	≥ 150 tons and < 300 tons	kW/ton	≤ 0.717	≤ 0.627	≤ 0.680	≤ 0.580	≤ 0.718	≤ 0.540	33W390	
	≥ 300 tons	kW/ton	≤ 0.639	≤ 0.571	≤ 0.620	≤ 0.540	≤ 0.639	≤ 0.490		
	< 150 tons	kW/ton	≤ 0.703	≤ 0.669						
Water cooled, electrically operated,	≥ 150 tons and < 300 tons	kW/ton	≤ 0.634	≤ 0.596	≤ 0.634	≤ 0.596	≤ 0.639	≤ 0.450		
centrifugal	≥ 300 tons and < 600 tons	kW/ton	≤ 0.576	≤ 0.549	≤ 0.576	≤ 0.549	≤ 0.600	≤ 0.400		
	≥ 600 tans	kW/ton	≤ 0.576	≤ 0.549	≤ 0.570	≤ 0.539	≤ 0.590	≤ 0.400		
Air cooled, absorption single effect	All capacities	COP	≥ 0.600	NR	≥ 0.600	NR	NA	NA		
Water cooled, absorption single effect	All capacities	COP	≥ 0.700	NR	≥ 0.700	NR	NA	NA	AHRI 560	
Absorption double effect, indirect fired	All capacities	COP	≥ 1.000	≥ 1.050	≥ 1.000	≥ 1.050	NA	NA		
Absorption double effect, direct fired	All capacities	COP	≥ 1.000	≥ 1.000	≥ 1.000	≥ 1.000	NA	NA	1	

For SI: 1 ton = 3517 W, 1 British thermal unit per hour = 0.2931 W, "C = {(°F) - 32}/1.8.

NA = Not applicable, not to be used for compliance; NR = No requirement.

a. The centrifugal childre equipment requirements, after adjustment in accordance with Section C403.2.3.1 or Section C403.2.3.2, do not apply to childres used in low-temperature applications where the design leaving fluid temperature is less than 36°F. The requirements do not apply to positive displacement childres with leaving fluid temperatures less than or equal to 32°F. The requirements do not apply to absorption childres with design leaving fluid temperatures less than 40°F.

b. Compliance with this structure can be obtained by consulting the releasing nearly properties of Path A or B. However, both the full look and IPL V shall be used to felfill.

^{6.} Compliance with this standard can be obtained by meeting the minimum requirements of Path A or B. However, both the full load and IPLV shall be met to fulfill the requirements of Path A or B. C. Chapter 6 of the referenced standard contains a complete specification of the referenced test procedure, including the referenced year version of the test procedure.

TABLE C403.2.3(7)
WATER CHILLING PACKAGES – FEFICIENCY REQUIREMENTS^{A, b, d}

EQUIPMENT TO DE	AUTT 0.175000W		BEFORE	1/1/2015	AS OF	1/1/2015	TEST
EQUIPMENT TYPE	SIZE CATEGORY	UNITS	Path A	Path B	Path A	Path B	PROCEDUR
	- 150 T		≥ 9.562 FL	NA°	≥ 10.100 FL	≥ 9.700 FL	
	< 150 Tons	EER	≥ 12.500 IPLV	NA	≥ 13.700 IPLV	≥ 15,800 IPLV	
Air-cooled chillers	≥ 150 Tons	(Btu/W)	≥ 9.562 FL	NA.	≥ 10.100 FL	≥ 9.700 FL	
717.00.101	2 150 1 ons		≥ 12.500 IPLV	NA.	≥ 14.000 IPLV	≥ 16.100 IPLV	İ
Air cooled without condenser, electrically operated	All capacities	EER (Btu/W)	Air-cooled o matching con				
	< 75 Tons		≤ 0.780 FL	≤ 0.800 FL	≤ 0.750 FL	≤ 0.780 FL	Ī
	< /3 Tolls		≤ 0.630 IPLV	≤ 0.600 IPLV	≤ 0.600 IPLV	≤ 0.500 IPLV	İ
	≥ 75 tons and < 150 tons		≤ 0.775 FL	≤ 0.790 FL	≤ 0.720 FL	≤ 0.750 FL	İ
	2 /3 tons and < 150 tons		≤0.615 IPLV	≤ 0.586 IPLV	≤ 0.560 IPLV	≤ 0.490 IPLV	İ
Water cooled, electrically	\$ 150 mm - 2 < 200 mm	1.777	≤ 0.680 FL	≤0.718 FL	≤ 0.660 FL	≤ 0.680 FL	İ
operated positive displacement	≥ 150 tons and < 300 tons	kW/ton	≤ 0.580 IPLV	≤ 0.540 IPLV	≤ 0.540 IPLV	≤ 0.440 IPLV	İ
	≥ 300 tons and < 600 tons		≤ 0.620 FL	≤0.639 FL	≤ 0.610 FL	≤ 0.625 FL	AHRI 550/ 590
	≥ 300 tons and < 000 tons		≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.520 IPLV	≤ 0.410 IPLV	
	> 600 tons		≤ 0.620 FL	≤0.639 FL	≤ 0.560 FL	≤ 0.585 FL	
	≥ 000 tons		≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	
	- 150 T		≤ 0.634 FL	≤0.639 FL	≤ 0.610 FL	≤ 0.695 FL	
	< 150 Tons		≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.440 IPLV	
	5 150 · 1 · 200 ·		≤ 0.634 FL	≤0.639 FL	≤ 0.610 FL	≤ 0.635 FL	
	≥ 150 tons and < 300 tons		≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.400 IPLV	
Water cooled, electrically	≥ 300 tons and < 400 tons		≤ 0.576 FL	≤0.600 FL	≤ 0.560 FL	≤ 0.595 FL	
operated centrifugal	≥ 300 tons and < 400 tons	kW/ton	≤0.549 IPLV	≤ 0.400 IPLV	≤ 0.520 IPLV	≤ 0.390 IPLV	
	≥ 400 tons and < 600 tons		≤ 0.576 FL	≤0.600 FL	≤ 0.560 FL	≤ 0.585 FL	t
	< 400 tons and < 000 tons		≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	t
	m		≤ 0.570 FL	≤0.590 FL	≤ 0.560 FL	≤ 0.585 FL	İ
	≥ 600 Tons		≤ 0.539 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	t
Air cooled, absorption, single effect	All capacities	COP	≥ 0.600 FL	NA°	≥ 0.600 FL	NA°	
Water cooled absorption, single effect	All capacities	COP	≥ 0.700 FL	NA°	≥ 0.700 FL	NA°	
Absorption, double effect, indirect fired	All capacities	cities COP	≥ 1.000 FL ≥ 1.050 IPLV	NA°	≥ 1.000 FL ≥ 1.050 IPLV	NA°	AHRI 560
Absorption double effect direct fired	All capacities	COP	≥ 1.000 FL ≥ 1.000 IPLV	NA ^c	≥ 1.000 FL ≥ 1.050 IPLV	NA°	

a. The requirements for centrifugal chiller shall be adjusted for nonstandard rating conditions in accordance with Section C403 2.3.1 and are only applicable for the range of conditions listed in Section C403 2.3.1. The requirements for air-cooled, water-cooled positive displacement and absorption chillers are at standard rating conditions defined in the reference test procedure.

b. Both the full-load and IPLV requirements shall be met or exceeded to comply with this standard. Where there is a Path B, compliance can be with either Path A or Path B for any application.

c. NA means the requirements are not applicable for Path B and only Path A can be used for compliance.

d. FL represents the full-load performance requirements and IPLV the part-load performance requirements.

TABLE C403.3.2(7)
WATER CHILLING PACKAGES — EFFICIENCY REQUIREMENT St. b. d

EQUIPMENT TYPE	SIZE CATEGORY	UNITS	BEFORE	1/1/2015	AS OF	1/1/2015	TEST
EQUIPMENT TIPE	SIZE CATEGORI	UNITS	Path A	Path B	Path A	Path B	PROCEDURE
	< 150 Tons		≥ 9.562 FL	NAC	≥ 10.100 FL	≥ 9.700 FL	
Air-cooled chillers	< 100 IOHS	EER	≥ 12.500 IPLV	l NA	≥ 13.700 IPLV	≥ 15,800 IPLV	
All-cooled chillers	≥ 150 Tons	(Btu/W)	≥ 9.562 FL	NAG	≥ 10.100 FL	≥ 9.700 FL	
	2 150 10115		≥ 12.500 IPLV	INA.	≥ 14.000 IPLV	≥ 16.100 IPLV	
Air cooled without condenser, electrically operated	All capacities	acities EER (Btu/W)		ndensers and co	condenser shall b omplying with air- equirements.		
	< 75 Tons		≤ 0.780 FL	≤ 0.800 FL	≤ 0.750 FL	≤ 0.780 FL	
			≤ 0.630 IPLV	≤ 0.600 IPLV	≤ 0.600 IPLV	≤ 0.500 IPLV	
	> 75 tons and < 150 tons	1	≤ 0.775 FL	≤ 0.790 FL	≤ 0.720 FL	≤ 0.750 FL	
	2 75 tons and < 150 tons		≤ 0.615 IPLV	≤ 0.586 IPLV	≤ 0.560 IPLV	≤ 0.490 IPLV	
Water cooled, electrically	≥ 150 tons and < 300 tons	kW/ton	≥ 0.680 FL	≥ 0.718 FL	≥ 0.660 FL	≥ 0.680 FL	
operated positive displacement	2 150 tons and < 300 tons	KVV/ton	≥ 0.580 IPLV	≥ 0.540 IPLV	≥ 0.540 IPLV	≥ 0.440 IPLV	AHRI 550/590
	≥ 300 tons and < 600 tons	1	≤ 0.620 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.625 FL	
	2 300 tons and < 000 tons		≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.520 IPLV	≤ 0.410 IPLV	
	≥ 600 tons		≤ 0.620 FL	≤ 0.639 FL	≤ 0.560 FL	≤ 0.585 FL	
			≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	
	< 150 Tons		≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.895 FL	
		-	≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.440 IPLV	
	> 150 tons and < 300 tons		≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.635 FL	
	2 150 tons and < 300 tons		≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.400 IPLV	
Water cooled, electrically	≥ 300 tons and < 400 tons	kW/ton	≤ 0.578 FL	≤ 0.600 FL	≤ 0.560 FL	≤ 0.595 FL	
operated centrifugal	2 300 tons and < 400 tons	KVV/ton	≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.520 IPLV	≤ 0.390 IPLV	
	≥ 400 tons and < 600 tons	1	≤ 0.578 FL	≤ 0.600 FL	≤ 0.560 FL	≤ 0.585 FL	
	2 400 tons and < 000 tons		≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	
	> 600 Tons	1	≤ 0.570 FL	≤ 0.590 FL	≤ 0.580 FL	≤ 0.585 FL	
	2 000 IONS		≤ 0.539 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	
Air cooled, absorption, single effect	All capacities	COP	≥ 0.800 FL	NA°	≥ 0.600 FL	NA°	
Water cooled absorption, single effect	All capacities	COP	≥ 0.700 FL	NA°	≥ 0.700 FL	NA°	
Absorption, double	All capacities	COP	≥ 1.000 FL	NAG	≥ 1.000 FL	NAc	AHRI 560
effect, indirect fired	Air capacities	001	≥ 1.050 IPLV	INA.	≥ 1.050 IPLV	130	
Absorption double effect direct fired	All capacities	COP	≥ 1.000 FL ≥ 1.000 IPLV	NA°	≥ 1.000 FL ≥ 1.050 IPLV	NA°	

a. The requirements for centrifugal civiler shall be adjusted for nonstandard rating conditions in accordance with Section C403.3.2.1 and are only applicable for the range of conditions listed in Section C403.3.2.1. The requirements for air-cooled, water-cooled positive displacement and absorption chillers are at standard rating conditions defined in the reference test procedure.

b. Both the full-load and IPLV requirements shall be made or exceeded to comply with this standard. Where there is a Path B, compliance can be with either Path A or Path B for any application.

c. NA means the requirements are not applicable for Path B and only Path C and be used for compliance.

d. FL represents the full-load performance requirements and IPLV the part-load performance requirements.

MEASURE CODE:

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2.5.6 Heat Pump Systems

DESCRIPTION

This measure applies to the installation of high efficiency air-cooled, water source, ground water source, and ground source heat pump systems. This measure could apply to replacing an existing unit at the end of its useful life, or installation of a new unit in a new or existing building.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

For this characterization to apply, the efficient equipment is assumed to be a high-efficiency aircooled, water source, ground water source, or ground source heat pump system that exceeds both the full load and part load efficiencies associated with the applicable code described in the Definition of Baseline Equipment, energy efficiency requirements specified by the building code applicable to local jurisdiction, prior to January 1, 2024. This may be a version of the 2009, 2012 or 2015 International Energy Conservation Code (IECC) or ASHRAE 90.1 standard, After January 1, 2024, the applicable building code is 2015 IECC.

DEFINITION OF BASELINE EQUIPMENT

For this characterization to apply, the baseline equipment is assumed to be a standard-efficiency air- cooled, water source, ground water source, or ground source heat pump system that meets the 2015 IECC energy efficiency requirements of local building code, effective January 1, 2024.

Prior to January 1, 2024, the applicable baseline is assumed to be similar equipment meeting the energy efficiency requirements of local building code. When local code does not exist, use of IECC 2012 is defined as the building code baseline.

The rating conditions for the baseline and efficient equipment efficiencies must be equivalent.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years.¹⁶⁷

DEEMED MEASURE COST

For analysis purposes, the incremental capital cost for this measure is assumed as \$100 per ton for air-cooled units. ¹⁶⁸ The incremental cost for all other equipment types should be determined on a site-specific basis.

LOADSHAPE

Cooling BUS Heating BUS

Algorithm

¹⁶⁷ Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007.

¹⁶⁸ Based on a review of TRM incremental cost assumptions from Vermont, Wisconsin, and California.

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

For units with cooling capacities less than 65 kBtu/hr:

```
ΔkWh = Annual kWh Savingscool + Annual kWh Savingsheat
```

Annual kWh Savingsheat =
$$(kBtu/hr_{heat}) * [(1/HSPF_{base}) - (1/HSPF_{ee})] * EFLH_{heat}$$

For units with cooling capacities equal to or greater than 65 kBtu/hr:

```
\Delta kWh = Annual \ kWh \ Savings_{cool} + Annual \ kWh \ Savings_{heat}
```

Where:

kBtu/hr_{cool} = Capacity of the cooling equipment in kBtu per hour (1 ton of cooling

capacity equals 12 kBtu/hr).

= Actual installed

 $SEER_{base}$ = Seasonal Energy Efficiency Ratio of the baseline equipment

= SEER from tables below, based on the applicable IECC.

= For units with cooling capacity <65kbtu/hr and efficient unit is measured in terms of SEER2, convert SEERbase to SEER2base, if applicable code is

based on IECC, or custom input as necessary. 169

SEER_{ee} = Seasonal Energy Efficiency Ratio of the energy efficient equipment.

= Actual installed

EFLH_{cool} = Equivalent Full Load Hours for cooling are provided in section 2.7 HVAC

End Use.

HSPF_{base} = Heating Seasonal Performance Factor of the baseline equipment

= HSPF from tables below, based on the applicable IECC. For units with cooling capacity <65kbtu/hr and efficient unit is measured in terms of HSPF2, convert HSPF_{base} to HSPF2_{base}, if applicable code is based on IECC

or custom input as necessary. 170

HSPF_{ee} = Heating Seasonal Performance Factor of the energy efficient equipment.

= Actual installed. If rating is COP, HSPF = COP * 3.413

¹⁶⁹ SEER to SEER2 conversion factor: SEER2 = SEER x 96%. Conversion factor for SEER to SEER2 is used when converting a existing system that is rated in SEER to SEER2. This is to meet the DOE M1 CFR Standard beginning January 1, 2023. The efficiency levels of the existing, baseline, and efficient case must be expressed in the same metrics (e.g., both SEER or SEER2 before applying formulas.

before applying formulas.

170 HSPF to HSPF2 conversion factor: HSPF2 = HSPF x 87%. Conversion factor for HSPF to HSPF2 is used when converting a existing system that is rated in HSPF to HSPF2. This is to meet the DOE MI CFR Standard beginning January 1, 2023. The efficiency levels of the existing, baseline, and efficient case must be expressed in the same metrics (e.g., both HSPF or HSPF2 before applying formulas.

Ameren Missouri

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EFLH_{heat} = Heating mode equivalent full load hours are provided in section 2.7 HVAC

End Use.

IEER_{base} = Integrated Energy Efficiency Ratio of the baseline equipment

= IEER from tables below, based on the applicable IECC.

IEER_{ee} = Integrated Energy Efficiency Ratio of the energy efficient equipment.

= Actual installed

kBtu/hr_{heat} = Capacity of the heating equipment in kBtu per hour.

= Actual installed

3.412 = Btu per Wh.

COP_{base} = Coefficient of performance of the baseline equipment

= COP from tables below, based on the applicable IECC. If rating is HSPF,

COP = HSPF / 3.413. If rating is HSPF2, COP2 = HSPF * 87% / 3.413

COPee = Coefficient of performance of the energy efficient equipment.

= Actual installed

Minimum Efficiency Requirements: 2009 IECC

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TABLE 503.2.3(2)
UNITARY AIR CONDITIONERS AND CONDENSING UNITS, ELECTRICALLY OPERATED, MINIMUM EFFICIENCY REQUIREMENTS

EQUIPMENT TYPE	SIZE CATEGORY	SUBCATEGORY OR RATING CONDITION	MINIMUM EFFICIENCyb	TEST PROCEDURE®	
		Split system	13.0 SEER		
	< 65,000 Btu/h ^a	Single package	13.0 SEER	6 277777	
	≥ 65,000 Btu/h and < 135,000 Btu/h	Split system and single package	10.1 EERc (before Jan 1, 2010) 11.0 EERc (as of Jan 1, 2010)	AHRI210/240	
(Cooling mode) < 2.	≥ 135,000 Btu/h and < 240,000 Btu/h	Split system and single package	9.3 EERc (before Jan 1, 2010) 10.6 EERc (as of Jan 1, 2010)		
	≥ 240,000 Btu/h	Split system and single package	9.0 EERc 9.2 IPLYc (before Jan 1, 2010) 9.5 EERc 9.2 IPLYc (as of Jan 1, 2010)	AHRI 340/360	
Through-the-Wall		Split system	10.9 SEER (before Jan 23, 2010) 12.0 SEER (as of Jan 23,2010)		
(Air cooled, cooling mode)	< 30,000 Btu/h ^d	Single package	10.6 SEER (before Jan 23, 2010) 12.0 SEER (as of Jan 23,2010)	AHRI210/240	
	< 17,000 Btu/h	86°F entering water	11.2 EER	AHRI/ASHRAE 1325	
Water Source (Cooling mode)	≥ 17,000 Btu/h and < 135,000 Btu/h	86°F entering water	12.0 EER	AHRIASHRAE 1325	
Groundwater Source (Cooling mode)	< 135,000 Btu∕h	59°F entering water	16.2 EER	AHRI/ASHRAE 1325	
Ground source (Cooling mode)	< 135,000 Btu/h	77°F entering water	13.4 EER	AHRI/ASHRAE 1325	
	< 65,000 Btu/h ^a	Split system	7.7 HSPF		
Air cooled (Heating mode)	(Cooling capacity)	Single package	7.7 HSPF		
	≥ 65,000 Btu/h and < 135,000 Btu/h (Cooling capacity)	47°F db/43°F wb Outdoor air	3.2 COP (before Jan 1, 2010) 3.3 COP (as of Jan 1, 2010)	AHRI210/240	
	≥ 135,000 Btu/h (Cooling capacity)	47°F db/43°F wb Outdoor air	3.1 COP (before Jan 1, 2010) 3.2 COP (as of Jan 1, 2010)	AHRI 340/360	

TABLE 503.2.3(2)-continued UNITARY AIR CONDITIONERS AND CONDENSING UNITS. ELECTRICALLY OPERATED. MINIMUM EFFICIENCY REQUIREMENTS.

EQUIPMENT TYPE	SIZE CATEGORY	SUBCATEGORY OR RATING CONDITION	MINIMUM EFFICIENCyb	TEST PROCEDURE®	
Through-the-wall		Split System	7.1 HSPE (before Jan 23, 2010) 7.4 HSPF (as of Jan 23,2010)	AVIDIOIO	
(Air cooled, heating mode)	< 30,000 Btu/h Single package		7.0 HSPF (before Jan 23, 2010) 7.4 HSPF (as of Jan 23,2010)	AHRI210/240	
Water source (Heating mode)	< 135,000 Btu/h (Cooling capacity)	68°F entering water	4.2 COP	AHRI/ASHRAE 13256-1	
Groundwater source (Heating mode)	< 135,000 Btu/h (Cooling capacity)	50°F entering water	3.6 COP	AHRI/ASHRAE 13256-1	
Ground source (Heating mode)	< 135,000 Btu/h (Cooling capacity)	32°F entering water	3.1 COP	AHRI/ASHRAE 13256-1	

For SI: °C = [(OF) - 32]/1.8, 1 British thermal unit per hour = 0.2931 W

db = dry-bulb temperature, of; wb = wet-bulb temperature, of.

a. Chapter 6 contains a complete specification of the referenced test procedure, including the referenced year versions of the test procedure.

b. IPLVs and Part load rating conditions are only applicable to equipment with capacity modulation.

c. Deduct 0.2 from the required EERs and IPLVs for units with a heating section other than electric resistance heat.

d. Single-phase air-cooled heat pumps = 65,000 Btu/h are regulated by the National Appliance Energy Conservation Act of 1987 (NAECA), SEER and HSPF values are those set by NAECA.

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Minimum Efficiency Requirements: 2012 IECC

TABLE C403.2.3(2) MINIMUM EFFICIENCY REQUIREMENTS: ELECTRICALLY OPERATED UNITARY AND APPLIED HEAT PUMPS

EQUIPMENT TYPE	SIZE CATEGORY	HEATING SECTION TYPE	SUBCATEGORY OR RATING CONDITION	MINIMUM EFFICIENCY	TEST PROCEDURE	
Air cooled	or one public		Split System	13.0 SEER		
(cooling mode)	< 65,000 Btu/h ^b	All	Single Packaged	13.0 SEER		
Through-the-wall,	≤ 30.000 Btu/h ^b	All	Split System	13.0 SEER	AHRI 210/240	
air cooled	S 30,000 Buvii	All	Single Packaged	13.0 SEER	210/210	
Single-duct high-velocity air cooled	< 65,000 Btu/hb	All	Split System	10.0 SEER	1	
	≥ 65,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER		
Air cooled (cooling mode)	< 135,000 Btu/h	All other	Split System and Single Package	10.8 EER 11.0 IEER	1	
	≥ 135,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	10.6 EER 10.7 IEER	AHRI	
	< 240,000 Btu/h	All other	Split System and Single Package	10.4 EER 10.5 IEER	340/360	
	≥ 240,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	9.5 EER 9.6 IEER	1	
		All other	Split System and Single Package	9.3 EER 9.4 IEER	1	
9	< 17,000 Btu/h	All	86°F entering water	11.2 EER		
Water source (cooling mode)	≥ 17,000 Btu/h and < 65,000 Btu/h	All	86°F entering water	12.0 EER	1	
	≥ 65,000 Btu/h and < 135,000 Btu/h	All	86°F entering water	12.0 EER	ISO 13256-1	
Ground water source	125 000 D. A.	All	59°F entering water	16.2 EER	1	
(cooling mode)	< 135,000 Btu/h	All	77°F entering water	13.4 EER	1	
Water-source water to water	< 135.000 Btu/h	All	86°F entering water	10.6 EER		
(cooling mode)	< 135,000 Billi	All	59°F entering water	16.3 EER	ISO 13256-2	
Ground water source Brine to water (cooling mode)	< 135,000 Btu/h	All	77°F entering fluid	12.1 EER		
Air cooled	es non perhi	-	Split System	7.7 HSPF		
(heating mode)	< 65,000 Btu/h ^b	_	Single Package	7.7 HSPF	1	
Through-the-wall, (air cooled, heating mode)	≤ 30,000 Btu/h ^b	_	Split System	7.4 HSPF	AHRI 210/240	
	(cooling capacity)	-	Single Package	7.4 HSPF		
Small-duct high velocity	< 65.000 Btu/h ^b		Split System	6.8 HSPF	1	

(continued)

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TABLE C403.2.3(2)—continued MINIMUM EFFICIENCY REQUIREMENTS: FLECTRICALLY OPERATED LINITARY AND APPLIED HEAT PLIMPS

EQUIPMENT TYPE	SIZE CATEGORY	HEATING SECTION TYPE	SUB-CATEGORY OR RATING CONDITION	MINIMUM EFFICIENCY	TEST PROCEDURE
Air cooled (heating mode)	≥ 65,000 Btu/h and < 135,000 Btu/h (cooling capacity)		47°F db/43°F wb Outdoor Air	3.3 COP	
			17°F db/15°F wb Outdoor Air	2.25 COP	AHRI
	≥ 135,000 Btu/h		47°F db/43°F wb Outdoor Air	3.2 COP	340/360
	(cooling capacity)		17°F db/15°F wb Outdoor Air	2.05 COP	
Water source (heating mode)	< 135,000 Btu/h (cooling capacity)	-	68°F entering water	4.2 COP	
Ground water source (heating mode)	< 135,000 Btu/h (cooling capacity)	_	50°F entering water	3.6 COP	ISO 13256-1
Ground source (heating mode)	< 135,000 Btu/h (cooling capacity)	_	32°F entering fluid	3.1 COP	1
Water-source water to water	< 135,000 Btu/h	-	68°F entering water	3.7 COP	
(heating mode)	(cooling capacity)	_	50°F entering water	3.1 COP	ISO 13256-2
Ground source brine to water (heating mode)	water (cooling canacity) —		32°F entering fluid	2.5 COP	

For SL 1 British thermal unit per hour = 0.2931 W, "C = [("F) - 32]/1.8.

a. Chapter 6 of the referenced standard contains a complete specification of the referenced test procedure, including the reference year version of the test procedure.

b. Single-phase, air-cooled air conditioners less than 65,000 Btu/h are regulated by NAECA. SEER values are those set by NAECA.

Minimum Efficiency Requirements: 2015 IECC

TABLE C403.2.3(2) MINIMUM EFFICIENCY REQUIREMENTS: ELECTRICALLY OPERATED UNITARY AND APPLIED HEAT PUMPS

EQUIPMENT TYPE	SIZE CATEGORY	HEATING	SUBCATEGORY OR		MUM IENCY	TEST PROCEDURE*	
	5.22 5.11.2 5.11.	SECTION TYPE	RATING CONDITION	Before 1/1/2016	As of 1/1/2016	PROCEDURE*	
Air cooled			Split System	13.0 SEER°	14.0 SEER°		
(cooling mode)	< 65,000 Btu/h ^b	All	Single Package	13.0 SEER°	14.0 SEER°		
Through-the-wall,	≤ 30.000 Btu/h ^b	All	Split System	12.0 SEER	12.0 SEER	AHRI 210/240	
air cooled	2 50,000 Bitth	All	Single Package	12.0 SEER	12.0 SEER		
Single-duct high-velocity air cooled	< 65,000 Btu/hb	All	Split System	11.0 SEER	11.0 SEER		
Air cooled (cooling mode)	≥ 65,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER	11.0 EER 12.0 IEER		
	< 135,000 Btu/h	All other	Split System and Single Package	10.8 EER 11.0 IEER	10.8 EER 11.8 IEER		
	≥ 135,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	10.6 EER 10.7 IEER	10.6 EER 11.6 IEER	AHRI 340/360	
	< 240,000 Btu/h	All other	Split System and Single Package	10.4 EER 10.5 IEER	10.4 EER 11.4 IEER		
	≥ 240,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	9.5 EER 9.6 IEER	9.5 EER 10.6 IEER		
		All other	Split System and Single Package	9.3 EER 9.4 IEER	9.3 EER 9.4 IEER		
	< 17,000 Btu/h	A11	86°F entering water	12.2 EER	12.2 EER		
Water to Air: Water Loop (cooling mode)	≥ 17,000 Btu/h and < 65,000 Btu/h	A11	86°F entering water	13.0 EER	13.0 EER	ISO 13256-1	
	≥ 65,000 Btu/h and < 135,000 Btu/h	All	86°F entering water	13.0 EER	13.0 EER		
Water to Air: Ground Water (cooling mode)	< 135,000 Btu/h	A11	59°F entering water	18.0 EER	18.0 EER	ISO 13256-1	
Brine to Air: Ground Loop (cooling mode)	< 135,000 Btu/h	A11	77°F entering water	14.1 EER	14.1 EER	ISO 13256-1	
Water to Water: WaterLoop (cooling mode)	< 135,000 Btu/h	A11	86°F entering water	10.6 EER	10.6 EER		
Water to Water: Ground Water (cooling mode)	< 135,000 Btu/h	A11	59°F entering water	16.3 EER	16.3 EER	ISO 13256-2	
Brine to Water: Ground Loop (cooling mode)	< 135,000 Btu/h	All	77°F entering fluid	12.1 EER	12.1 EER		

(continued)

TABLE C403.2.3(2)—continued MINIMUM EFFICIENCY REQUIREMENTS: ELECTRICALLY OPERATED UNITARY AND APPLIED HEAT PUMPS

EQUIPMENT TYPE	SIZE CATEGORY	HEATING SECTION TYPE	SUBCATEGORY OR		MUM IENCY	TEST PROCEDURE*	
		SECTION TYPE	RATING CONDITION	Before 1/1/2016	As of 1/1/2016	FROCEDORE	
Air cooled	< 65.000 Btu/h ^b		Split System	7.7 HSPF°	8.2 HSPF°		
(heating mode)	05,000 Blair	1911	Single Package	7.7 HSPF°	8.0 HSPF°		
Through-the-wall,	≤ 30,000 Btu/h ^b	-	Split System	7.4 HSPF	7.4 HSPF	AHRI 210/240	
(air cooled, heating mode)	(cooling capacity)	_	Single Package	7.4 HSPF	7.4 HSPF		
Small-duct high velocity (air cooled, heating mode)	< 65,000 Btu/h ^b	-	Split System	6.8 HSPF	6.8 HSPF		
	≥ 65,000 Btu/h and < 135,000 Btu/h (cooling capacity)		47°F db/43°F wb outdoor air	3.3 COP	3.3 COP	AHRI	
Air cooled			17°F db/15°F wb outdoor air	2.25 COP	2.25 COP		
(heating mode)	≥ 135.000 Btu/h		47°F db/43°F wb outdoor air	3.2 COP	3.2 COP	340/360	
	(cooling capacity)	_	17°F db/15°F wb outdoor air	2.05 COP	2.05 COP	Ī	
Water to Air: Water Loop (heating mode)	< 135,000 Btu/h (cooling capacity)	, - ,	68°F entering water	4.3 COP	4.3 COP		
Water to Air: Ground Water (heating mode)	< 135,000 Btu/h (cooling capacity)	-	50°F entering water	3.7 COP	3.7 COP	ISO 13256-1	
Brine to Air: Ground Loop (heating mode)	< 135,000 Btu/h (cooling capacity)	_	32°F entering fluid	3.2 COP	3.2 COP		
Water to Water: Water Loop (heating mode)	< 135,000 Btu/h (cooling capacity)	=3	68°F entering water	3.7 COP	3.7 COP		
Water to Water: Ground Water (heating mode)	< 135,000 Btu/h (cooling capacity)	-	50°F entering water	3.1 COP	3.1 COP	ISO 13256-2	
Brine to Water: Ground Loop (heating mode)	< 135,000 Btu/h (cooling capacity)	-	32°F entering fluid	2.5 COP	2.5 COP		

For SI: 1 British thermal unit per hour = 0.2931 W, °C = [(°F) - 32]/1.8.

a. Chapter 6 contains a complete specification of the referenced test procedure, including the reference year version of the test procedure.

b. Single-phase, air-cooled air conditioners less than 65,000 Btu/h are regulated by NAECA. SEER values are those set by NAECA.

c. Minimum efficiency as of January 1, 2015.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWHcool*CF$

Where:

 ΔkWH = Annual cooling electricity savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0009106840

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.5.7 Packaged Terminal Air Conditioner (PTAC) - Packaged Terminal Heat Pump (PTHP)

DESCRIPTION

A PTAC is a packaged terminal air conditioner that cools and provides heat through an electric resistance heater (heat strip). A PTHP is a packaged terminal heat pump. A PTHP uses its compressor year-round to heat or cool. In warm weather, it efficiently captures heat from inside a space and pumps it outside for cooling. In cool weather, it captures heat from outdoor air and pumps it into a space, adding heat from electric heat strips as necessary to provide heat.

This measure characterizes:

- 1) Time of Sale: the purchase and installation of a new efficient PTAC or PTHP.
- 2) Early Replacement: the early removal of an existing PTAC or PTHP from service, prior to its natural end of life, and replacement with a new efficient PTAC or PTHP unit. Savings are calculated between existing unit and efficient unit consumption during the remaining life of the existing unit, and between new baseline unit and efficient unit consumption for the remainder of the measure life. The measure is only valid for non-fuel switching installations for example replacing a cooling only PTAC with a PTHP can currently not use the TRM.

This measure was developed to be applicable to the following program types: TOS, NC, and EREP.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to be PTACs or PTHPs that exceed baseline efficiencies.

DEFINITION OF BASELINE EQUIPMENT

TOS: the baseline conditions is <u>in provided in the 2015 IECC building code</u>, which is summarized in the Federal Baseline baseline reference table provided below.

EREP: the baseline is the existing PTAC or PTHP for the assumed remaining useful life of the unit and the new baseline as defined above for the remainder of the measure life.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years.¹⁷¹

Remaining life of existing equipment is assumed to be 5 years.¹⁷²

DEEMED MEASURE COST

TOS: The incremental capital cost for this equipment is estimated to be \$84/ton. 173

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¹⁷¹ Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007
¹⁷² Standard assumption of one third of effective useful life.

¹⁷³ DEER 2008. This assumes that baseline shifts between IECC versions carries the same incremental costs. Values should be verified during evaluation

EREP: The measure cost is the full cost of removing the existing unit and installing a new one. The actual program cost should be used. If unknown assume \$1,047 per ton. 174

The assumed deferred cost (after 5 years) of replacing existing equipment with new baseline unit is assumed to be \$1,039 per ton.¹⁷⁵ This cost should be discounted to present value using the utilities' discount rate.

LOADSHAPE

Cooling BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Electric savings for PTACs and PTHPs should be calculated using the following algorithms

ENERGY SAVINGS

TOS:

```
PTAC \Delta kWh^{176} = \Delta kWh_{cool}
```

PTHP
$$\Delta kWh$$
 = $\Delta kWh_{cool} + \Delta kWh_{heat}$

$$\Delta kWh_{cool}$$
 = kBtu/hr_{cool} * (1/EER_{base} - 1/EER_{ee}) * EFLH_{cool}

$$\Delta kWh_{heat}$$
 = kBtu/hr_{heat} / 3.412 * (1/COP_{base} - 1/COP_{ee}) * EFLH_{heat}

EREP:

∆kWh for remaining life of existing unit (1st 5years)

```
\Delta kWh \hspace{1cm} = \Delta kWh_{cool} + \Delta kWh_{heat}
```

$$\Delta kWh_{cool}$$
 = kBtu/hr_{cool} * (1/EER_{exist} - 1/EER_{ee}) * EFLH_{cool}

$$\Delta kWh_{heat}$$
 = kBtu/hr_{heat} / 3.412 * (1/COP_{exist} - 1/COP_{ee}) * EFLH_{heat}

∆kWh for remaining measure life (next 10 years)

$$\Delta kWh$$
 = $\Delta kWh_{cool} + \Delta kWh_{heat}$

$$\Delta kWh_{cool}$$
 = $kBtu/hr_{cool} * (1/EER_{base} - 1/EER_{ee}) * EFLH_{cool}$

$$\Delta kWh_{heat}$$
 = kBtu/hr_{heat} / 3.412 * (1/COP_{base} – 1/COP_{ee}) * EFLH_{heat}

Where:

 $^{^{\}rm 174}$ Based on DCEO – IL PHA Efficient Living Program data.

¹⁷⁵ Based on subtracting TOS incremental cost from the DCEO data and incorporating inflation rate of 1.91%.

¹⁷⁶ There are no heating efficiency improvements for PTACs since although some do provide heating, it is always through electric resistance and therefore the COPbase and COPee would be 1.0.

$kBtu/hr_{cool} =$	Capacity of the	cooling equipment	in kBtu per hour ((1 ton of cooling
--------------------	-----------------	-------------------	--------------------	-------------------

capacity equals 12 kBtu/hr).

= Actual installed

EFLH_{cool} = Equivalent Full Load Hours for cooling are provided in section 2.7

HVAC End Use

EFLH_{heat} = Equivalent Full Load Hours for heating are provided in section 2.7

HVAC End Use

EER_{exist} = Energy Efficiency Ratio of the existing equipment

= Actual. If unknown assume 8.1 EER¹⁷⁷

EER_{base} = Energy Efficiency Ratio of the baseline equipment.

= See the table below for requirements <u>based on 2015 IECC.the Code</u> <u>of Federal Regulations</u>. Note the compliance data is applicable to the <u>date of manufacture</u>, and not the date of <u>purchase</u>, where local code is <u>based on IECC</u>. Content is based on tables 503.3.3(3) (IECC 2009) and C403.2.3(3) (IECC 2012, 2015): Minimum Efficiency Requirements: Electrically operated packaged terminal air conditioners, packaged terminal heat pumps. An alternate, custom input may be necessary for jurisdictions recognizing alternative code.

EER_{ee} = Energy Efficiency Ratio of the energy efficient equipment. For air-

cooled units < 65 kBtu/hr, if the actual EERee is unknown, assume the following conversion from SEER to EER for calculation of peak

savings: 178 EER = $(-0.02 * SEER^2) + (1.12 * SEER)$

= Actual installed

kBtu/hr_{heat} = Capacity of the heating equipment in kBtu per hour.

= Actual installed

3.412 = Btu per Wh.

COP_{exist} = Coefficient of performance of the existing equipment

= Actual. If unknown assume 1.0 COP for PTAC units and 2.6 COP¹⁷⁹

for PTHPs.

COP_{base} = Coefficient of performance of the baseline equipment; see table

above below for values.

COP_{ee} = Coefficient of performance of the energy efficient equipment.

= Actual installed

IECC Minimum Efficiency Requirements

Equipment Type	HECC 2009	IECC 2012 Minimum	HECC 2015	
	Minimum Efficiency	Efficiency	Minimum Efficiency	

 $^{^{177}\,\}mathrm{Estimated}$ using the IECC building energy code up until year 2003 (p107;

https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; EER = 10 - (0.16 * 12,000/1,000) = 8.1.
¹⁷⁸ Based on Wassmer, M. (2003). A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations. Masters Thesis, University of Colorado at Boulder. Note this is appropriate for single speed units only.
¹⁷⁹ Estimated using the IECC building energy code up until year 2003 (p107;

https://law.resource.org/pub/us/code/ibr/icc.iecc.2000.pdf) and assuming a 1 ton unit; COP = 2.9 - (0.026 * 12,000/1,000) = 2.6.

PTAC (Cooling mode)	12.5 - (0.213 .	13.8 - (0.300 x	14.0 – (0.300 x
New Construction	Cap/1000) EER	Cap/1000) EER	Cap/1000) EER
PTAC (Cooling mode)	10.9 (0.213 .	10.9 (0.213 x	10.9 (0.213 x
Replacements	Cap/1000) EER	Cap/1000) EER	Cap/1000) EER
PTHP (Cooling mode)	12.3 - (0.213 .	14.0 - (0.300 x	14.0 – (0.300 x
New Construction	Cap/1000) EER	Cap/1000) EER	Cap/1000) EER
PTHP (Cooling mode)	10.8 (0.213 .	10.8 (0.213 x	10.8 (0.213 x
Replacements	Cap/1000) EER	Cap/1000) EER	Cap/1000) EER
PTHP (Heating mode)	3.2 - (0.026 .	3.2 - (0.026 x Cap/1000)	3.2 - (0.026 x Cap/1000)
New Construction	Cap/1000) COP	COP	COP
PTHP (Heating mode)	2.9 (0.026 .	2.9 (0.026 x Cap/1000)	2.9 (0.026 x Cap/1000)
Replacements	Cap/1000) COP	COP	COP

[&]quot;Cap" = The rated cooling capacity of the project in Btu/hr. If the unit's capacity is less than 7000 Btu/hr, use 7,000 Btu/hr in the calculation. If the unit's capacity is greater than 15,000 Btu/hr, use 15,000 Btu/hr in the calculations.

Replacement unit shall be factory labeled as follows: "MANUFACTURED FOR REPLACEMENT APPLICATIONS ONLY; NOT TO BE INSTALLED IN NEW

CONSTRUCTION PROJECTS," Replacement efficiencies apply only to units with existing sleeves less than 16 inches (406mm) in height and less than 42 inches (1067 mm) in width.

2015 IECC Building Code Baseline Efficiencies

Equipment Type	Category	Efficiency Levela	
PTAC	New Construction	$EER = 14 - (0.3 \times Cap/1000)$	
	Replacements ^b	$EER = 10.9 - (0.213 \times Cap/1000)$	
РТНР	New Construction	$EER = 14.0 - 0.3 \times Cap/1000$	
		$COP = 3.7 - (0.052 \times Cap/1000)$	
	Replacements ^b	$EER = 10.8 - (0.213 \times Cap/1000)$	
		$COP = 2.9 - (0.026 \times Cap/1000)$	

^a "Cap" = The rated cooling capacity of the project in Btu/hr. If the unit's capacity is less than 7000 Btu/hr, use 7,000 Btu/hr in the calculation. If the unit's capacity is greater than 15,000 Btu/hr, use 15,000 Btu/hr in the calculations.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

TOS:

 $\Delta kW = \Delta kWH_{cool} * CF$

EREP:

ΔkW for remaining life of existing unit (1st 5years)

b Replacement unit shall be factory labeled as follows "MANUFACTURED FOR REPLACEMENT APPLICATIONS ONLY; NOT TO BE INSTALLED IN NEW CONSTRUCTION PROJECTS".
 Replacement efficiencies apply only to units with existing sleeves less than 16 inches (406mm) in height and less than 42 inches (1067 mm) in width.

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Appendix H - TRM - Vol. 2: C&I Measures

 $\Delta kW = \Delta kW_{(1st \, 5 \, years)} * CF$ ΔkW for remaining measure life (next 10 years)

 $\Delta kW = \Delta kW$ (next 10 years) * CF

Where:

 $\Delta kWH_{cool} \ = Annual \ cooling \ electricity \ savings, \ as \ calculated \ above$

CF = Summer peak coincidence demand (kW) to annual energy (kWh)

factor for cooling = 0.0009106840

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.5.8 Single-Package and Split System Unitary Air Conditioner

DESCRIPTION

This measure promotes the installation of high-efficiency unitary air-, water-, and evaporatively cooled air conditioning equipment, both single-package and split systems. Air conditioning (AC) systems are a major consumer of electricity and systems that exceed baseline efficiencies can save considerable amounts of energy. This measure could apply to the replacement of an existing unit at the end of its useful life or the installation of a new unit in a new or existing building.

This measure was developed to be applicable to the following program types: TOS and NC. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to be a high-efficiency air-, water-, or evaporatively cooled air conditioner that exceeds both the full load and part-load efficiencies associated with the applicable code described in the Definition of Baseling Equipment energy efficiency requirements specified by the building code applicable to local jurisdiction, prior to January 1, 2024. This may be a version of the 2009, 2012 or 2015 IECC or ASHRAE 90.1 standard. After January 1, 2024, the applicable building code is 2015 IECC.

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline equipment is assumed to be a standard-efficiency air-, water, or evaporatively cooled air conditioner that meets the <u>2015 IECC</u> energy efficiency requirements of local building code, effective January 1, 2024.

Prior to January 1, 2024, the applicable baseline is assumed be similar equipment meeting the energy efficiency requirements of local building code. When local code does not exist, use of IECC 2012 is defined as the building code baseline.

The rating conditions for the baseline and efficient equipment efficiencies must be equivalent.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years. 180

DEEMED MEASURE COST

MEEIA 2019-21 Plan

The incremental capital cost for this measure is assumed to be \$100 per ton. 181

LOADSHAPE

Cooling BUS

Algorithm

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¹⁸⁰ Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, Inc., June 2007

¹⁸¹ Based on a review of TRM incremental cost assumptions from Vermont, Wisconsin, and California. This assumes that baseline shift from between IECC versions carries the same incremental costs. Values should be verified during evaluation.

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

For units with cooling capacities less than 65 kBtu/hr:

 $\Delta kWH = kBtu/hr * (1/SEERbase - 1/SEERee) * EFLH$

For units with cooling capacities equal to or greater than 65 kBtu/hr:

 $\Delta kWH = kBtu/hr * (1/IEERbase - 1/IEERee) * EFLH$

Where:

kBtu/hr = Capacity of the cooling equipment actually installed in kBtu per hour (1 ton of cooling capacity equals 12 kBtu/hr)

 $SEER_{base} \ = Seasonal \ Energy \ Efficiency \ Ratio \ of the \ baseline \ equipment$

= SEER values from tables below, based on the applicable IECC.

= For units with cooling capacity <65kbtu/hr and efficient unit is measured in terms of SEER2, convert SEER_{base} to SEER2_{base}. ¹⁸², if applicable code is based on IECC, or custom input as necessary.

SEER_{ee} = Seasonal Energy Efficiency Ratio of the energy efficient equipment (actually installed)

IEER_{base} = Integrated Energy Efficiency Ratio of the baseline equipment

= IEER values from tables below, based on the applicable IECC, if applicable code is based on IECC, or custom input as necessary.

IEER_{ee} = Integrated Energy Efficiency Ratio of the energy efficient equipment

(actually installed.)

EFLH = Equivalent Full Load Hours for cooling are provided in section 2.7 HVAC

End Use

¹⁸² SEER to SEER2 conversion factor: SEER2 = SEER x 96%. Conversion factor for SEER to SEER2 is used when converting an existing system that is rated in SEER to SEER2. This is to meet the DOE M1 CFR Standard beginning January 1, 2023. The efficiency levels of the existing, baseline, and efficient case must be expressed in the same metrics (e.g., both SEER or SEER2) before applying formulas.

2009 IECC Minimum Efficiency Requirements

TABLE 503.2.3(1)

EQUIPMENT TYPE	SIZE CATEGORY	SUBCATEGORY OR RATING CONDITION	MINIMUM EFFICIENCy	TEST PROCEDURE	
Air conditioners, Air cooled	- 45 000 P. 04	Split system	13.0 SEER		
	< 65,000 Btu/h ^d	Single package 13.0 SEER			
	≥ 65,000 Btu/h and < 135,000 Btu/h	Split system and single package	10.3 EERc (before Jan 1, 2010) 11.2 EERc (as of Jan 1, 2010)	AHRI210/240	
	≥ 135,000 Btu/h and < 240,000 Btu/h	Split system and single package	9.7 EERc (before Jan 1, 2010) 11.0 EERc (as of Jan 1, 2010)	AHRI 340/360	
	≥ 240,000 Btu/h and < 760,000 Btu/h	Split system and single package	9.5 EERc 9.7 IPLYc (before Jan 1, 2010) 10.0 EERc 9.7 IPLyg (as of Jan 1, 2010)		
	≥ 760,000 Btu/h	Split system and single package	9.2 EERc 9.4 IPLYc (before Jan 1, 2010) 9.7 EERc 9.4 IPLYc (as of Jan 1, 2010)		
Through-the-wall, Air cooled	< 30.000 Btu/h ^d	Split system	10.9 SEER (before Jan 23, 2010) 12.0 SEER (as of Jan 23,2010)	AHRI210/240	
	- 30,000 Dian	Single package	10.6 SEER (before Jan 23, 2010) 12.0 SEER (as of Jan 23,2010)		
Air conditioners, Water and evaporatively cooled	< 65,000 Btu/h	Split system and single package	12.1 EER	AHRI210/240	
	≥ 65,000 Btu/h and < 135,000 Btu/h	Split system and single package	11.5 EERe		
	≥ 135,000 Btu/h and < 240,000 Btu/h	Split system and single package	11.0 EERe	AHRI 340/360	
	≥ 240,000 Btu/h		11.5 EERe		

For SI: 1 British thermal unit per hour = 0.2931 W
a. Chapter 6 contains a complete specification of the referenced test procedure, including the referenced year wrising of the test procedure.
b. IPLVs are only applicable to equipment with capacity modulation.
c. Deduct 0.2 from the required EERs and IPLVs for units with a heating section other than electric resistance heat.
d. Single-phase air-cooled air conditioners < 65,000 Btulh are regulated by the National Appliance Energy Conservation Act of 1987 (NAECA); SEER values are those set by NAECA.

2012 IECC Minimum Efficiency Requirements

TABLE C403.2.3(1) MINIMUM EFFICIENCY REQUIREMENTS:

EQUIPMENT TYPE	SIZE CATEGORY	HEATING SECTION TYPE	SUBCATEGORY OR RATING CONDITION	MINIMUM EFFICIENCY		TEST
				Before 6/1/2011	As of 6/1/2011	PROCEDURE
Air conditioners, air cooled	< 65,000 Btu/h ^b	All	Split System	13.0 SEER	13.0 SEER	AHRI 210/240
			Single Package	13.0 SEER	13.0 SEER	
Through-the-wall	≤ 30,000 Btu/h ^b	All	Spltt system	12.0 SEER	12.0 SEER	
(atr cooled)			Single Package	12.0 SEER	12.0 SEER	
Small-duct high-velocity (air cooled)	< 65,000 Btu/hb	All	Split System	10.0 SEER	10.0 SEER	
Air conditioners.	≥ 65,000 Btu/h and < 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.2 EER 11.4 IEER	11.2 EER 11.4 IEER	AHRI 340/360
		All other	Split System and Single Package	11.0 EER 11.2 IEER	11.0 EER 11.2 IEER	
	≥ 135,000 Btu/h and < 240,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER	11.0 EER 11.2 IEER	
		All other	Split System and Single Package	10.8 EER 11.0 IEER	10.8 EER 11.0 IEER	
air cooled	≥ 240,000 Btu/h and < 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	10.0 EER 10.1 IEER	10.0 EER 10.1 IEER	
		All other	Split System and Single Package	9.8 EER 9.9 IEER	9.8 EER 9.9 IEER	
	≥ 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	9.7 EER 9.8 IEER	9.7 EER 9.8 IEER	
		All other	Split System and Single Package	9.5 EER 9.6 IEER	9.5 EER 9.6 IEER	
Air conditioners, water cooled	< 65,000 Btu/h ^b	All	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 12.3 IEER	AHRI 210/240
	≥ 65,000 Btu/h and < 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.5 EER 11.7 IEER	12.1 EER 12.3 IEER	AHRI 340/360
		All other	Split System and Single Package	11.3 EER 11.5 IEER	11.9 EER 12.1 IEER	
	≥ 135,000 Btu/h and < 240,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER	12.5 EER 12.7 IEER	
		All other	Split System and Single Package	10.8 EER 11.0 IEER	12.3 EER 12.5 IEER	
	≥ 240,000 Btu/h and < 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.1 IEER	12.4 EER 12.6 IEER	
		All other	Split System and Single Package	10.8 EER 10.9 IEER	12.2 EER 12.4 IEER	
	≥ 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.1 IEER	12.0 EER 12.4 IEER	
		All other	Split System and Single Package	10.8 EER 10.9 IEER	12.0 EER 12.2 IEER	

(continued)

TABLE C403.2.3(1)—continued MINIMUM EFFICIENCY REQUIREMENTS: ELECTRICALLY OPERATED UNITARY AIR CONDITIONERS AND CONDENSING UNITS

EQUIPMENT TYPE	SIZE CATEGORY	HEATING	SUB-CATEGORY OR	MINIMUM E	TEST		
EQUIPMENT TYPE	SIZE CATEGORY	SECTION TYPE	RATING CONDITION	Before 6/1/2011	As of 6/1/2011	PROCEDURE:	
	< 65,000 Btu/h ^b	All	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 12.3 IEER	AHRI 210/240	
	≥ 65,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.5 EER 11.7 IEER	12.1 EER 12.3 IEER	.,	
	< 135,000 Btu/h	All other	Split System and Single Package	11.3 EER 11.5 IEER	11.9 EER 12.1 IEER		
	≥ 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER	12.0 EER 12.2 IEER		
Air conditioners, evaporatively cooled	< 240,000 Btu/h	All other	Split System and Single Package	10.8 EER 11.0 IEER	11.8 EER 12.0 IEER	AHRI	
	≥ 240,000 Btu/h and < 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.1 IEER	11.9 EER 12.1 IEER	340/360	
		All other	Split System and Single Package	10.8 EER 10.9 IEER	12.2 EER 11.9 IEER		
	≥ 760.000 Btu/h	Electric Resistance (or None)	Split System and Single Package	10.0 EER 11.1 IEER	11.7 EER 11.9 IEER		
2 760,000 Btt	2 700,000 Btu/li	All other	Split System and Single Package	10.8 EER 10.9 IEER	11.5 EER 11.7 IEER		
Condensing units, air cooled	≥ 135,000 Btu/h			10.1 EER 11.4 IEER	10.5 EER 14.0 IEER		
Condensing units, water cooled	≥ 135,000 Btu/h			13.1 EER 13.6 IEER	13.5 EER 14.0 IEER	AHRI 365	
Condensing units, evaporatively cooled	≥ 135,000 Btu/h			13.1 EER 13.6 IEER	13.5 EER 14.0 IEER		

For SI: 1 British thermal unit per hour = 0.2931 W.

a. Chapter 6 of the referenced standard contains a complete specification of the referenced test procedure, including the reference year version of the test procedure.

b. Single-phase, air-cooled air conditioners less than 65,000 Btu/h are regulated by NAECA. SEER values are those set by NAECA.

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2015 IECC Minimum Efficiency Requirements

TABLE C403.2.3(1)

MINIMUM EFFICIENCY REQUIREMENTS:
ELECTRICALLY OPERATED LINITARY AND CONDITIONERS AND CONDENSING LINIT

EQUIPMENT TYPE	SIZE CATEGORY	HEATING	SUBCATEGORY OR	MINIMUM E	TEST	
EQUIPMENT TIPE	SIZE CATEGORY	SECTION TYPE	RATING CONDITION	Before 1/1/2016	As of 1/1/2016	PROCEDURE
Air conditioners.	- (C 000 D- 1)	433	Split System	13.0 SEER.	13.0 SEER	
air cooled	< 65,000 Btu/h ^b	All	Single Package	13.0 SEER	14.0 SEER ^c	
Through-the-wall	< 20 000 P. 13		Split system	12.0 SEER	12.0 SEER	AHRI
(air cooled)	≤ 30,000 Btu/h ^b	All	Single Package	12.0 SEER	12.0 SEER	210/240
Small-duct high-velocity (air cooled)	< 65,000 Btu/h ^b	All	Split System	11.0 SEER	11.0 SEER	
	≥ 65,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.2 EER 11.4 IEER	11.2 EER 12.8 IEER	
	< 135,000 Btu/h	All other	Split System and Single Package	11.0 EER 11.2 IEER	11.0 EER 12.6 IEER	1
	≥ 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.0 EER 11.2 IEER	11.0 EER 12.4 IEER	1
Air conditioners.	and < 240,000 Btu/h	All other	Split System and Single Package	10.8 EER 11.0 IEER	10.8 EER 12.2 IEER	AHRI 340/360
air cooled ≥ 240 < 760	≥ 240,000 Btu/h and < 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	10.0 EER 10.1 IEER	10.0 EER 11.6 IEER	
		All other	Split System and Single Package	9.8 EER 9.9 IEER	9.8 EER 11.4 IEER	
	≥ 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	9.7 EER 9.8 IEER	9.7 EER 11.2 IEER	
		All other	Split System and Single Package	9.5 EER 9.6 IEER	9.5 EER 11.0 IEER	1
	< 65,000 Btu/h ^b	All	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 12.3 IEER	AHRI 210/240
	≥ 65,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 13.9 IEER	
	< 135,000 Btu/h	All other	Split System and Single Package	11.9 EER 12.1 IEER	11.9 EER 13.7 IEER	
	≥ 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	12.5 EER 12.5 IEER	12.5 EER 13.9 IEER	1
Air conditioners, water cooled	< 240,000 Btu/h	All other	Split System and Single Package	12.3 EER 12.5 IEER	12.3 EER 13.7 IEER	AHRI
	≥ 240,000 Btu/h and	Electric Resistance (or None)	Split System and Single Package	12.4 EER 12.6 IEER	12.4 EER 13.6 IEER	340/360
	< 760,000 Btu/h	All other	Split System and Single Package	12.2 EER 12.4 IEER	12.2 EER 13.4 IEER	1
	750 000 Dr. 1	Electric Resistance (or None)	Split System and Single Package	12.2 EER 12.4 IEER	12.2 EER 13.5 IEER	
	≥ 760,000 Btu/h	All other	Split System and Single Package	12.0 EER 12.2 IEER	12.0 EER 13.3 IEER	

(continued)

TABLE C403.2.3(1)—continued MINIMUM EFFICIENCY REQUIREMENTS:

EQUIPMENT TYPE	SIZE CATEGORY	HEATING SECTION TYPE	SUB-CATEGORY OR	MINIMUM E	FFICIENCY	TEST PROCEDURE*
COOPMENT TIPE	SIZE CATEGORY		RATING CONDITION	Before 1/1/2016	As of 1/1/2016	
	< 65,000 Btu/h ^b	All	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 12.3 IEER	AHRI 210/240
	≥ 65,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	12.1 EER 12.3 IEER	12.1 EER 12.3 IEER	
	< 135,000 Btu/h	All other	Split System and Single Package	11.9 EER 12.1 IEER	11.9 EER 12.1 IEER	1
	≥ 135,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	12.0 EER 12.2 IEER	12.0 EER 12.2 IEER	AHRI 340/360
evaporatively cooled ≥ 240,000 Btv and	<240,000 Btu/h	All other	Split System and Single Package	11.8 EER 12.0 IEER	11.8 EER 12.0 IEER	
	≥ 240,000 Btu/h and < 760,000 Btu/h	Electric Resistance (or None)	Split System and Single Package	11.9 EER 12.1 IEER	11.9 EER 12.1 IEER	
		All other	Split System and Single Package	11.7 EER 11.9 IEER	11.7 EER 11.9 IEER	
	> 760 000 Pm &	Electric Resistance (or None)	Split System and Single Package	11.7 EER 11.9 IEER	11.7 EER 11.9 IEER]
	2 700,000 Billing	All other	Split System and Single Package	11.5 EER 11.7 IEER	11.5 EER 11.7 IEER	
Condensing units, air cooled	≥ 135,000 Btu/h			10.5 EER 11.8 IEER	10.5 EER 11.8 IEER	
Condensing units, water cooled	≥ 135,000 Btu/h			13.5 EER 14.0 IEER	13.5 EER 14.0 IEER	AHRI 365
Condensing units, evaporatively cooled	≥ 135,000 Btu/h			13.5 EER 14.0 IEER	13.5 EER 14.0 IEER	

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWH * CF$

Where:

ΔkWH = Annual electricity savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

for Cooling = 0.0009106840

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

For SI: 1 British thermal unit per hour = 0.2931 W.

a. Chapter 6 contains a complete specification of the referenced test procedure, including the reference year version of the test procedure.

b. Single-phase, air-cooled air conditioners less than 65,000 Bru/h are regulated by NAECA. SEER values are those set by NAECA.

c. Minimum efficiency as of Jamany 1, 2015.

2.5.9 High Volume Low Speed Fans

DESCRIPTION

The measure applies to 20-24 foot diameter horizontally mounted ceiling high volume low speed (HVLS) fans that are replacing multiple non HVLS fans that have reached the end of useful life.

This measure was developed to be applicable to the following program types: TOS and RF If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to be classified as HVLS and have a VFD.¹⁸³

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline condition is assumed to be multiple non HVLS existing fans that have reached the end of useful life.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 10 years, $\frac{183}{4}$

DEEMED MEASURE COST

The incremental capital cost for the fans are as follows: 183174

Fan Diameter Size (feet)	Incremental Cost
20	\$4150
22	\$4180
24	\$4225

LOADSHAPE

HVAC BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS 183174

The annual electric savings from this measure are deemed values depending on fan size and apply to all building types:

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^{183 &}quot;Illinois Statewide Technical Reference Manual for Energy Efficiency Version 8.0, Volume 2: Commercial and Industrial Measures," Section 4.1.2, High Volume Low Speed Fans.

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Fan Diameter Size (feet)	kWh Savings
20	6,577
22	8,543
24	10,018

SUMMER COINCIDENT PEAK DEMAND SAVINGS184

 $\Delta kW = h * CF$

Where:

 ΔkWh = Electric energy savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.00044\overline{3983}$

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

 $^{^{184}}$ "Illinois Statewide Technical Reference Manual for Energy Efficiency Version 8.0, Volume 2: Commercial and Industrial Measures," Section 4.1.2, High Volume Low Speed Fans.

2.5.10 Chiller Tune Up

DESCRIPTION

This measure is the tune-up of an existing air-cooled or water-cooled electric chiller. The tune-up consists of tube cleaning, chilled and condenser water temperature adjustments, and reciprocating compressor unloading switch adjustments.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient condition is an existing chiller post tune-up.

DEFINITION OF BASELINE EQUIPMENT

The baseline condition is an existing chiller prior to receiving the tune-up.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected lifetime of the measure is 5 years.

DEEMED MEASURE COST

The incremental cost for this measure varies. Use actual cost.

DEEMED O&M COST ADJUSTMENTS

There are no expected O&M cost adjustments for this measure.

BASELINE EFFICIENCY VALUES BY CHILLER TYPE AND CAPACITY

Refer to 2012 IECC Minimum Efficiency Requirements in Reference Tables section of this measure.

LOADSHAPE

Cooling BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS185

 $\Delta kWh = TONS * IPLVBASE * EFLH * ESF$

Where:

TONS = Chiller nominal cooling capacity in tons (= actual; 1 ton = 12,000 Btu/hr)

IPLV_{BASE} = Efficiency of baseline equipment expressed as Integrated Part Load Value (kW/ton). Chiller units are dependent on chiller type. See 'Chiller Units,

Conversion Values' and 'Baseline Efficiency Values by Chiller Type' and

Conversion Values' and 'Baseline Efficiency Values by Chiller Type' and Capacity in the Reference Tables section within this measure section.

= Equivalent full load hours (= dependent on location and building type,

see table 2.5 in Appendix H)

ESF = Energy savings factor (= 0.08)

MEEIA 2019-21 Plan

EFLH

Revision 4.0<u>5.0</u>

¹⁸⁵ "Indiana Technical Reference Manual Version 2.2," Page 217.

For example, energy savings for the tune-up of a 350-ton chiller with an IPLV of .540kW/Ton serving a Medium Office in St Louis is calculated as:

$$\Delta kWh = TONS * IPLVBASE * EFLH * ESF = 350 * .540 * 1386 * 0.08 = 20,956 kWh$$

SUMMER COINCIDENT PEAK DEMAND SAVINGS186

 $\Delta kW = \Delta kWh * CF$

Where:

ΔkWh = Electric energy savings, as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor for Cooling (0.0009106840)

For example, demand reduction for the tune-up of the above chiller resulting in 20,956 kWh of energy savings is calculated as:

$$\Delta kW = 20,956 \text{ kWh} * 0.0009106840 = 19.08 \text{ kW}$$

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

REFERENCE TABLES

Chillers Ratings - Chillers are rated with different units based on equipment type as shown below

Equipment Type	Unit
Air cooled, electrically operated	EER
Water cooled, electrically operated, positive displacement (reciprocating)	kW/ton
Water cooled, electrically operated, positive displacement (rotary screw and scroll)	kW/ton

In order to convert chiller equipment ratings to IPLV the following relationships are provided:

kW/ton = 12 / EER

kW/ton = $12 / (COP \times 3.412)$ COP = EER / 3.412

¹⁸⁶ Indiana Technical Reference Manual Version 2.2," Page 219.

Ameren Missouri

Appendix H - TRM - Vol. 2: C&I Measures

COP = 12 / (kW/ton) / 3.412

EER = 12 / kW/ton**EER** $= COP \times 3.412$

2012 IECC Baseline Efficiency Values by Chiller Type and Capacity¹⁸⁷

TABLE C403.2.3(7) MINIMUM EFFICIENCY REQUIREMENTS: WATER CHILLING PACKAGES*

			BEFORE 1/1/2010			AS OF 1	/1/2010 ^b	Uhren I	
	7.00				PAT	TH A	PAT	НВ	T 1977
EQUIPMENT TYPE	SIZE		FULL	IPLV	FULL	IPLV	FULL	IPLV	TEST PROCEDURES
A	< 150 tons	EER	≥ 9.562	≥10.4	≥ 9.562	≥ 12.500	NA	NA	
Air-cooled chillers	≥ 150 tons	EER	29.562	16	≥ 9.562	≥ 12.750	NA	NA	1
Air cooled without condenser, electrical operated	All capacities	EER	≥ 10.586	≥ 11.782	Air-cooled chillers without condens- ers shall be rated with matching con- densers and comply with the air-cooled chiller efficiency requirements		ng con- ir-cooled	11	
Water cooled, electrically operated, reciprocating	All capacities	kW/ton	≤ 0.837	≤ 0.696	water coo	ating units oled positiv y requirem	ve displac		
	< 75 tons	kW/ton			≤ 0.780	≤ 0.630	≤ 0.800	≤ 0.600	
Water cooled, electrically operated, post-	≥ 75 tons and < 150 tons	kW/ton	≤ 0.790	≤ 0.676	≤ 0.775	≤ 0.615	≤ 0.790 ≤	≤ 0.586	AHRI 550/590
tive displacement	≥ 150 tons and < 300 tons	kW/ton	≤ 0.717	≤ 0.627	≤ 0.680	≤ 0.580	≤ 0.718	≤ 0.540	
	≥ 300 tons	kW/ton	≤ 0.639	≤ 0.571	≤ 0.620	≤ 0.540	≤ 0.639	≤ 0.490	
	< 150 tons	kW/ton	≤ 0.703	≤ 0.669	≤ 0.634	0.634 ≤ 0.596			1
Water cooled, electrically operated,	≥ 150 tons and < 300 tons	kW/ton	≤ 0.634	≤ 0.596			≤ 0.639	≤ 0.450	-
centrifugal	≥ 300 tons and < 600 tons	kW/ton	≤ 0.576	≤ 0.549	≤ 0.576	≤ 0.549	≤ 0.600	≤ 0.400	
	≥ 600 tons	kW/ton	≤ 0.576	≤ 0.549	≤ 0.570	≤ 0.539	≤ 0.590	≤ 0.400	1
Air cooled, absorption single effect	All capacities	COP	≥ 0.600	NR	≥ 0.600	NR	NA	NA	
Water cooled, absorption single effect	All capacities	COP	≥ 0.700	NR	≥0.700	NR	NA	NA	AHRI 560
Absorption double effect, indirect fired	All capacities	COP	≥ 1.000	≥ 1.050	≥ 1.000	≥ 1.050	NA	NA	
Absorption double effect, direct fired	All capacities	COP	≥ 1.000	≥ 1.000	≥ 1.000	≥ 1.000	NA	NA	

For SI: 1 ton = 3517 W, 1 British thermal unit per hour = 0.2931 W, "C = [("F) - 32]/1.8.

NA = Not applicable, not to be used for compliance; NR = No requirement.

a. The centrifugal chiller equipment requirements, after adjustment in accordance with Section C403.2.3.1 or Section C403.2.3.2, do not apply to chillers used in low-temperature applications where the design leaving fluid temperature is less than 36°F. The requirements do not apply to positive displacement chillers with leaving fluid temperatures less than or equal to 32°F. The requirements do not apply to absorption chillers with design leaving fluid temperatures less than 60°F.

No compliance with this readed on the state of the second of the

b. Compliance with this standard can be obtained by meeting the minimum requirements of Path A or B. However, both the full load and IPLV shall be met to fulfill
the requirements of Path A or B.
 c. Chapter 6 of the referenced standard contains a complete specification of the referenced test procedure, including the referenced year version of the test

¹⁸⁷ Note: Efficiency requirements depend on the path (Path A or Path B) that the building owner has chosen to meet compliance requirements. For air cooled and absorption chillers, Path A should be assumed. For water cooled chillers, the building owner should be consulted, and the relevant path used for calculations. When unknown, Path A should be used.

2015 IECC Baseline Efficiency Values by Chiller Type and Capacity

TABLE C403.2.3(7)
WATER CHILLING PACKAGES - FEBRUENCY DECLIDEMENTS A M.

		UNITS	BEFORE 1/1/2015		AS OF	TEST				
EQUIPMENT TYPE	SIZE CATEGORY		Path A	Path B	Path A	Path B	PROCEDURE*			
						≥ 9.562 FL		≥ 10.100 FL	≥ 9.700 FL	
	< 150 Tons	EER	≥ 12.500 IPLV	NA°	≥ 13.700 IPLV	≥ 15,800 IPLV				
Air-cooled chillers	S 100 m	(Btu/W)	≥ 9.562 FL	NA°	≥ 10.100 FL	≥ 9.700 FL	İ			
	≥ 150 Tons		≥ 12.500 IPLV	NA.	≥ 14.000 IPLV	≥ 16.100 IPLV	t			
Air cooled without condenser, electrically operated	All capacities	EER (Btu/W)		Air-cooled chillers without condenser shall be rated with matching condensers and complying with air-cooled chiller efficiency requirements.						
	< 75 Tons		≤ 0.780 FL	≤0.800 FL	≤ 0.750 FL	≤ 0.780 FL	Ī			
	< /3 Tolls		≤ 0.630 IPLV	≤ 0.600 IPLV	≤ 0.600 IPLV	≤ 0.500 IPLV	İ			
	≥ 75 tons and < 150 tons		≤ 0.775 FL	≤0.790 FL	≤ 0.720 FL	≤ 0.750 FL	Ī			
	≥ /5 tons and < 150 tons		≤0.615 IPLV	≤ 0.586 IPLV	≤ 0.560 IPLV	≤ 0.490 IPLV	Ī			
Water cooled, electrically operated positive	≥ 150 tons and < 300 tons	kW/ton	≤ 0.680 FL	≤0.718 FL	≤ 0.660 FL	≤0.680 FL	İ			
displacement	≥ 150 tons and < 500 tons	nonwa	≤ 0.580 IPLV	≤ 0.540 IPLV	≤ 0.540 IPLV	≤ 0.440 IPLV	AHRI 550/ 590			
- All	≥ 300 tons and < 600 tons		≤ 0.620 FL	≤0.639 FL	≤ 0.610 FL	≤ 0.625 FL				
	2 300 tons and < 600 tons		≤0.540 IPLV	≤ 0.490 IPLV	≤ 0.520 IPLV	≤ 0.410 IPLV				
	≥ 600 tons		≤ 0.620 FL	≤0.639 FL	≤ 0.560 FL	≤ 0.585 FL				
			≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV				
	< 150 Tons		≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.695 FL				
	< 150 Tolls		≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.440 IPLV				
	≥ 150 tons and < 300 tons ≥ 300 tons and < 400 tons		≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.635 FL				
			≤0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.400 IPLV				
Water cooled, electrically			kW/ton	≤ 0.576 FL	≤0.600 FL	≤ 0.560 FL	≤ 0.595 FL	Ī		
operated centrifugal		kW/ton	≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.520 IPLV	≤ 0.390 IPLV				
	≥ 400 tons and < 600 tons		≤ 0.576 FL	≤0.600 FL	≤ 0.560 FL	≤ 0.585 FL				
	= 400 tons and < 000 tons		≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV	Ī			
	≥ 600 Tons		≤ 0.570 FL	≤0.590 FL	≤ 0.560 FL	≤ 0.585 FL	Ī			
	2 000 10ms		≤ 0.539 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV				
Air cooled, absorption, single effect	All capacities	COP	≥ 0.600 FL	NA°	≥ 0.600 FL	NA°				
Water cooled absorption, single effect	All capacities	COP	≥ 0.700 FL	NA°	≥ 0.700 FL	NA°	AHRI 560			
Absorption, double effect, indirect fired	All capacities	COP	≥ 1.000 FL ≥ 1.050 IPLV	NA°	≥ 1.000 FL ≥ 1.050 IPLV	NA°				
Absorption double effect direct fired	All capacities	COP	≥ 1.000 FL ≥ 1.000 IPLV	NA°	≥ 1.000 FL ≥ 1.050 IPLV	NA°				

a. The requirements for centrifugal chiller shall be adjusted for nonstandard rating conditions in accordance with Section C403.2.3.1 and are only applicable for the range of conditions listed in Section C403.2.3.1. The requirements for air-cooled, water-cooled positive displacement and absorption chillers are at standard rating conditions defined in the reference test procedure.
b. Both the full-load and IPLV requirements shall be met or exceeded to comply with this standard. Where there is a Path B, compliance can be with either Path. A or Path B for any application.
c. NA means the requirements are not applicable for Path B and only Path A can be used for compliance.
d. FL represents the full-load performance requirements and IPLV the part-load performance requirements.

2018 IECC Baseline Efficiency Values by Chiller Type and Capacity

TABLE C403.3.2(7)
WATER CHILLING PACKAGES — EFFICIENCY REQUIREMENT St. b. d

EQUIPMENT TYPE	SIZE CATEGORY	UNITS	BEFORE	1/1/2015	AS OF	1/1/2015	TEST	
EQUIPMENT TIPE	SIZE CATEGORY	UNITS	Path A	Path B	Path A	Path B	PROCEDURE®	
	< 150 Tons		≥ 9.562 FL	NAc	≥ 10.100 FL	≥ 9.700 FL		
Air-cooled chillers	< 150 Ions	EER	≥ 12.500 IPLV	NA-	≥ 13.700 IPLV	≥ 15,800 IPLV		
Air-cooled chillers	≥ 150 Tons	(Btu/W)	≥ 9.562 FL	NAc	≥ 10.100 FL	≥ 9.700 FL		
	2 100 Ions		≥ 12.500 IPLV	NA-	≥ 14.000 IPLV	≥ 16.100 IPLV		
Air cooled without condenser, electrically operated	All capacities	EER (Btu/W)		ndensers and co	condenser shall b complying with air- equirements.			
	< 75 Tons		≤ 0.780 FL	≤ 0.800 FL	≤ 0.750 FL	≤ 0.780 FL		
	< /5 IONS		≤ 0.630 IPLV	≤ 0.600 IPLV	≤ 0.600 IPLV	≤ 0.500 IPLV		
	> 75 tons and < 150 tons	1	≤ 0.775 FL	≤ 0.790 FL	≤ 0.720 FL	≤ 0.750 FL		
	2 /o tons and < 150 tons		≤ 0.615 IPLV	≤ 0.586 IPLV	≤ 0.560 IPLV	≤ 0.490 IPLV		
Water cooled, electrically	> 150 tons and < 300 tons	kW/ton	≥ 0.680 FL	≥ 0.718 FL	≥ 0.660 FL	≥ 0.680 FL		
operated positive displacement	2 150 tons and < 300 tons	KVV/ton	≥ 0.580 IPLV	≥ 0.540 IPLV	≥ 0.540 IPLV	≥ 0.440 IPLV	AHRI 550/590	
and placement	5 000 t d d 000 t	1	≤ 0.620 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.625 FL		
	≥ 300 tons and < 600 tons	_	≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.520 IPLV	≤ 0.410 IPLV		
	≥ 600 tons		≤ 0.620 FL	≤ 0.639 FL	≤ 0.560 FL	≤ 0.585 FL		
			≤ 0.540 IPLV	≤ 0.490 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV		
	< 150 Tons		≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.695 FL		
			≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.440 IPLV		
		1	≤ 0.634 FL	≤ 0.639 FL	≤ 0.610 FL	≤ 0.635 FL		
	≥ 150 tons and < 300 tons		≤ 0.596 IPLV	≤ 0.450 IPLV	≤ 0.550 IPLV	≤ 0.400 IPLV		
Water cooled, electrically	5 000 to of 400 to	kW/ton	≤ 0.578 FL	≤ 0.600 FL	≤ 0.560 FL	≤ 0.595 FL		
operated centrifugal	≥ 300 tons and < 400 tons	≥ 300 tons and < 400 tons	KVV/ton	≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.520 IPLV	≤ 0.390 IPLV	
	≥ 400 tons and < 600 tons	1	≤ 0.578 FL	≤ 0.600 FL	≤ 0.560 FL	≤ 0.585 FL		
	≥ 400 tons and < 000 tons		≤ 0.549 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV		
	> 600 Tons	1	≤ 0.570 FL	≤ 0.590 FL	≤ 0.560 FL	≤ 0.585 FL		
	2 000 Ions		≤ 0.539 IPLV	≤ 0.400 IPLV	≤ 0.500 IPLV	≤ 0.380 IPLV		
Air cooled, absorption, single effect	All capacities	COP	≥ 0.600 FL	NAª	≥ 0.600 FL	NAª		
Water cooled absorption, single effect	All capacities	COP	≥ 0.700 FL	NA°	≥ 0.700 FL	NAª		
Absorption, double effect, indirect fired	All capacities	COP	≥ 1.000 FL ≥ 1.050 IPLV	NAº	≥ 1.000 FL ≥ 1.050 IPLV	NA°	AHRI 560	
Absorption double effect direct fired	All capacities	COP	≥ 1.000 FL ≥ 1.000 IPLV	NA°	≥ 1.000 FL ≥ 1.050 IPLV	NA°		

a. The requirements for centrifugal civiler shall be adjusted for nonstandard rating conditions in accordance with Section C403.3.2.1 and are only applicable for the range of conditions listed in Section C403.3.2.1. The requirements for air-cooled, water-cooled positive displacement and absorption chillers are at standard rating conditions defined in the reference test procedure.

b. Both the full-load and IPLV requirements shall be made or exceeded to comply with this standard. Where there is a Path B, compliance can be with either Path A or Path B for any application.

c. NA means the requirements are not applicable for Path B and only Path C and be used for compliance.

d. FL represents the full-load performance requirements and IPLV the part-load performance requirements.

MEASURE CODE:

2.6 Lighting

C&I Lighting Deemed Hours and Waste Heat Factors by Building Type

Building Type	Fixture Annual Operating Hours ¹⁸⁸ (Hours)	Waste Heat Cooling Energy Factor ¹⁸⁹ (WHFe)	Waste Heat Electric Resistance Heating ¹⁹⁰ (IFkWh)	Waste Heat Electric Heat Pump Heating (IFkWh)	Waste Heat Gas Heating ¹⁹¹ (IFTherms)
Large Office	3170	1.06	0.32	0.14	0.014
Medium Office	3170	1.14	0.19	0.08	0.008
Small Office	2884	1.11	0.21	0.09	0.009
Warehouse	2827	1.04	0.26	0.11	0.011
Stand-alone Retail	3421	1.08	0.21	0.09	0.009
Strip Mall	3694	1.08	0.22	0.10	0.009
Primary School	3466	1.08	0.28	0.12	0.012
Secondary School	3466	1.14	0.30	0.13	0.013
Supermarket	3765	1.07	0.26	0.11	0.011
Quick Service Restaurant	6443	1.12	0.27	0.12	0.012
Full Service Restaurant	6443	1.11	0.22	0.10	0.009
Hospital	3812	1.11	0.34	0.15	0.015
Outpatient Health Care	3898	1.21	0.28	0.12	0.012
Small Hotel - Building	3713	1.21	0.22	0.09	0.009
Large Hotel - Building	3713	1.24	0.01	0.00	0.000
Midrise Apartment - Building	2876	1.14	0.44	0.19	0.019
C&I Average	3351	1.09	0.24	0.10	0.010

¹⁸⁸ Fixtures hours-of-use are based upon schedule assumptions used in the computer models. Nonresidential Average is a weighted average of indoor spaces using the relative area of each Building Type in the region (CBECS). These values are references in cases where the project-specific hours are unknown.

¹⁸⁹ The Waste Heat Factor for Energy is developed using computer models for the various Building Types. Exterior and garage values are 1, unknown is a weighted average of the other Building Types.

¹⁹⁰ Electric heat penalty assumptions are based on converting the IFTherm multiplier value into kWh and then applying relative heating system efficiencies. The gas efficiency was assumed to be 80% AFUE, electric resistance is assumed to be 100%, Heat Pump is assumed to be 2.3 COP.

¹⁹¹ IFTherms value is developed using computer models consistent with methodology for Waste Heat Factor for Energy.

C&I Lighting Effective Useful Life (EUL) by Equipment Category

Measure Category	Lighting Type [1]	Effective Useful Life (EUL) [2]
	Fixture	15
	Type A & Hybrid	10
2.6.3 LED Bulbs and Fixtures	Type B	15
2.6.4 LED Screw Based Omnidirectional Bulb	Type C	11
2.6.7 LED Specialty Lamp	Retrofit Kit	15
	HID Replacement	15
	Lamp Replacement	10
2.6.6 LED Exit Sign	Exit Signs	7
2.6.8 Lighting Power Density	Lighting Power Density	15

Notes:

^[1] Ameren Missouri maintains a table that "maps" each lighting measure code to the appropriate Lighting Type.

^[2] These effective useful lives were researched by Opinion Dynamics as part of the PY19/PY20 Ameren Missouri Evaluation efforts. EUL values for each measure group were developed through a benchmarking review of TRMs and analysis of equipment specifications (e.g., lamp life) and annual operating hours from PY19/PY20 project tracking data. See Memorandum: Recommended EUL Values for Ameren Missouri Business Lighting Measures, January 6, 2021.

2.6.1 Fluorescent Delamping

DESCRIPTION

This measure entails the permanent removal of an existing 4-foot or 8-foot T8 lamp and the associated lamp holders and ballasts from the fixture. Customers are responsible for determining whether or not to use reflectors in combination with lamp removal in order to maintain adequate lighting levels. Lighting levels are expected to meet the Illuminating Engineering Society of North America (IESNA) recommended light levels. Unused lamps, lamp holders, and ballasts must be permanently removed from the fixture and disposed of in accordance with local regulations.

This measure was developed to be applicable to RF.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient condition will vary depending on the existing fixture and number of lamps removed, however for the purposes of this measure, savings are defined on a per removed lamp basis. The retrofit wattage (efficient condition) is therefore assumed to be zero.

DEFINITION OF BASELINE EQUIPMENT

The baseline condition is a T8 lamp with default wattages provided below.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The measure life is assumed to be 11 years. 192

DEEMED MEASURE COST

Actual incremental costs should be used if available. For default values, see table below.

Measure	Cost
8-Foot Lamp Removal	\$16.00
4-Foot Lamp Removal	\$12.00
8-Foot Lamp Removal with reflector	\$30.00
4-Foot Lame Removal with reflector	\$25.00

LOADSHAPE

Lighting BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS193

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000}*Hours*ISR*WHF_e$$

¹⁹² KCP&L measure life assumption.

¹⁹³ The savings numbers are for the straight lamp removal measures, as well as the lamp removal and install reflector measures.

Where:

Watts_{Base} = Wattage reduction of lamp removed. Custom input; otherwise, use

values in the table below.

Wattsee = 0

Hours = Average annual lighting hours of use as provided by the customer.

If unknown, the default value based on Building Type may be selected from the Lighting Reference Table in Section 2.6.

WHF_e = Waste heat factor for energy to account for cooling energy savings

from light removal is selected from the Lighting Reference Table in Section 2.6 for each Building Type. If building is un-cooled, the

value is 1.0 and if unknown use C&I Average value.

ISR = In Service Rate, 100% since permanent removal is assumed.

T8 Lamp Size	Wattage ¹⁹⁴
8-ft T8	38.6
4-ft T8	19.4

Heating Penalty

If electrically heated building:195

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta k = \Delta kWh * CF$

Where:

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635

NATURAL GAS ENERGY SAVINGS

¹⁹⁴ Default wattage reduction is based on averaging the savings from moving from a 2 to 1, 3 to 2 and 4 to 3 lamp fixture, as provided in the Standard Performance Contract Procedures Manual: Appendix B: Table of Standard Fixture Wattages (http://www.sce.com/NR/rdonlyres/7A3455F0-A337-439B-9607-10A016D32D4B/0/spc_B_Std_Fixture_Watts.pdf). An adjustment is made to the T8 delamped fixture to account for the significant increase in ballast factor that can be expected when delamping fixtures with parallel ballasts. See "Delamping calculation.xlsx" for details.
¹⁹⁵ Negative value because this is an increase in heating consumption due to the efficient lighting.

Heating Penalty if fossil fuel heated building (or if heating fuel is unknown):196

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

IF_{Thern}

= Lighting-HVAC Interaction Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

Other factors as defined above.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

¹⁹⁶ Negative value because this is an increase in heating consumption due to the efficient lighting.

2.6.2 High Performance and Reduced Wattage T8 Fixtures and Lamps

DESCRIPTION

This measure applies to High Performance T8 (HPT8) lamp/ballast systems that have higher lumens per watt than standard T8 systems. This measure applies to the installation of new equipment with efficiencies that exceed that of the equipment that would have been installed following standard market practices and is applicable to time of sale as well as retrofit measures. Retrofit measures may include new fixtures or relamp/reballast measures. In addition, options have been provided to allow for the "Reduced Wattage T8 lamps" or RWT8 lamps that result in relamping opportunities that produce equal or greater light levels than standard T8 lamps while using fewer watts.

This measure was developed to be applicable to the following program types: TOS, RF, and DI. If applied to other program types, the measure savings should be verified.

The measure applies to all commercial HPT8 installations excluding new construction and major renovation or change of use measures (see lighting power density measure). Lookup tables have been provided to account for the different types of installations. Whenever possible, actual costs and hours of use should be utilized for savings calculations. Default new and baseline assumptions have been provided in the reference tables. Default component costs and lifetimes have been provided for O&M calculations. Please see the Definition Table to determine applicability for each program. HPT8 configurations not included in the TRM may be included in custom program design using the provided algorithms as long as energy savings is achieved.

The following table defines the applicability for different programs:

Time of Sale (TOS)

This measure relates to the installation of new equipment with efficiency that exceeds that of equipment that would have been installed following standard market practices. In general, the measure will include qualifying highefficiency, low ballast-factor ballasts paired with high-efficiency, long- life lamps as detailed in the attached tables. High-bay applications use this system paired with qualifying high ballast factor ballasts and high performance 32 w lamps. Custom lighting designs can use qualifying low, normal or high ballast-factor ballasts and qualifying lamps in lumen equivalent applications where total system wattage is reduced when calculated using the calculation of savings algorithms.

Retrofit (RF) and Direct Install (DI)

This measure relates to the replacement of existing equipment with new equipment with efficiency that exceeds that of the existing equipment. In general, the retrofit will include qualifying high efficiency lowballast factor ballasts paired with high efficiency long life lamps as detailed in the attached tables. Custom lighting designs can use qualifying low, normal or high-ballast factor ballasts and qualifying lamps in lumen equivalent applications where total system wattage is reduced when calculated using the calculation of savings algorithms.

High-efficiency troffers (new/or retrofit) utilizing HPT8 technology can provide even greater savings. When used in a high-bay application, high performance T8 fixtures can provide equal light to HID high-bay fixtures, while using fewer watts; these systems typically utilize high ballast-factor ballasts, but qualifying low and normal ballast factor ballasts may be used when appropriate light levels are provided and overall wattage is reduced.

DEFINITION OF EFFICIENT EQUIPMENT

This characterization assumes the efficient condition for all applications are qualifying HP or RWT8 fixture and lamp/ballast combinations listed on the CEE website under qualifying HP T8 products¹⁹⁷ and qualifying RWT8 products.¹⁹⁸

The definition of efficient equipment varies based on the program and is defined below:

Time of Sale (TOS)	Retrofit (RF) and Direct Install (DI)
High-efficiency troffers combined with high	High-efficiency troffers (new or retrofit kits)
efficiency lamps and ballasts allow for fewer	combined with high efficiency lamps and ballasts
lamps to be used to provide a given lumen output.	allow for fewer lamps to be used to provide a given
High-efficiency troffers must have a fixture	lumen output. High efficiency troffers must have a
efficiency of 80% or greater to qualify.	fixture efficiency of 80% or greater to qualify.
High bay fixtures must have fixture efficiencies	High bay fixtures will have fixture efficiencies of
of 85% or greater.	85% or greater.

DEFINITION OF BASELINE EQUIPMENT

The definition of baseline equipment varies based on the program and is defined below:

Time of Sale (TOS)	Retrofit (RF) and Direct Install (DI)
The baseline is standard efficiency T8	The baseline is the existing system.
systems that would have been installed. The baseline for high-bay fixtures is pulse start metal halide fixtures.	In July 14, 2012, federal standards were enacted that were expected to eliminate T12s as an option for linear fluorescent fixtures. However, due to significant loopholes in the legislation, T12 compliant product is still freely available.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The deemed lifetime of efficient equipment varies based on the program and is defined below:

Time of Sale (TOS)	Retrofit (RF) and Direct Install
	(DI)
Fixture lifetime is 15 years. ¹⁹⁹	Fixture lifetime is 15 years.
Fixture retrofits which utilize RWT8 lamps have a lifetime	Note, since the fixture lifetime is
equivalent to the life of the lamp, capped at 15 years. There is	deemed at 15 years, the replacement
no guarantee that a reduced wattage lamp will be installed at	cost of both the lamp and ballast
time of burnout, but if one is, savings will be captured in the	should be incorporated into the O&M
RWT8 measure below.	calculation.
RWT8 lifetime is the life of the product, at the reported	
operating hours (lamp life in hours divided by operating hours	

http://library.ccel.org/content/cce-high-performance-t8-specification
 http://library.ccel.org/content/reduced-wattage-t8-specification
 159 15 years from GDS Measure Life Report, June 2007.

per year – see reference table "RWT8 Component Costs and	
Lifetime"), capped at 15 years. ²⁰⁰	

DEEMED MEASURE COST

Actual incremental costs should be used if available. For default values, see the reference table at the end of this characterization.

LOADSHAPE

Lighting BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = (Watts_{BASE} - Watts_{EE}) * Hour * WHF_e * ISR$

Where:

Watts_{BASE} = Input wattage of the existing system which depends on the baseline

fixture configuration (number and type of lamp) and number of fixtures. Value can be selected from the appropriate reference table as shown below, or a custom value can be entered if the configurations in the

tables is not representative of the existing system.

Watts_{EE} = New Input wattage of EE fixture which depends on new fixture

configuration (number of lamps) and ballast factor and number of fixtures. Value can be selected from the appropriate reference table, or a custom value can be entered if the configurations in the tables is not

representative of the existing system.

Hours = Average hours of use per year as provided by the customer or selected

from the Reference Table in Section 2.8. If hours or Building Type are

unknown, use the C&I Average value.

WHF_e = Waste heat factor for energy to account for cooling energy savings

from efficient lighting is selected from the Reference Table in Section 2.8 for each Building Type. If building is un-cooled, the value is 1.0.

ISR = In Service Rate is assumed to be 100%

Program	Reference Table
Time of Sale	A-1: HPT8 and RWT8 New and Baseline Assumptions
Retrofit	A-2: HPT8 and RWT8 New and Baseline Assumptions
High-Bay T8 Time of Sale and Retrofit	A-3: High Bay T8 New and Baseline Assumptions

²⁰⁰ 15 years from GDS Measure Life Report, June 2007.

Heating Penalty

If electrically heated building:201

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Reference Table in Section 2.8. If unknown, use the C&I Average value.

SUMMER COINCIDENT DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635

NATURAL GAS SAVINGS

Heating Penalty if fossil fuel heated building (or if heating fuel is unknown): 201192

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

 $IF_{Therms} \\$

= Lighting-HVAC Interaction Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 2.8 for each Building Type.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

Actual operation and maintenance costs will vary by specific equipment installed/replaced. See Reference Tables for O&M values:

²⁰¹ Negative value because this is an increase in heating consumption due to the efficient lighting.

Program	Reference Table
TOS	B-1: HPT8 and RWT8 New and Baseline Assumptions
RF	B-2: HPT8 and RWT8 New and Baseline Assumptions
High-Bay T8 Time of Sale and Retrofit	B-3: High Bay T8 New and Baseline Assumptions

REFERENCE TABLES

A-1: Time of Sale: HPT8 and RWT8 New and Baseline Assumptions²⁰²

EE Measure Description	Watts _{EE}	Baseline Description	Watts _{BASE}	Incremental Cost
1-Lamp 32w HPT8 (BF < 0.79)	24.0	Standard T8	29.1	\$15.00
2-Lamp 32w HPT8 (BF < 0.77)	48.0	Standard T8	57.0	\$17.50
3-Lamp 32w HPT8 (BF < 0.76)	71.0	Standard T8	84.5	\$20.00
4-Lamp 32w HPT8 (BF < 0.78)	98.0	Standard T8	112.6	\$22.50
6-Lamp 32w HPT8 (BF < 0.76)	142.0	Standard T8	169.0	\$40.00
1-Lamp 28w RWT8 (BF < 0.76)	21.3	Standard T8	29.1	\$15.00
2-Lamp 28w RWT8 (BF < 0.76)	42.6	Standard T8	57.0	\$17.50
3-Lamp 28w RWT8 (BF < 0.77)	63.0	Standard T8	84.5	\$20.00
4-Lamp 28w RWT8 (BF < 0.79)	88.5	Standard T8	112.6	\$22.50
6-Lamp 28w RWT8 (BF < 0.77)	126.0	Standard T8	169.0	\$40.00

A-2: Retrofit: HPT8 and RWT8 New and Baseline Assumptions

EE Measure Description	Watts _{EE}	Baseline Description	Watts _{BASE}	Full Cost	Mid Life Savings Adjustment (2020)
1-Lamp Relamp/Reballast T12 to HPT8	24.0	1-Lamp 40w T12	31.0	\$50.00	N/A
2-Lamp Relamp/Reballast T12 to HPT8	48.0	2-Lamp 40w T12	62.0	\$55.00	N/A
3-Lamp Relamp/Reballast T12 to HPT8	71.0	3-Lamp 40w T12	108.0	\$60.00	N/A
4-Lamp Relamp/Reballast T12 to HPT8	98.0	4-Lamp 40w T12	144.0	\$65.00	N/A
6-Lamp Relamp/Reballast T12 to HPT8	142.0	6-Lamp 40w T12	216.0	\$75.00	N/A
1-Lamp Relamp/Reballast T12 to RWT8	21.3	1-Lamp 40w T12	31.0	\$50.00	N/A
2-Lamp Relamp/Reballast T12 to RWT8	42.6	2-Lamp 40w T12	62.0	\$55.00	N/A
3-Lamp Relamp/Reballast T12 to RWT8	63.0	3-Lamp 40w T12	108.0	\$60.00	N/A
4-Lamp Relamp/Reballast T12 to RWT8	88.5	4-Lamp 40w T12	144.0	\$65.00	N/A
6-Lamp Relamp/Reballast T12 to RWT8	126.0	6-Lamp 40w T12	216.0	\$75.00	N/A
1-Lamp Relamp/Reballast T8 to HPT8	24.0	1-Lamp 32w T8	29.1	\$50.00	N/A

²⁰² Watt, lumen, lamp life, and ballast factor assumptions for efficient measures are based upon Consortium for Energy Efficiency (CEE) Commercial Lighting Qualifying Product Lists. Watt, lumen, lamp life, and ballast factor assumptions for baseline fixtures are based upon manufacturer specification sheets. Baseline and efficient measure cost data comes from lighting suppliers, past Efficiency Vermont projects, and professional judgment. See "HPT8 TRM Reference Tables.xlsx" for more information and specific product links. Currently, 25WT8 are not considered under this measure as their lower light trade off and limitations on temperature and dimming have caused most distributers/contractors to use 28W almost exclusively in other markets.

2-Lamp Relamp/Reballast T8 to HPT8	48.0	2-Lamp 32w T8	57.0	\$55.00	N/A
3-Lamp Relamp/Reballast T8 to HPT8	71.0	3-Lamp 32w T8	84.5	\$60.00	N/A
4-Lamp Relamp/Reballast T8 to HPT8	98.0	4-Lamp 32w T8	112.6	\$65.00	N/A
6-Lamp Relamp/Reballast T8 to HPT8	142.0	6-Lamp 32w T8	169.0	\$75.00	N/A
1-Lamp Relamp/Reballast T8 to RWT8	21.3	1-Lamp 32w T8	29.1	\$50.00	N/A
2-Lamp Relamp/Reballast T8 to RWT8	42.6	2-Lamp 32w T8	57.0	\$55.00	N/A
3-Lamp Relamp/Reballast T8 to RWT8	63.0	3-Lamp 32w T8	84.5	\$60.00	N/A
4-Lamp Relamp/Reballast T8 to RWT8	88.5	4-Lamp 32w T8	112.6	\$65.00	N/A
6-Lamp Relamp/Reballast T8 to RWT8	126.0	6-Lamp 32w T8	169.0	\$75.00	N/A

^{*} New T12s that meeting EISA efficacy standards changed from 34w to 40w to meet the lumen/per watt requirement.

A-3: Time of Sale/Retrofit: High Bay T8 New and Baseline Assumptions

EE Measure Description	Wattsee	Baseline Description	Watts _{BASE}	Incremental Cost	Full Cost
4-Lamp HPT8 w/ High- BF Ballast High-Bay	218.5	200 Watt Pulse Start Metal-Halide	232.0	\$75	\$200
4-Lamp HPT8 w/ High-BF Ballast High-Bay	218.5	250 Watt Metal Halide	295.0	\$75	\$200
6-Lamp HPT8 w/ High- BF Ballast High-Bay	330.1	320 Watt Pulse Start Metal-Halide	348.8	\$75	\$225
6-Lamp HPT8 w/ High- BF Ballast High-Bay	330.1	400 Watt Pulse Start Metal Halide	455.0	\$75	\$225
8-Lamp HPT8 w/ High- BF Ballast High-Bay	418.6	Proportionally Adjusted according to 6-Lamp HPT8 Equivalent to 320 PSMH	476.0	\$75	\$250
8-Lamp HPT8 w/ High- BF Ballast High-Bay	418.6	Proportionally Adjusted according to 6-Lamp HPT8 Equivalent to 400 W Metal Halide	618.0	\$75	\$250

B-1: Time of Sale: HPT8 and RWT8 Component Costs and Lifetime

			EE N	1easure		Baseline			
EE Measure Description	Lamp Quantity	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost
1-Lamp 32w HPT8 (BF < 0.79)	1	24,000	\$8.17	70,000	\$52.50	20,000	\$5.67	70,000	\$35.00
2-Lamp 32w HPT8 (BF < 0.77)	2	24,000	\$16.34	70,000	\$52.50	20,000	\$11.34	70,000	\$35.00
3-Lamp 32w HPT8 (BF < 0.76)	3	24,000	\$24.51	70,000	\$52.50	20,000	\$17.01	70,000	\$35.00
4-Lamp 32w HPT8 (BF < 0.78)	4	24,000	\$32.68	70,000	\$52.50	20,000	\$22.68	70,000	\$35.00
6-Lamp 32w HPT8 (BF < 0.76)	6	24,000	\$49.02	70,000	\$105.00	20,000	\$34.02	70,000	\$35.00
1-Lamp 28w RWT8 (BF < 0.76)	1	18,000	\$8.17	70,000	\$52.50	20,000	\$5.67	70,000	\$35.00
2-Lamp 28w RWT8 (BF < 0.76)	2	18,000	\$16.34	70,000	\$52.50	20,000	\$11.34	70,000	\$35.00
3-Lamp 28w RWT8 (BF < 0.77)	3	18,000	\$24.51	70,000	\$52.50	20,000	\$17.01	70,000	\$35.00
4-Lamp 28w RWT8 (BF < 0.79)	4	18,000	\$32.68	70,000	\$52.50	20,000	\$22.68	70,000	\$35.00
6-Lamp 28w RWT8 (BF < 0.77)	6	18,000	\$49.02	70,000	\$105.00	20,000	\$34.02	70,000	\$35.00

B-2: Retrofit: HPT8 and RWT8 Component Costs and Lifetime

			EE Me	asure		Baseline			
EE Measure Description	Lamp Quantity	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost
1-Lamp Relamp/Reballast T12 to HPT8	1	24,000	\$8.17	70,000	\$52.50	20,000	\$5.87	40,000	\$35.00
2-Lamp Relamp/Reballast T12 to HPT8	2	24,000	\$16.34	70,000	\$52.50	20,000	\$11.74	40,000	\$35.00
3-Lamp Relamp/Reballast T12 to HPT8	3	24,000	\$24.51	70,000	\$52.50	20,000	\$17.61	40,000	\$35.00
4-Lamp Relamp/Reballast T12 to HPT8	4	24,000	\$32.68	70,000	\$52.50	20,000	\$23.48	40,000	\$35.00
6-Lamp Relamp/Reballast T12 to HPT8	6	24,000	\$49.02	70,000	\$105.00	20,000	\$35.22	40,000	\$35.00
1-Lamp Relamp/Reballast T12 to RWT8	1	18,000	\$8.17	70,000	\$52.50	20,000	\$5.87	40,000	\$35.00
2-Lamp Relamp/Reballast T12 to RWT8	2	18,000	\$16.34	70,000	\$52.50	20,000	\$11.74	40,000	\$35.00
3-Lamp Relamp/Reballast T12 to RWT8	3	18,000	\$24.51	70,000	\$52.50	20,000	\$17.61	40,000	\$35.00
4-Lamp Relamp/Reballast T12 to RWT8	4	18,000	\$32.68	70,000	\$52.50	20,000	\$23.48	40,000	\$35.00
6-Lamp Relamp/Reballast T12 to RWT8	6	18,000	\$49.02	70,000	\$105.00	20,000	\$35.22	40,000	\$35.00
1-Lamp Relamp/Reballast T8 to HPT8	1	24,000	\$8.17	70,000	\$52.50	20,000	\$5.67	70,000	\$35.00

Ameren Missouri

		EE Measure				Baseline			
EE Measure Description	Lamp Ouantity	Lamp Life	Total Lamp Replacement	Ballast Life	Total Ballast Replacement	Lamp Life	Total Lamp Replacement	Ballast Life	Total Ballast Replacement
	Quantity	(hrs)	Cost	(hrs)	Cost	(hrs)	Cost	(hrs)	Cost
2-Lamp Relamp/Reballast T8 to HPT8	2	24,000	\$16.34	70,000	\$52.50	20,000	\$11.34	70,000	\$35.00
3-Lamp Relamp/Reballast T8 to HPT8	3	24,000	\$24.51	70,000	\$52.50	20,000	\$17.01	70,000	\$35.00
4-Lamp Relamp/Reballast T8 to HPT8	4	24,000	\$32.68	70,000	\$52.50	20,000	\$22.68	70,000	\$35.00
6-Lamp Relamp/Reballast T8 to HPT8	6	24,000	\$49.02	70,000	\$105.00	20,000	\$34.02	70,000	\$35.00
1-Lamp Relamp/Reballast T8 to RWT8	1	18,000	\$8.17	70,000	\$52.50	20,000	\$5.67	70,000	\$35.00
2-Lamp Relamp/Reballast T8 to RWT8	2	18,000	\$16.34	70,000	\$52.50	20,000	\$11.34	70,000	\$35.00
3-Lamp Relamp/Reballast T8 to RWT8	3	18,000	\$24.51	70,000	\$52.50	20,000	\$17.01	70,000	\$35.00
4-Lamp Relamp/Reballast T8 to RWT8	4	18,000	\$32.68	70,000	\$52.50	20,000	\$22.68	70,000	\$35.00
6-Lamp Relamp/Reballast T8 to RWT8	6	18,000	\$49.02	70,000	\$105.00	20,000	\$34.02	70,000	\$35.00

B-3: High Bay HPT8 Component Costs and Lifetime

	I	EE Measure				Baseline				
EE Measure Description	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost	Baseline Description	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost	
4-Lamp HPT8 w/ High-BF Ballast High-Bay	24000	\$46.68	70000	\$47.50	200 Watt Pulse Start Metal-Halide 250 Watt Metal Halide	12000 10000	\$35.67 \$27.67	40000 40000	\$110.25 \$114.50	
6-Lamp HPT8 w/ High-BF Ballast High-Bay	24000	\$70.02	70000	\$47.50	320 Watt Pulse Start Metal-Halide 400 Watt Metal-Halide	20000	\$78.67 \$23.67	40000	\$131.85 \$136.50	
8-Lamp HPT8 w/ High-BF Ballast High-Bay	24000	\$93.36	70000	\$47.50	Proportionally Adjusted according to 6-Lamp HPT8 Equivalent to 320 PSMH	20000	\$23.67	40000	\$131.85	

MEASURE CODE:

2.6.3 LED Bulbs and Fixtures

DESCRIPTION

The installation of Light-Emitting Diode (LED) lighting systems have comparable luminosity to incandescent bulbs and equivalent fluorescent lamps at significantly less wattage, lower heat, and with significantly longer lifetimes.

This measure provides savings assumptions for a variety of efficient lighting fixtures including internal and external LED fixtures, recess (troffer), canopy, and pole fixtures as well as refrigerator and display case lighting.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, all LED fixtures are assumed to be ENERGY STAR® labeled or on the Design Light Consortium qualifying fixture list.²⁰³

LED Fixtures and Retrofit Kits with Network Controls achieve additional savings similar to the savings described in the Occupancy Controls section.

DEFINITION OF BASELINE EQUIPMENT

For TOS and RF installations, the baselines efficiency case is project specific and is determined using actual fixture types and counts from the existing space. The existing fluorescent fixture end connectors and ballasts must be completely removed to qualify.

Where the installation technology is not known, the assumed baselines condition for an outdoor pole/arm, wall-mounted, garage/canopy fixture and high-bay luminaire with a high intensity discharge light source is a metal halide fixture. Deemed fixture wattages are provided in reference tables at the end of this characterization.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

See Lighting EUL Reference Table for EUL values by Lighting Measure Group.

DEEMED MEASURE COST

Actual incremental costs should be used if available. For default values, refer to the reference tables below.

LOADSHAPE

Lighting BUS Ext Lighting BUS Miscellaneous BUS

 $^{^{203}\} Design\ Lights\ Consortium\ Qualified\ Products\ List\ http://www.designlights.org/qpl.$

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000}*Hours*WHF_e*ISR$$

Where:

WattsBase = Actual wattage of the existing or baseline system. Reference the

"LED New and Baseline Assumptions" table for default values.

Watts_{EE} = Actual wattage of LED fixture purchased / installed. If unknown,

use default provided in "LED New and Baseline Assumptions."

Hours = Average annual lighting hours of use as provided by the customer

or selected from the Lighting Reference Table in Section 2.6 by Building Type. If hours or Building Type are unknown, use the C&I

Average value.

WHFe = Waste heat factor for energy to account for cooling energy savings

from efficient lighting is selected from the Lighting Reference Table in Section 2.6 for each Building Type. If building is un-cooled, the

value is 1.0.

ISR = In Service Rate represents the percentage of reported lamps or

fixtures that is installed and operating and varies with the program delivery approach. Use 100% for programs with direct installation and/or installation verification procedures (e.g., verification inspections for a sample of projects), use 98.7% for program delivery

inspections for a sample of projects); use 98.7% for program delivery without installation verification.²⁰⁴ The ISR may also be set to 100% if the installation verification is embedded in other evaluation

adjustments.

Note that LED Fixtures and Retrofit Kits with Network Controls achieve additional savings similar to the savings described in the Occupancy Controls section.

Heating Penalty:

If electrically heated building:205

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

²⁰⁴ ISR is based on results presented in Ameren Missouri Lighting Impact and Process Evaluation: Program Year 2015 and consistent with other program ISR in neighboring states (Illinois and Iowa). These evaluation results are from a retail-based lighting program with multiple delivery channels including point-of-sale markdown, online website, coupons, and social marketing distribution.

²⁰⁵ Negative value because this is an increase in heating consumption due to the efficient lighting.

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWh * CF$$

Where:

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635 for indoor lighting

= 0.0000056160 for exterior lighting

= 0.0001379439 for <u>exterior</u> 24/7 lighting

NATURAL GAS ENERGY SAVINGS

Heating penalty if fossil fuel heated building (or if heating fuel is unknown):

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

IF_{Therms} = Lighting-HVAC Interaction Factor for gas heating impacts.²⁰⁶ This factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

See Reference Tables below for default assumptions.

²⁰⁶ Negative value because this is an increase in heating consumption due to the efficient lighting.

Ameren Missouri REFERENCE TABLES ²⁰⁷

Appendix H - TRM - Vol. 2: C&I Measures

LED New and Baseline Assumptions:

LED Catagony	EE Measure	Baseline	Incremental		
LED Category	Description	Wattsee	Description	Wattsbase	Cost
LED Downlight Fixtures	LED Recessed, Surface, Pendant Downlights	17.6	40% CFL 26W Pin Based & 60% PAR30/38	54.3	\$27
LED Interior	LED Track Lighting	12.2	10% CMH PAR38 & 90% Halogen PAR38	60.4	\$59
Directional LED Wall-Wash Fixtures 8.3 40%		40% CFL 42W Pin Base & 60% Halogen PAR38	17.7	\$59	
	LED Display Case Light Fixture	7.1 / ft	50% 2'T5 Linear & 50% 50W Halogen	36.2 / ft	\$11/ft
LED Dissilate Cons	LED Undercabinet Shelf-Mounted Task Light Fixtures	7.1 / ft	50% 2'T5 Linear & 50% 50W Halogen	36.2 / ft	\$11/ft
LED Display Case	LED Refrigerated Case Light, Horizontal or Vertical	7.6 / ft	5'T8	15.2 / ft	\$11/ft
	LED Freezer Case Light, Horizontal or Vertical	7.7 / ft	6'T12HO	18.7 / ft	\$11/ft
LED Linear	LED 4' Linear Replacement Lamp	18.7	Lamp Only 32w T8	32.0	\$24
Replacement Lamps	LED 2' Linear Replacement Lamp	9.7	Lamp Only 17w T8	17.0	\$13
	LED 2x2 Recessed Light Fixture, 2000-3500 lumens	34.1	2-Lamp 32w T8 (BF < 0.89)	57.0	\$48
	LED 2x2 Recessed Light Fixture, 3501-5000 lumens	42.8	3-Lamp 32w T8 (BF < 0.88)	84.5	\$91
	LED 2x4 Recessed Light Fixture, 3000-4500 lumens	37.9	2-Lamp 32w T8 (BF < 0.89)	57.0	\$62
LED Troffers	LED 2x4 Recessed Light Fixture, 4501-6000 lumens	54.3	3-Lamp 32w T8 (BF < 0.88)	84.5	\$99
LED Irollers	LED 2x4 Recessed Light Fixture, 6001-7500 lumens	72.7	4-Lamp 32w T8 (BF < 0.88)	112.6	\$150
	LED 1x4 Recessed Light Fixture, 1500-3000 lumens	18.1	1-Lamp 32w T8 (BF <0.91)	29.1	\$36
	LED 1x4 Recessed Light Fixture, 3001-4500 lumens	39.6	2-Lamp 32w T8 (BF < 0.89)	57.0	\$76
	LED 1x4 Recessed Light Fixture, 4501-6000 lumens	53.1	3-Lamp 32w T8 (BF < 0.88)	84.5	\$130
	LED Surface & Suspended Linear Fixture, ≤ 3000 lumens	19.7	1-Lamp 32w T8 (BF <0.91)	29.1	\$54
LED Linear	LED Surface & Suspended Linear Fixture, 3001-4500 lumens	37.8	2-Lamp 32w T8 (BF < 0.89)	57.0	\$104
Ambient Fixtures	LED Surface & Suspended Linear Fixture, 4501-6000 lumens	55.9	3-Lamp 32w T8 (BF < 0.88)	84.5	\$158
Amoient Fixtures	LED Surface & Suspended Linear Fixture, 6001-7500 lumens	62.6	T5HO 2L-F54T5HO - 4'	120.0	\$215
	LED Surface & Suspended Linear Fixture, > 7500 lumens	95.4	T5HO 3L-F54T5HO - 4'	180.0	\$374

²⁰⁷ Watt, lumen, lamp life, and ballast factor assumptions for efficient measures are based upon Consortium for Energy Efficiency (CEE) Commercial Lighting Qualifying Product Lists alongside past Efficiency Vermont projects and PGE refrigerated case study. Watt, lumen, lamp life, and ballast factor assumptions for baseline fixtures are based upon manufacturer specification sheets. Baseline cost data comes from lighting suppliers, past Efficiency Vermont projects, and professional judgment. Efficient cost data comes from 2012 DOE "Energy Savings Potential of Solid-State Lighting in General Illumination Applications," Table A.1. See "LED Lighting Systems TRM Reference Tables.xlsx" for more information and specific product links.

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	LED Low-Bay Fixtures, ≤ 10,000 lumens	90.3	3-Lamp T8HO Low-Bay	157.0	\$191
LED High & Low	LED High-Bay Fixtures, 10,001-15,000 lumens	127.5	4-Lamp T8HO High-Bay	196.0	\$331
Bay Fixtures	LED High-Bay Fixtures, 15,001-20,000 lumens	191.0	6-Lamp T8HO High-Bay	294.0	\$482
	LED High-Bay Fixtures, > 20,000 lumens	249.7	8-Lamp T8HO High-Bay	392.0	\$818
	LED Ag Interior Fixtures, ≤ 2,000 lumens	17.0	25% 73 Watt EISA Inc, 75% 1L T8	42.0	\$33
	LED Ag Interior Fixtures, 2,001-4,000 lumens	27.8	25% 146 Watt EISA Inc, 75% 2L T8	81.0	\$54
	LED Ag Interior Fixtures, 4,001-6,000 lumens	51.2	25% 217 Watt EISA Inc, 75% 3L T8	121.0	\$125
LED Agricultural	LED Ag Interior Fixtures, 6,001-8,000 lumens	71.7	25% 292 Watt EISA Inc, 75% 4L T8	159.0	\$190
Interior Fixtures	LED Ag Interior Fixtures, 8,001-12,000 lumens	103.5	200W Pulse Start Metal Halide	227.3	\$298
	LED Ag Interior Fixtures, 12,001-16,000 lumens	143.8	320W Pulse Start Metal Halide	363.6	\$450
	LED Ag Interior Fixtures, 16,001-20,000 lumens	183.3	350W Pulse Start Metal Halide	397.7	\$595
	LED Ag Interior Fixtures, > 20,000 lumens	305.0	(2) 320W Pulse Start Metal Halide	727.3	\$998
	LED Exterior Fixtures, ≤ 5,000 lumens	42.6	100W Metal Halide	113.6	\$190
LED Exterior	LED Exterior Fixtures, 5,001-10,000 lumens	68.2	175W Pulse Start Metal Halide	198.9	\$287
Fixtures	LED Exterior Fixtures, 10,001-15,000 lumens	122.5	250W Pulse Start Metal Halide	284.1	\$391
	LED Exterior Fixtures, > 15,000 lumens	215.0	400W Pulse Start Metal Halide	454.5	\$793

LED Component Costs and Lifetimes:²⁰⁸

		EE Measure				Baseline			
LED Category	EE Measure Description	Lamp Life (hrs)	Total Lamp Replace Cost	LED Driver Life (hrs)	Total LED Driver Replace Cost	Lamp Life (hrs)	Total Lamp Replace Cost	Ballast Life (hrs)	Total Ballast Replace Cost
LED Downlight Fixtures	LED Recessed, Surface, Pendant Downlights	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Interior	LED Track Lighting	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Directional	LED Wall-Wash Fixtures	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Dissilate Cons	LED Display Case Light Fixture	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Display Case	LED Undercabinet Shelf-Mounted Task Light Fixtures	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Display Case	LED Refrigerated Case Light, Horizontal or Vertical	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Display Case	LED Freezer Case Light, Horizontal or Vertical	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00

²⁰⁸ Costs are based on actual costs, and measure lives are based on analysis of actual lamp life and hours of use.

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LED Linear	LED 4' Linear Replacement Lamp	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Replacement Lamps Replacement	LED 2' Linear Replacement Lamp	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 2x2 Recessed Light Fixture, 2000-3500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 2x2 Recessed Light Fixture, 3501-5000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 2x4 Recessed Light Fixture, 3000-4500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Troffers	LED 2x4 Recessed Light Fixture, 4501-6000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Hollers	LED 2x4 Recessed Light Fixture, 6001-7500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 1x4 Recessed Light Fixture, 1500-3000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 1x4 Recessed Light Fixture, 3001-4500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED 1x4 Recessed Light Fixture, 4501-6000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Surface & Suspended Linear Fixture, ≤ 3000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Linear	LED Surface & Suspended Linear Fixture, 3001-4500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Ambient	LED Surface & Suspended Linear Fixture, 4501-6000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Fixtures	LED Surface & Suspended Linear Fixture, 6001-7500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Surface & Suspended Linear Fixture, > 7500 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED High &	LED Low-Bay Fixtures, ≤ 10,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Led Fligh &	LED High-Bay Fixtures, 10,001-15,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Fixtures	LED High-Bay Fixtures, 15,001-20,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Tixtures	LED High-Bay Fixtures, > 20,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, ≤ 2,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, 2,001-4,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, 4,001-6,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Agricultural	LED Ag Interior Fixtures, 6,001-8,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Interior Fixtures	LED Ag Interior Fixtures, 8,001-12,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, 12,001-16,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, 16,001-20,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Ag Interior Fixtures, > 20,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Exterior Fixtures, ≤ 5,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
LED Exterior	LED Exterior Fixtures, 5,001-10,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
Fixtures	LED Exterior Fixtures, 10,001-15,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00
	LED Exterior Fixtures, > 15,000 lumens	\$62.50	15,000	\$58.00	40,000	\$102.50	\$62.50	15,000	\$58.00

MEASURE CODE:

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2.6.4 LED Screw Based Omnidirectional Bulb (Retired, effective 8/1/2023)

DESCRIPTION

LEDs lighting systems convert electricity to light and emit more lumens per watt when compared to baseline EISA incandescent, halogen, or compact fluorescent lamps.

This specific characterization provides savings assumptions for LED lamps that replace standard screw-in connections (e.g., A-Type lamp) such as interior/exterior omnidirectional bulb options.

This characterization assumes that the LED is installed in a commercial location. This is, therefore, appropriate for commercially targeted programs, or, if the implementation strategy does not allow for the installation location to be known (e.g., an upstream retail program), utilities should develop an assumption of the residential versus nonresidential split and apply the relevant assumptions to each portion.

Federal legislation stemming from the Energy Independence and Security Act of 2007 (EISA) requires all general-purpose light bulbs between 40W and 100W to be approximately 30% more energy efficient than standard incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ended in 2012, followed by restrictions on 75W in 2013 and 60W and 40W in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, new LED screw-based lamps must be ENERGY STAR® qualified based upon the ENERGY STAR® specification v2.0 which will become effective on 1/2/2017 (https://www.energystar.gov/sites/default/files/Luminaires%20V2%200%20Final.pdf).

Qualification could also be based or on the Design Light Consortium's qualified product list. 209

DEFINITION OF BASELINE EQUIPMENT

The baseline condition for this measure is assumed to be an EISA-qualified halogen or incandescent.²¹⁰ A midlife adjustment example is provided but not applied to measures installed prior to 2022.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

See Lighting EUL Reference Table for EUL values by Lighting Measure Group.

DEEMED MEASURE COST

²⁰⁹ https://www.designlights.org/QPL

²¹⁰ A provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. However, in 2019, the Department of Energy issued two final rules and clarified that a) the EISA backstop provision had not been triggered and therefore b) the efficiency standard would not change in 2020. As of 10/15/2020, the 45 lumen per watt EISA standard is not effective.

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Actual incremental costs should be used if available. If unavailable, assume \$3.26 (baseline cost of \$1.80 and efficient cost of \$5.06).211

LOADSHAPE

Lighting BUS Ext Lighting BUS Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * WHF_e * ISR$$

Where:

WattsBase = Based on lumens of LED bulb installed

Wattsee = Actual wattage of LED purchased/installed. If unknown, use

default provided below.212

Hours = Average hours of use per year as provided by the customer or

selected from the Lighting Reference Table in Section 2.6 and based

upon Building Type. If unknown, use the C&I Average value.

WHFe = Waste heat factors for energy to account for cooling energy savings

from efficient lighting are provided for each Building Type in the Lighting Reference Table in Section 2.6. If unknown, use the C&I

Average value.

ISR = In-Service Rate represents the percentage of reported lamps or

fixtures that is installed and operating and varies with the program delivery approach. Use 100% for programs with direct installation and/or installation verification procedures (e.g., verification

inspections for a sample of projects); use 98.7% for program delivery

²¹¹ Incandescent/halogen and LED cost assumptions based on Cadmus "LED Incremental Cost Study: Overall Final Report," February 2016

⁽http://ma-eeac.org/wordpress/wp-content/uploads/MA-Task-5b-LED-Incremental-Cost-Study FINAL 01FEB2016.pdf), p.19. 212 WattsEE defaults are based upon the average available ENERGY STAR® product, accessed 06/18/2015. For any lumen range where there is no ENERGY STAR® product currently available, Wattsee is based upon the ENERGY STAR® minimum luminous efficacy (55Lm/W for lamps with rated wattages less than 15W and 65 Lm/W for lamps with rated wattages \geq 15 watts) for the mid-point of the lumen range. See calculation at "cerified-light-bulbs-2015-06-18.xlsx." These assumptions should be reviewed regularly to ensure they represent the available product.

without installation verification. 213 The ISR may also be set to 100% if the installation verification is embedded in other evaluation adjustments.

Lower Lumen Range	Upper Lumen Range	Watts _{Base}	Watts _{EE} LED	Delta Watts
250	309	25	4.0	21
310	749	29	6.7	22.3
750	1,049	43	10.1	32.9
1,050	1,489	53	12.8	40.2
1,490	2,600	72	17.4	54.6
2,601	3,000	150	43.1	106.9
3,001	3,999	200	53.8	146.2
4,000	6,000	300	76.9	223.1

Mid-Life Baseline Adjustment Example

During the lifetime of a standard omnidirectional LED, the baseline incandescent/halogen bulb would need to be replaced multiple times. Since the baseline bulb changes to a CFL equivalent in 2020 due to the EISA backstop provision (except for <310 and 2600+ lumen lamps), the annual savings claim must be reduced within the life of the measure to account for this baseline shift. This reduced annual savings will need to be incorporated in to cost effectiveness screening calculations. The baseline adjustment also impacts the O&M schedule. However, in 2019, the Department of Energy issued two final rules and clarified that a) the EISA backstop provision had not been triggered and therefore b) the efficiency standard would not change in 2020. As of 10/15/2020, the 45 lumen per watt EISA standard is not effective.

For example, for 43W equivalent LED lamp installed in 2016, the full savings (as calculated above in the Algorithm) should be claimed for the first four years, but a reduced annual savings (calculated energy savings above multiplied by the adjustment factor in the table below) should be claimed for the remainder of the measure life. 214&215

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²¹³ ISR is based on results presented in Ameren Missouri Lighting Impact and Process Evaluation: Program Year 2015. This value takes into account the time-delay of when bulbs are installed over subsequent program years. The reported ISR is based on the net present value (NPV) of the savings over 4 year installation period from the PY15 bulbs, discounted back to Year 1 at 6.95% (utility discount rate). These evaluation results are from a retail-based lighting program with multiple delivery channels including point-of-sale markdown, online website, coupons, and social marketing distribution. ²¹⁴ These adjustments should be applied to kW and gas impacts as well.

²¹⁵ Calculated with EISA requirement of 45lumens/watt.

Lower Lumen Range	Upper Lumen Range	Mid Lumen Range	Watts EE	WattsBase before EISA 2020	Delta Watts before EISA 2020	WattsBase after EISA 2020 ²⁰⁸	Delta Watts after EISA 2020	Mid Life adjustment (in 2020) to first year savings
250	309	280	4.0	25	21	25	21	100.0%
310	749	530	6.7	29	22.3	9.4	2.7	12.1%
750	1049	900	10.1	43	32.9	13.4	3.3	10.0%
1050	1489	1270	12.8	53	40.2	18.9	6.1	15.2%
1490	2600	2045	17.4	72	54.6	24.8	7.4	13.6%
2,550	3,000	2,775	43.1	150	106.9	150	106.9	100.0%
3,001	3,999	3,500	53.8	200	146.2	200	146.2	100.0%
4,000	6,000	5,000	76.9	300	223.1	300	223.1	100.0%

Heating Penalty:

If electrically heated building:216

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6 and based upon Building Type. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta k = \Delta kWh * CF$$

Where:

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

- = 0.0001899635 for indoor lighting
- = 0.0000056160 for exterior lighting
- = 0.0001379439 for <u>exterior</u> 24/7 lighting

NATURAL GAS ENERGY SAVINGS

Heating penalty if fossil fuel heated building (or if heating fuel is unknown): 216207

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

²¹⁶ Results in a negative value because this is an increase in heating consumption due to the efficient lighting.

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 $IF_{Therms} \\$

= Lighting-HVAC Interaction Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6 and based upon Building Type. If unknown, use the C&I Average value.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

In order to account for the falling EISA-Qualified backdrop provision, an equivalent annual levelized baseline replacement cost over the lifetime of the LED bulb is calculated. The key assumptions used in this calculation are documented below:²¹⁷

Incandescent / Halogen	CFL	LED ALamp
\$1.80	\$2.20	\$5.06

The present value of replacement lamps and annual levelized replacement costs using utilities' average real discount rate of 6.91% are presented below:

Location	Location PV of replacement costs for period			Levelized annual replacement cost savings			
Location	2016 - 2017	2017 - 2018	2018 - 2019	2016 - 2017	2017 - 2018	2018 - 2019	
C&I Average	\$18.66	\$14.70	\$10.46	\$2.04	\$1.60	\$1.14	

Note: incandescent lamps in lumen range <310 and >2600 are exempt from EISA. For these bulb types, an O&M cost should be applied as follows. If unknown Building Type, assume C&I Average:

²¹⁷ All cost assumptions based on Cadmus "LED Incremental Cost Study: Overall Final Report," February 2016 (http://mahttp://ma-eeac.org/wordpress/wp-content/uploads/MA-Task-5b-LED-Incremental-Cost-Study_FINAL_01FEB2016.pdfeeac.org/wordpress/wp-content/uploads/MA-Task-5b-LED-Incremental-Cost-Study_FINAL_01FEB2016.pdf), p.19.

Building Type	Replacement Period (years) ²¹⁸	Replacement Cost
Large Office	0.32	
Medium Office	0.32	
Small Office	0.35	
Warehouse	0.35	
Stand-alone Retail	0.29	
Strip Mall	0.27	
Primary School	0.29	
Secondary School	0.29	
Supermarket	0.27	\$1.80 ²¹⁹
Quick Service Restaurant	0.16	
Full Service Restaurant	0.16	
Hospital	0.26	
Outpatient Health Care	0.26	
Small Hotel - Building	0.27	
Large Hotel - Building	0.27	
Midrise Apartment - Building	0.35	
C&I Average	0.30	

MEASURE CODE:

²¹⁸ Calculated by dividing assumed rated life of baseline bulb by hours of use. Assumed lifetime of EISA-qualified halogen/incandescent is 1000 hours (manufacturers are simply using a regular incandescent lamp with halogen fill gas rather Halogen Infrared to meet the standard (as provided by G. Arnold, NEEP and confirmed by N. Horowitz at NRDC)).
²¹⁹ Incandescent/halogen cost assumptions based on Cadmus "LED Incremental Cost Study: Overall Final Report," February 2016 (http://ma-eeac.org/wordpress/wp-content/uploads/MA-Task-5b-LED-Incremental-Cost-Study_FINAL_01FEB2016.pdf), p.19.

2.6.5 T5 Fixtures and Lamps

DESCRIPTION

T5 HO lamp/ballast systems have greater lumens per watt than a typical T8 system. The smaller lamp diameter of the T5HO also increases optical control efficiency and allows for more precise control and directional distribution of lighting. These characteristics make it easier to design light fixtures that can produce equal or greater light than standard T8 or T12 systems, while using fewer watts. In addition, when lighting designers specify T5 HO lamps/ballasts, they can use fewer luminaries per project, especially for large commercial projects, thus increasing energy savings further.²²⁰

The main markets served by T5 HO fixtures and lamps include retrofit in the commercial and nonresidential sector, specifically industrial, warehouse, and grocery facilities with higher ceiling heights that require maximum light output.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The definition of the efficient equipment is T5 HO high-bay (>15ft mounting height) fixtures with 3, 4, 6, or 8-lamp configurations.

DEFINITION OF BASELINE EQUIPMENT

The definition of baseline equipment varies based on number of lamps in a fixture and is defined in the baseline reference table at the end of this characterization. The default baseline is assumed to be a PulseStart Metal Halide fixture.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The deemed lifetime of the efficient equipment fixture is 15 years.²²¹

DEEMED MEASURE COST

Actual costs should be used if available. If not available, \$10/lamp and \$37.50/ballast can be used to account for installation labor costs.

LOADSHAPE

Lighting BUS Ext Lighting BUS Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

Lighting Research Center. T5 Fluorescent Systems. http://www.lrc.rpi.edu/programs/nlpip/lightingAnswers/lat5/abstract.asp
 Focus on Energy Evaluation "Business Programs: Measure Life Study" Final Report, August 9, 2009, prepared by PA Consulting Group.

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000}*Hours*WHF_e*ISR$$

Where:

Watts_{Base} = Custom input. If unknown, input wattage of the baseline system is dependent on new fixture configuration and found in the 'T5HO Efficient and Baseline Wattage

and Cost Assumptions' reference table below.

Wattsee = Custom Input. If unknown, input wattage depends on new fixture configuration (number of lamps) and hallast factor and number of fixtures. Value can be selected

(number of lamps) and ballast factor and number of fixtures. Value can be selected from the 'T5HO Efficient and Baseline Wattage and Cost Assumptions' reference

table below.

Hours = Average annual lighting hours of use as provided by the customer or selected from

the Lighting Reference Table in Section 2.6 as annual operating hours, by Building

Type. If hours or Building Type are unknown, use the C&I Average value.

WHF_e = Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Lighting Reference Table in Section 2.6 for each

Building Type. If building is un-cooled, the value is 1.0.

ISR = In Service Rate represents the percentage of reported lamps or fixtures that is

installed and operating and varies with the program delivery approach. Use 100% for programs with direct installation and/or installation verification procedures (e.g., verification inspections for a sample of projects); use 98% for program delivery without installation verification.²²² The ISR may also be set to 100% if the installation

verification is embedded in other evaluation adjustments.

Heating Penalty:

If electrically heated building:²²³

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours* ISR* (-IF_{kWH})$$

Where:

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

SUMMER COINCIDENT DEMAND SAVINGS

$$\Delta k = \Delta kWh * CF$$

²²² Based upon review of PY5-6 evaluations from ComEd, IL commercial lighting program (BILD).

²²³ Negative value because this is an increase in heating consumption due to the efficient lighting.

Where:

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635 for indoor lighting = 0.0000056160 for exterior lighting = 0.0001379439 for exterior 24/7 lighting

NATURAL GAS ENERGY SAVINGS

Heating penalty if fossil fuel heated building (or if heating fuel is unknown): 224

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

 $IF_{Therms} \hspace{0.5cm} = Lighting-HVAC \hspace{0.1cm} Interaction \hspace{0.1cm} Factor \hspace{0.1cm} for \hspace{0.1cm} gas \hspace{0.1cm} heating \hspace{0.1cm} impacts; \hspace{0.1cm} this \hspace{0.1cm} factor \hspace{0.1cm} represents$

the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

DEEMED O&M COST ADJUSTMENT CALCULATION

See reference tables for different cost assumptions for lamps and ballasts. When available, actual costs and hours of use should be used.

REFERENCE TABLES

T5HO Efficient and Baseline Wattage and Cost Assumptions²²⁵&²²⁶

EE Measure Description	Watts _{EE}	Baseline Description	Watts _{BASE}	Incremental Cost
3-Lamp T5 High-Bay	176	200 Watt Pulse Start Metal-Halide	227	\$100.00
4-Lamp T5 High-Bay	235	320 Watt Pulse Start Metal-Halide	364	\$100.00
6-Lamp T5 High-Bay	352	400 Watt Pulse Start Metal-Halide	455	\$100.00
8-Lamp T5 High-Bay	470	750 Watt Pulse Start Metal-Halide	825	\$100.00

²²⁴ Negative value because this is an increase in heating consumption due to the efficient lighting.

²²⁵ Reference Table adapted from Efficiency Vermont TRM, T5 Measure Savings Algorithms and Cost Assumptions, October,

²²⁶ Refer to "T5HO-adjusted deemed costs.baselines.xlsx" for more information.

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T5 HO Component Costs and Lifetimes²²⁷

	EE Measure			Baseline				
EE Measure Description	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost	Lamp Life (hrs)	Total Lamp Replacement Cost	Ballast Life (hrs)	Total Ballast Replacement Cost
3-Lamp T5 High-Bay	30,000	\$63.00	70,000	\$87.50	15,000	\$63.00	40,000	\$107.50
4-Lamp T5 High-Bay	30,000	\$84.00	70,000	\$87.50	20,000	\$68.00	40,000	\$117.50
6-Lamp T5 High-Bay	30,000	\$126.00	70,000	\$112.50	20,000	\$73.00	40,000	\$127.50
8-Lamp T5 High-Bay	30,000	\$168.00	70,000	\$137.50	20,000	\$78.00	40,000	\$137.50

MEASURE CODE:

 $^{^{227} \} Costs \ include \ labor \ cost-see \ ``T5HO-adjusted \ deemed \ costs. baselines.xlsx" \ for \ more \ information.$

2.6.6 LED Exit Sign

This measure characterizes the savings associated with installing a new LED exit sign (or retrofit kit) in place of a CFL or incandescent exit sign in a commercial building. LED exit signs use less power (\leq 5 watts), have a significantly longer lifetime, and have less maintenance costs compared to incandescent or CFL exit signs.²²⁸

This measure applies to the following program types: RF and DI.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment is an LED exit sign with an input power demand of 5 watts or less.²²⁹

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is the existing exit sign (either a CFL or incandescent unit).

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

See Lighting EUL Reference Table for EUL values by Lighting Measure Group.

DEEMED MEASURE COST

Actual program delivery costs should be used if available. If not, use the full cost of \$39²³⁰ for a new LED exit sign and \$25 for a retrofit kit, plus \$6.25 in labor,²³¹ for a total measure cost of \$45.25 and \$31.25, respectively.

LOADSHAPE

Lighting BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS²³²

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000}*Hours*WHF_e$$

Where:

²²⁸ ENERGY STAR® "Save Energy, Money and Prevent Pollution with LED Exit Signs."

²²⁹ ENERGY STAR® "Program Requirements for Exit Signs Version 3.0." While the EPA suspended the ENERGY STAR® Exit Sign specification effective May 1, 2008, Federal requirements specify minimum efficiency standards for electrically-powered, single-faced exit signs with integral lighting sources that are equivalent to ENERGY STAR® levels for input power demand of 5 watts or less per face.

²³⁰ Cost of new LED exit sign from ENERGY STAR® Exit Signs Calculator.xlsx.

²³¹ Assumption based on 15 minutes (including portion of travel time) and \$25 per hour, which is in line with the typical prevailing wage of a General Laborer, as per the Annual Wage Order No. 23 published by the Missouri Department of Labor.

²³² There is no ISR calculation. Exit signs and emergency lighting are required by federal regulations to be installed and functional in all public buildings as outlined by the U.S. Occupational Safety and Health Standards (USOSHA 1993).

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WattsBase

= Actual wattage if known, if unknown assume the following:

Baseline Type	Watts _{BASE}
Incandescent (dual sided)	50 W ²³³
Incandescent (single sided)	25 W
CFL (dual sided)	14 W ²³⁴
CFL (single sided)	7 W

Wattsee

= Actual wattage if known; if unknown assume 2W for singled sided and 4W for

dual sided.235

Hours

= Annual operating hours = 8,766

WHFe

= Waste heat factor for energy to account for cooling energy savings from efficient lighting is selected from the Lighting Reference Table in Section 2.6 for each

Building Type. If building is un-cooled, the value is 1.0.

HEATING PENALTY

If electrically heated building:236

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Reference Table in Section 2.8. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, including cooling savings, as calculated above.

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

CF = 0.0001899635

²³³ Average incandescent single sided (5W, 10W, 15W, 20W, 25W, 34W, 40W, 50W) from Appendix B 2013-14 Table of

Standard Fixture Wattages. Available at: http://www.aescinc.com/download/spc/2013SPCDocs/PGE/App%20B%20Standard%20Fixture%20Watts.pdf
²³⁴ Average CFL single sided (5W, 7W, 9W) from Appendix B 2013-14 Table of Standard Fixture Wattages. Available at: http://www.aescinc.com/download/spc/2013SPCDocs/PGE/App%20B%20Standard%20Fixture%20Watts.pdf

²³⁵ Average Exit LED watts are assumed as a 2W as listed in Appendix B 2013-14 Table of Standard Fixture Wattages. Available at: http://www.aesc-inc.com/download/spc/2013SPCDocs/PGE/App%20B%20Standard%20Fixture%20Watts.pdf

NATURAL GAS ENERGY SAVINGS

Heating penalty if fossil fuel heated building (or if heating is unknown):237

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

 IF_{Therms}

= Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 2.6 for each Building Type.

Other factors as defined above.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

The annual O&M cost adjustment savings should be calculated using the following component costs and lifetimes.

Component	Baseline Measure			
Component	Cost ²³⁸	Life (yrs) ²³⁹		
CFL lamp	\$8.91	0.63 years		
Incandescent lamp	\$7.39	0.14 years		

MEASURE CODE:

²³⁷ Negative value because this is an increase in heating consumption due to the efficient lighting.

²³⁸ Includes cost of labor and new replacement bulb. Labor cost of \$6.25 based on 15 minutes (including portion of travel time) and \$25 per hour, which is in line with the typical prevailing wage of a General Laborer, as per the Annual Wage Order No. 23 published by the Missouri Department of Labor. Cost of new 7W CFL bulb is \$2.66, from Itron "2010-2012 WO017 Ex Ante Measure Cost Study Final Report." Prepared for California Public Utilities Commission, May 27, 2014.

²³⁹ ENERGY STAR® "Save Energy, Money and Prevent Pollution with LED Exit Signs" states that CFL bulbs for exit signs typically have an average rated life of 5,000-6,000 hours. Given 24/7 run time, assume a CFL in an exit sign will require replacement every 0.63 years (5,500 hours/8,766 hours).

2.6.7 LED Specialty Lamp (Retired, effective 8/1/2023)

DESCRIPTION

This characterization provides savings assumptions for LED directional, decorative, and globe lamps. This characterization assumes that the LED is installed in a commercial location. This is therefore appropriate for commercially targeted programs, or, if the implementation strategy does not allow for the installation location to be known (e.g., an upstream retail program), utilities should develop an assumption of the Residential v Nonresidential split and apply the relevant assumptions to each portion.

Federal legislation stemming from the EISA requires all general-purpose light bulbs between 40W and 100W to be approximately 30% more energy efficient than standard incandescent bulbs. Production of 100W, standard efficacy incandescent lamps ended in 2012, followed by restrictions on 75W lamps in 2013 and 60W and 40W lamps in 2014. The baseline for this measure has therefore become bulbs (improved incandescent or halogen) that meet the new standard.

A provision in the EISA regulations requires that by January 1, 2020, all lamps meet efficiency criteria of at least 45 lumens per watt, in essence making the baseline equivalent to a current day CFL. However, in 2019, the Department of Energy issued two final rules and clarified that a) the EISA backstop provision had not been triggered and therefore b) the efficiency standard would not change in 2020. As of 10/15/2020, the 45 lumen per watt EISA standard is not effective.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, new lamps must be ENERGY STAR® labeled based upon the ENERGY STAR® specification v2.0 which will become effective on 1/2/2017.https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Lamps%20V2_0%20 Revised%20AUG-2016.pdf). Qualification could also be based on the Design Light Consortium's qualified product list.²⁴⁰

DEFINITION OF BASELINE EQUIPMENT

The baseline condition for this measure is assumed to be an EISA-qualified halogen or incandescent.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

See Lighting EUL Reference Table for EUL values by Lighting Measure Group.

DEEMED MEASURE COST

²⁴⁰ https://www.designlights.org/QPL

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Wherever possible, actual incremental costs should be used. If unavailable, assume the following incremental costs:²⁴¹

Bulb Type	LED Wattage	LED	Incandescent	Incremental Cost
Directional	< 20W	\$14.52	\$6.31	\$8.21
Directional	≥20W	\$45.85	\$0.51	\$39.54
	<15W	\$8.09		\$4.17
Decorative	15 to <25W	\$15.86	\$3.92	\$11.94
	≥25W	\$15.86		\$11.94

LOADSHAPE

Lighting BUS Ext Lighting BUS Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * WHF_e * ISR$$

Where:

 $Watts_{Base}$ = Based on bulb type and lumens of LED bulb installed. See table

below.

Wattsee = Actual wattage of LED purchased / installed - If unknown, use default

provided below:242

Hours = Average hours of use per year as provided by the customer or selected

from the Lighting Reference Table in Section 2.6 and based upon

Building Type. If unknown, use the C&I Average value.

WHFe = Waste heat factors for energy to account for cooling energy savings

from efficient lighting are provided for each Building Type in the

²⁴¹ Incandescent based on "2010-2012 WA017 Ex Ante Measure Cost Study Draft Report," Itron, February 28, 2014. LED lamp costs are based on a 2014/2015 VEIC review of a year's worth of LED sales through VEIC implemented programs. The retail cost was averaged and then DOE price projection trends (from Department of Energy, 2012; "Energy Savings Potential of Solid-State Lighting in General Illumination Applications," Table A.1) used to decrease the cost for a 2017 TRM assumption (see 2015 LED Sales Review.xls). LED costs are falling rapidly and should be reviewed in each update cycle.
²⁴² Wattsee defaults are based upon the average available ENERGY STAR® product, accessed 06/18/2015. For any lumen range

²⁴² Wattseg defaults are based upon the average available ENERGY STAR* product, accessed 06/18/2015. For any lumen range where there is no ENERGY STAR* product currently available, Wattseg is based upon the ENERGY STAR* minimum luminous efficacy (55Lm/W for lamps with rated wattages less than 15W and 65 Lm/W for lamps with rated wattages ≥ 15 watts) for the mid-point of the lumen range. See calculation at "cerified-light-bulbs-2015-06-18.xlsx." These assumptions should be reviewed regularly to ensure they represent the available product.

Lighting Reference Table in Section 2.6. If unknown, use the C&I Average value.

ISR

= In Service Rate represents the percentage of reported lamps or fixtures that is installed and operating and varies with the program delivery approach. Use 100% for programs with direct installation and/or installation verification procedures (e.g., verification inspections for a sample of projects); use 98.7% for program delivery without installation verification.²⁴³ The ISR may also be set to 100% if the installation verification is embedded in other evaluation adjustments.

Bulb Type	Lower Lumen Range	Upper Lumen Range	Watts _{Base}	Wattsee	Delta Watts
	250	349	25	5.6	19.4
	350	399	35	6.3	28.7
Directional	400	599	40	7.5	32.5
Directional	600	749	60	9.7	50.3
	750	999	75	12.7	62.3
	1000	1250	100	16.2	83.8
	70	89	10	1.8	8.2
	90	149	15	2.7	12.3
Decorative	150	299	25	3.2	21.8
	300	499	40	4.7	35.3
	500	699	60	6.9	53.1
	250	349	25	4.1	20.9
	350	499	40	5.9	34.1
Globe	500	574	60	7.6	52.4
	575	649	75	13.6	61.4
	650	1099	100	17.5	82.5
	1100	1300	150	13.0	137.0

Heating Penalty:

If electrically heated building:244

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

²⁴³ Based on results presented in Ameren Missouri Lighting Impact and Process Evaluation: Program Year 2015. This value takes into account the time-delay of when bulbs are installed over subsequent program years. The reported ISR is based on the net present value (NPV) of the savings over 4 year installation period from the PY15 bulbs, discounted back to Year 1 at 6.95% (utility discount rate). These evaluation results are from a retail-based lighting program with multiple delivery channels including point-of-sale markdown, online website, coupons, and social marketing distribution.

244 Results in a negative value because this is an increase in heating consumption due to the efficient lighting.

Where:

IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6 and based upon Building Type. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWh * CF$$

Where:

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635 for indoor lighting

= 0.0000056160 for exterior lighting

= 0.0001379439 for <u>exterior</u> 24/7 lighting

Other factors as defined above.

NATURAL GAS SAVINGS

Heating penalty if fossil fuel heated building (or if heating fuel is unknown):245

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

IF_{Therms} = Lighting-HVAC Interaction Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table in Section 2.6 and based upon Building Type. If unknown, use the C&I Average value.

DEEMED O&M COST ADJUSTMENT CALCULATION

O&M cost should be applied as follows:

²⁴⁵ Ibid.

Installation Location	Replacement Period (years) ²⁴⁶	Replacement Cost ²⁴⁷
Large Office	0.32	
Medium Office	0.32	
Small Office	0.35	
Warehouse	0.35	
Stand-alone Retail	0.29	
Strip Mall	0.27	
Primary School	0.29	Decorative:
Secondary School	0.29	\$6.31
Supermarket	0.27	
Quick Service Restaurant	0.16	Directional:
Full Service Restaurant	0.16	\$3.92
Hospital	0.26	
Outpatient Health Care	0.26	
Small Hotel - Building	0.27	
Large Hotel - Building	0.27	
Midrise Apartment - Building	0.35	
C&I Average	0.30	

MEASURE CODE:

²⁴⁶ Calculated by dividing assumed rated life of baseline bulb by hours of use. Assumed lifetime of EISA qualified Halogen/Incandescent is 1000 hours. The manufacturers are simply using a regular incandescent lamp with halogen fill gas rather than Halogen Infrared to meet the standard (as provided by G. Arnold, NEEP and confirmed by N. Horowitz at NRDC).
²⁴⁷ Incandescent costs based on "2010-2012 WA017 Ex Ante Measure Cost Study Draft Report," Itron, February 28, 2014.

2.6.8 Lighting Power Density

DESCRIPTION

This measure entails the installation of efficient lighting systems in either new construction or during substantial renovation of commercial buildings that triggers compliance with code. This methodology applies to situations where code specifies maximum lighting power density allowances (W/ft²). Either the Building Area Method or Space-by-Space (not recognized by IECC 2009) method as defined in IECC 2009, 2012, 2015, 2018 can be used for calculating the Interior Lighting Power Density (LPD). The measure consists of a design that has a lower LPD than code requires.

This measure was developed to be applicable to the following program types: NC and TOS. The measure is application for any project for which the project requires compliance with building code. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the lighting system must be more efficient than the baseline energy code maximum lighting power density in watts/square foot for either the interior space or exterior space.

DEFINITION OF BASELINE EQUIPMENT

The baseline is assumed to be the maximum lighting power density that meets the building code recognized by the local jurisdiction. For illustrative purposes in this characterization, IECC 2009, 2012, 2015, and 2018, are highlighted to demonstrate the methodology.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

See Lighting EUL Reference Table for EUL values by Lighting Measure Group.

DEEMED MEASURE COST

The actual incremental cost over a baseline system should be collected from the customer if possible or quantified using an alternative suitable source.

LOADSHAPE

Lighting BUS Ext Lighting BUS Miscellaneous BUS

Algorithm

²⁴⁸ Refer to the referenced code documents for specifics on calculating lighting power density using either the whole building method (IECC) or the Space by Space method (ASHRAE 90.1).

MEEIA 2019-21 Plan

ENERGY SAVINGS

$$\Delta kWh = \frac{WSF_{Base} - WSF_{EE}}{1000} * SF * Hours * WHF_{e}$$

Where:

WSF_{base} = Baseline lighting watts per square foot or linear foot as determined by

building or space type. IECC example whole building analysis values are

presented in the Reference Tables below.²⁴⁹

WSF_{EE} = The actual installed lighting watts per square foot or linear foot.

SF = Provided by customer based on square footage of the building area

applicable to the lighting design for new building.

Hours = Annual site-specific hours of operation of the lighting equipment

collected from the customer or selected from the Reference Table in

Section 2.8 if unavailable.

WHF_e = Waste Heat Factor for Energy to account for cooling savings from

efficient lighting is as provided in the Reference Table in Section 2.8 for

each Building Type. If building is not cooled, the value is 1.0.

Heating Penalty

If electrically heated building: 250

$$\Delta kWh_{heatpenalty} = \frac{WSF_{Base} - WSF_{EE}}{1000} * SF * Hours * (-IF_{kWH})$$

Where:

 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Reference Table in Section 2.8. If unknown, use the C&I Average value.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWh * CF$$

Where:

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635 for indoor lighting

= 0.0000056160 for exterior lighting

= 0.0001379439 for <u>exterior</u> 24/7 lighting

Other factors as defined above.

²⁴⁹ See IECC 2009, 2012 and 2015 - Reference Code documentation for additional information.

²⁵⁰ Negative value because this is an increase in heating consumption due to the efficient lighting.

NATURAL GAS ENERGY SAVINGS

$$\Delta Therms = \frac{WSF_{Base} - WSF_{EE}}{1000} * SF * Hours * (-IF_{therms})$$

Where:

IFTherm

= Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 2.8 for each Building Type.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

REFERENCE TABLES

Lighting Power Density Values from IECC 2009, 2012 and 2015 for Interior Commercial New Construction and Substantial Renovation Building Area Method

D 111 4 75 251	IECC 2009	IECC 2012	IECC 2015
Building Area Type ²⁵¹	Lighting Power Density (w/ft²)	Lighting Power Density (w/ft²)	Lighting Power Density (w/ft²)
Automativa Egaility	0.9	0.9	0.80
Automotive Facility Convention Center	1.2	1.2	1.01
Convention Center Court House	1.2	1.2	1.01
	1.3	1.2	1.01
Dining: Bar Lounge/Leisure	-	-	0.9
Dining: Cafeteria/Fast Food	1.4	1.4	
Dining: Family	1.6	1.6	0.95
Dormitory	1.0	1.0	0.57
Exercise Center	1.0	1.0	0.84
Fire station	1.0	0.8	0.67
Gymnasium	1.1	1.1	0.94
Healthcare – clinic	1.0	1.0	0.90
Hospital	1.2	1.2	1.05
Hotel	1.0	1.0	0.87
Library	1.3	1.3	1.19
Manufacturing Facility	1.3	1.3	1.17
Motel	1.0	1.0	0.87
Motion Picture Theater	1.2	1.2	0.76
Multifamily	0.7	0.7	0.51
Museum	1.1	1.1	1.02
Office	1.0	0.9	0.82
Parking Garage	0.3	0.3	0.21
Penitentiary	1.0	1.0	0.81
Performing Arts Theater	1.6	1.6	1.39
Police Station	1.0	1.0	0.87
Post Office	1.1	1.1	0.87
Religious Building	1.3	1.3	1.0
Retail ²⁵²	1.5	1.4	1.26
School/University	1.2	1.2	0.87
Sports Arena	1.1	1.1	0.91
Town Hall	1.1	1.1	0.89
Transportation	1.0	1.0	0.70
Warehouse	0.8	0.6	0.66
Workshop	1.4	1.4	1.19

²⁵¹ In cases where both a general building area type and a more specific building area type are listed, the more specific building area type shall apply.
²⁵² Where lighting equipment is specified to be installed to highlight specific merchandise in addition to lighting equipment

²⁵² Where lighting equipment is specified to be installed to highlight specific merchandise in addition to lighting equipment specified for general lighting and is switched or dimmed on circuits different from the circuits for general lighting, the small of the actual wattage of the lighting equipment installed specifically for merchandise, or additional lighting power as determined below shall be added to the interior lighting power determined in accordance with this line item.

Lighting Power Density Values from IECC 2012 for Interior Commercial New Construction and Substantial Renovation Space by Space Method

COMMON SPACE-BY-SPACE TYPES	LPD (w/ft²)
Atrium - First 40 feet in height	0.03 per ft. ht
Atrium - Above 40 feet in height	0.02 per ft. ht
Audience/seating area - permanent	
For auditorium	0.9
For performing arts theater For motion picture theater	2.6 1.2
Classroom/lecture/training	1.30
Conference/meeting/multipurpose	1.2
Corridor/transition	0.7
Dining area	
Bar/lounge/leisure dining Family dining area	1.40 1.40
Dressing/fitting room performing arts theater	1.1
Electrical/mechanical	1.10
Food preparation	1.10
· · ·	1.20
Laboratory for classrooms	
Laboratory for medical/industrial/research	1.8
Lobby	1.10
Lobby for performing arts theater	3.3
Lobby for motion picture theater	1.0
Locker room	0.80
Lounge recreation	0.8
Office – enclosed	1.1
Office – open plan	1.0
Restroom	1.0
Sales area	1.6ª
Stairway	0.70
Storage	0.8
Workshop	1.60
Courthouse/police station/penetentiary	
Courtroom	1.90
Confinement cells Judge chambers	1.30
Penitentiary audience seating	0.5
Penitentiary classroom	1.3
Penitentiary dining	1.1
BUILDING SPECIFIC SPACE-BY-SPACE	
Automotive - service/repair	0.70
Bank/office - banking activity area	1.5
Dormitory living quarters	1.10
Gymnasium/fitness center	0.0
Fitness area	0.9
Gymnasium audience/seating Playing area	1.40

COMMON SPACE-BY-SPACE TYPES	LPD (w/ft²)
Healthcare clinic/hospital	
Corridors/transition	1.00
Exam/treatment	1.70
Emergency	2.70
Public and staff lounge	0.80
Medical supplies	1.40
Nursery	0.9
Nurse station	1.00
Physical therapy	0.90
Patient room	0.70
Pharmacy	1.20
Radiology/imaging	1.3
Operating room	2.20
Recovery	1.2
Lounge/recreation	0.8
Laundry – washing	0.60
Hotel	
Dining area	1.30
Guest rooms	1.10
Hotel lobby	2.10
Highway lodging dining	1.20
Highway lodging guest rooms	1.10
Library	
Stacks	1.70
Card file and cataloguing	1.10
Reading area	1.20
Manufacturing	
Corridors/transition	0.40
Detailed manufacturing	1.3
Equipment room	1.0
Extra high bay (> 50-foot floor-ceiling height)	1.1
High bay (25 50-foot floor-ceiling height)	1.20
Low bay (< 25-foot floor-ceiling height)	1.2
Museum	
General exhibition	1.00
Restoration	1.70
Parking garage – garage areas	0.2
Convention center	1 0.2
Exhibit space	1.50
Audience/seating area	0.90
	0.70
Fire stations	0.90
Engine room	0.80
Sleeping quarters	0.30
Post office	0.9
Sorting area	J.,
Religious building	
Fellowship hall	0.60
Audience seating	2.40
Worship pulpit/choir	2.40
Retail	
Dressing/fitting area	0.9
Mall concourse	1.6
Sales area	1.6°

(continued)

TABLE C405.5.2(2)—continued INTERIOR LIGHTING POWER ALLOWANCES: SPACE-BY-SPACE METHOD

STAGE BY STAGE METHOD				
BUILDING SPECIFIC SPACE-BY-SPACE TYPES	LPD (w/ft ²)			
Sports arena				
Audience seating	0.4			
Court sports area - Class 4	0.7			
Court sports area – Class 3	1.2			
Court sports area - Class 2	1.9			
Court sports area - Class I	3.0			
Ring sports area	2.7			
Transportation	The Street of th			
Air/train/bus baggage area	1.00			
Airport concourse	0.60			
Terminal - ticket counter	1.50			
Warehouse				
Fine material storage	1.40			
Medium/bulky material	0.60			

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Lighting Power Density Values from IECC 2015 for Interior Commercial New Construction and Substantial Renovation Space by Space Method:

TABLE C405.4.2(2)
INTERIOR LIGHTING POWER ALLOWANCES:
SPACE-BY-SPACE METHOD

TABLE C405.4.2(2)—continued INTERIOR LIGHTING POWER ALLOWANCES: SPACE-BY-SPACE METHOD

COMMON SPACE TYPES	LPD (watts/sq.ft)	COMMON SPACE TYPES*	LPD (watts/sq.ft)
Atrium	_ to (memory.it)	Food preparation area	1.21
Autun	0.03 per foot	Guest room	0.47
Less than 40 feet in height	in total height	Laboratory	
23%		In or as a classroom	1.43
Greater than 40 feet in height	0.40 + 0.02 per foot in total height	Otherwise	1.81
	in total neight	Laundry/washing area	0.6
Audience seating area		Loading dock, interior	0.47
In an auditorium	0.63	Lobby	
In a convention center	0.82	In a facility for the visually impaired (and	1.8
In a gymnasium	0.65	not used primarily by the staff) ^b For an elevator	0.64
In a motion picture theater	1.14	In a hotel	1.06
In a penitentiary	0.28	In a motion picture theater	0.59
In a performing arts theater	2.43	In a performing arts theater	2.0
In a religious building	1.53	Otherwise	0.9
	0.43	Locker room	0.75
In a sports arena		Lounge/breakroom	
Otherwise	0.43	In a healthcare facility	0.92
Banking activity area	1.01	Otherwise	0.73
Breakroom (See Lounge/Breakroom)		Office	
Classroom/lecture hall/training room	7	Enclosed	1.11
In a penitentiary	1.34	Open plan	0.98
Otherwise	1.24	Parking area, interior	0.19
2277993	1.23	Pharmacy area	1.68
Conference/meeting/multipurpose room	1377	Restroom	
Copy/print room	0.72	In a facility for the visually impaired (and not used primarily by the staff ^b	1.21
Corridor		Otherwise	0.98
In a facility for the visually impaired (and	0.92	Sales area	1.59
not used primarily by the staff) ^b		Seating area, general	0.54
In a hospital	0.79	Stairway (See space containing stairway)	
In a manufacturing facility	0.41	Stairwell	0.69
Otherwise	0.66	Storage room	0.63
Courtroom	1.72	Vehicular maintenance area	0.67
Computer room	1.71	Workshop	1.59
Dining area		BUILDING TYPE SPECIFIC SPACE TYPES*	LPD (watts/sq.ft)
	0.00	Facility for the visually impaired ^b	
In a penitentiary	0.96	In a chapel (and not used primarily by the staff)	2.21
In a facility for the visually impaired (and not used primarily by the staff) ^b	1.9	In a recreation room (and not used primarily by the staff)	2.41
In bar/lounge or leisure dining	1.07	Automotive (See Vehicular Maintenance Area	bove)
In cafeteria or fast food dining	0.65	Convention Center—exhibit space	1.45
In family dining	0.89	Dormitory—living quarters	0.38
Otherwise	0.65	Fire Station—sleeping quarters	0.22
Electrical/mechanical room	0.95	Gymnasium/fitness center	The region of the
	0.56	In an exercise area	0.72
Emergency vehicle garage	0.30	In a playing area	1.2

(continued) (continued)

TABLE C405.4.2(2)—continued INTERIOR LIGHTING POWER ALLOWANCES: SPACE-BY-SPACE METHOD

BUILDING TYPE SPECIFIC SPACE TYPES*	LPD (watts/sq.ft)
healthcare facility	
In an exam/treatment room	1.66
In an imaging room	1.51
In a medical supply room	0.74
In a nursery	0.88
In a nurse's station	0.71
In an operating room	2.48
In a patient room	0.62
In a physical therapy room	0.91
In a recovery room	1.15
Library	V2
In a reading area	1.06
In the stacks	1.71
Manufacturing facility	V.7
In a detailed manufacturing area	1.29
In an equipment room	0.74
In an extra high bay area (greater than 50' floor-to-ceiling height)	1.05
In a high bay area (25-50' floor-to-ceiling height)	1.23
In a low bay area (less than 25' floor-to- ceiling height)	1.19
Museum	103
In a general exhibition area	1.05
In a restoration room	1.02
Performing arts theater—dressing room	0.61
Post Office—Sorting Area	0.94
Religious buildings	
In a fellowship hall	0.64
In a worship/pulpit/choir area	1.53
Retail facilities	11100
In a dressing/fitting room	0.71
In a mall concourse	1.1
Sports arena—playing area	
For a Class I facility	3.68
For a Class II facility	2.4
For a Class III facility	1.8
For a Class IV facility	1.2
Transportation facility	373,446
In a baggage/carousel area	0.53
In an airport concourse	0.36
At a terminal ticket counter	0.8
Warehouse—storage area	
For medium to bulky, palletized items	0.58
For smaller, hand-carried items	0.95

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a. In cases where both a common space type and a building area specific space type are listed, the building area specific space type are listed, the building area specific space type shall apply b. A. Facility for the Visually Impaired' is a facility that is licensed or will be licensed by local or state authorities for seuior long-term care, adult daycare, senior support or people with special visual needs.

The exterior lighting design will be based on the building location and the applicable "Lighting Zone" as defined in IECC 2015 Table C405.5.2(1) which follows. This table is identical to IECC 2012 Table C405.6.2(1) and IECC 2009 Table 505.6.2(1).

TABLE C405.5.2(1) EXTERIOR LIGHTING ZONES

LIGHTING ZONE	DESCRIPTION				
1	Developed areas of national parks, state parks, forest land, and rural areas				
2	Areas predominantly consisting of residential zoning, neighborhood business districts, light industrial with limited nighttime use and residential mixed-use areas				
3	All other areas not classified as lighting zone 1, 2 or 4				
4	High-activity commercial districts in major metropoli- tan areas as designated by the local land use planning authority				

The lighting power density savings will be based on reductions below the allowable design levels as specified in IECC 2009 Table 505.6.2(2), IECC 2012 Table C405.6.2(2) or IECC 2015 Table C405.5.2(2).

Allowable Design Levels from IECC 2009

TABLE 505.6.2(2) INDIVIDUAL LIGHTING POWER ALLOWANCES FOR BUILDING EXTERIORS

		Zone 1	Zone 2	Zone 3	Zone 4				
Base Site Allowance (Base allowance may be used in tradable or nontradable surfaces.)		500W	600W	750W	1300W				
	Uncovered Parking Areas								
	Parking areas and drives	0.04 W/ft ²	0.06 W/ft ²	0.10 W/ft ²	0.13 W/ft ²				
	Building Grounds								
	Walkways less than 10 feet wide	0.7 W/linear foot	0.7 W/linear foot	0.8 W/linear foot	1.0 W/linear foot				
	Walkways 10 feet wide or greater, plaza areas special feature areas	0.14 W/ft ²	0.14 W/ft ²	0.16 W/ft ²	0.2 W/ft ²				
	Stairways	0.75 W/ft ²	1.0 W/ft ²	1.0 W/ft ²	1.0 W/ft ²				
	Pedestrian tunnels	0.15 W/ft ²	0.15 W/ft ²	0.2 W/ft ²	0.3 W/ft ²				
Tradable Surfaces (Lighting power		В	uliding Entrances and Exi	ts					
densities for uncovered parking areas, building grounds, building	Main entries	20 W/linear foot of door width	20 W/linear foot of door width	30 W/linear foot of door width	30 W/linear foot of door width				
entrances and exits, canopies and overhangs and outdoor sales areas	Other doors	20 W/linear foot of door width	20 W/linear foot of door width	20 W/linear foot of door width	20 W/linear foot of door width				
may be traded.)	Entry canopies	0.25 W/ft ²	0.25 W/ft ²	0.4 W/ft ²	0.4 W/ft ²				
	Sales Canopies								
	Free-standing and attached	0.6 W/ft ²	0.6 W/ft ²	0.8 W/ft ²	1.0 W/ft ²				
	Outdoor Sales								
	Open areas (including vehicle sales lots)	0.25 W/ft ²	0.25 W/ft ²	0.5 W/ft ²	0.7 W/ft ²				
	Street frontage for vehicle sales lots in addition to "open area" allowance	No allowance	lOW/linear foot	lOW/linear foot	30 W/linear foot				
Nontradable Surfaces (Lighting power density calculations for the following applications can be used only for the specific application and cannot be traded between surfaces or with other exterior lighting. The following allowances are in addition to any allowance otherwise permitted in the "Tradable Surfaces"	Building facades	No allowance	0.1 W/ft ² for each illuminated wall or surface or 2.5 W/linear foot for each illuminated wall or surface length	0.15 W/ft ² for each illuminated wall or surface or 3.75 W/linear foot for each illuminated wall or surface length	0.2 W/ft ² for each illuminated wall or surface or 5.0 W/linear foot for each illuminate wall or surface length				
	Automated teller machines and night depositories	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location				
	Entrances and gatehouse inspection stations at guarded facilities	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area				
	Loading areas for law enforcement, fire, ambulance and other emergency service vehicles	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area				
section of this table.)	Drive-up windows/doors	400 W per drive-through	400 W per drive-through	400 W per drive-through	400 W per drive-through				
	Parking near 24-hour retail entrances	800 W per main entry	800 W per main entry	800 W per main entry	800 W per main entry				

For SI: 1 foot = 304.8 mm, 1 watt per square foot = $W/0.0929 \text{ m}^2$.

Allowable Design Levels from IECC 2012

TABLE C405.6.2(2) INDIVIDUAL LIGHTING POWER ALLOWANCES FOR BUILDING EXTERIORS

			LIGHTIN	IG ZONES				
		Zone 1	Zone 2	Zone 3	Zone 4			
Base Site Allowance (Base allowance is usable in tradable or nontradable surfaces.)		500 W	600 W	750 W	1300 W			
			Uncovered Parking Areas					
	Parking areas and drives	0.04 W/ft ²	0.06 W/ft ²	0.10 W/ft ²	0.13 W/ft ²			
			Building Grounds					
	Walkways less than 10 feet wide	0.7 W/linear foot	0.7 W/linear foot	0.8 W/linear foot	1.0 W/linear foot			
	Walkways 10 feet wide or greater, plaza areas special feature areas	0.14 W/ft ²	0.14 W/ft ²	0.16 W/ft ²	0.2 W/ft ²			
_	Stairways	0.75 W/ft ²	1.0 W/ft ²	1.0 W/ft ²	1.0 W/ft ²			
Tradable Surfaces	Pedestrian tunnels	0.15 W/ft ²	0.15 W/ft ²	0.2 W/ft ²	0.3 W/ft ²			
(Lighting power		E	Building Entrances and Ex	its				
densities for uncovered parking areas, building grounds, building	Main entries	20 W/linear foot of door width	20 W/linear foot of door width	30 W/linear foot of door width	30 W/linear foot of door width			
entrances and exits, canopies and overhangs	Other doors	20 W/linear foot of door width	20 W/linear foot of door width	20 W/linear foot of door width	20 W/linear foot of door width			
and outdoor sales areas are tradable.)	Entry canopies	0.25 W/ft ²	0.25 W/ft ²	0.4 W/ft ²	0.4 W/ft ²			
are tradable.)	Sales Canopies							
	Free-standing and attached	0.6 W/ft²	0.6 W/ft ²	0.8 W/ft ²	1.0 W/ft ²			
	Outdoor Sales							
	Open areas (including vehicle sales lots)	0.25 W/ft ²	0.25 W/ft ²	0.5 W/ft ²	0.7 W/ft ²			
	Street frontage for vehicle sales lots in addition to "open area" allowance	No allowance	10 W/linear foot	10 W/linear foot	30 W/linear foot			
Nontradable Surfaces (Lighting power density calculations	Building facades	No allowance	0.1 W/ft² for each illuminated wall or surface or 2.5 W/linear foot for each illuminated wall or surface length	0.15 W/ft² for each illuminated wall or surface or 3.75 W/linear foot for each illuminated wall or surface length	0.2 W/ft ² for each illuminated wall or surface or 5.0 W/linear foot for each illuminated wall or surface length			
for the following applications can be used only for the specific application and cannot be traded between surfaces or with other exterior lighting. The following allowances are in addition to any allowance otherwise permitted in the	Automated teller machines and night depositories	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location			
	Entrances and gatehouse inspection stations at guarded facilities	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area	0.75 W/ft ² of covered and uncovered area			
	Loading areas for law enforcement, fire, ambulance and other emergency service vehicles	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area	0.5 W/ft ² of covered and uncovered area			
"Tradable Surfaces" section of this table.)	Drive-up windows/doors	400 W per drive-through	400 W per drive-through	400 W per drive-through	400 W per drive-through			
	Parking near 24-hour retail entrances	800 W per main entry	800 W per main entry	800 W per main entry	800 W per main entry			

For SI: 1 foot = 304.8 mm, 1 watt per square foot = W/0.0929 m².

Allowable Design Levels from IECC 2015

TABLE C405.5.2(2) INDIVIDUAL LIGHTING POWER ALLOWANCES FOR BUILDING EXTERIORS

			LIGHTII	NG ZONES						
		Zone 1	Zone 2	Zone 3	Zone 4					
Base Site Allowance (Base allowance is usable in tradable or nontradable surfaces.)		500 W	600 W	750 W	1300 W					
	Uncovered Parking Areas									
·	Parking areas and drives	0.04 W/ft ²	0.06 W/ ft ²	0.10 W/ft ²	0.13 W/ft ²					
	Building Grounds									
·	Walkways less than 10 feet wide	0.7 W/linear foot	0.7 W/linear foot	0.8 W/linear foot	1.0 W/linear foot					
	Walkways 10 feet wide or greater, plaza areas special feature areas	0.14 W/ft²	0.14 W/ft²	0.16 W/ft ²	0.2 W/ft²					
	Stairways	0.75 W/ft ²	1.0 W/ft ²	1.0 W/ft ²	1.0 W/ft ²					
Tradable Surfaces	Pedestrian tunnels	0.15 W/ft ²	0.15 W/ft ²	0.2 W/ft ²	0.3 W/ft ²					
(Lighting power	Building Entrances and Exits									
densities for uncovered parking areas, building grounds, building entrances and exits, canopies and overhangs and outdoor sales areas are tradable.)	Main entries	20 W/linear foot of door width	20 W/linear foot of door width	30 W/linear foot of door width	30 W/linear foot of door width					
	Other doors	20 W/linear foot of door width								
	Entry canopies	0.25 W/ft ²	0.25 W/ft ²	0.4 W/ft ²	0.4 W/ft ²					
	Sales Canopies									
•	Free-standing and attached	0.6 W/ft²	0.6 W/ft ²	0.8 W/ft ²	1.0 W/ft²					
·	Outdoor Sales									
	Open areas (including vehicle sales lots)	0.25 W/ft ²	0.25 W/ft ²	0.5 W/ft ²	0.7 W/ft ²					
	Street frontage for vehicle sales lots in addition to "open area" allowance	No allowance	10 W/linear foot	10 W/linear foot	30 W/linear foot					
Nontradable Surfaces	Building facades	No allowance	0.075 W/ft² of gross above-grade wall area	0.113 W/ft² of gross above-grade wall area	0.15 W/ft² of gross above-grade wall area					
(Lighting power density calculations for the following applications can be used only for the specific application and cannot be traded between surfaces or with other exterior lighting. The following allowances are in addition to any allowance otherwise	Automated teller machines (ATM) and night depositories	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location	270 W per location plus 90 W per additional ATM per location					
	Entrances and gatehouse inspection stations at guarded facilities	0.75 W/ft² of covered and uncovered area	0.75 W/ft² of covered and uncovered area	0.75 W/ft² of covered and uncovered area	0.75 W/ft² of covered and uncovered area					
	Loading areas for law enforcement, fire, ambulance and other emergency service vehicles	0.5 W/ft² of covered and uncovered area	0.5 W/ft² of covered and uncovered area	0.5 W/ft² of covered and uncovered area	0.5 W/ft² of covered and uncovered area					
permitted in the "Tradable Surfaces"	Drive-up windows/doors	400 W per drive-through								
section of this table.)	Parking near 24-hour retail entrances	800 W per main entry								

For SI: 1 foot = 304.8 mm, 1 watt per square foot = $W/0.0929 \text{ m}^2$. W = watts.

MEASURE CODE

2.6.9 Metal Halide Fixtures and Lamps

DESCRIPTION

This measure involves the installation of high efficiency pulse start metal halide fixtures and lamps in place of a standard metal halide. Pulse start metal halide luminaires produce more lumens per watt and have an improved lumen maintenance compared to standard probe start technology. Similarly, the high efficiency pulse start metal halide ballast lasts longer than a standard system due to their cooler operating temperatures.²⁵³

This measure was developed to be applicable for the following program type: RF.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient condition is an EISA-compliant pulse start metal halide lamp and ballasts for luminaires. Under 2009 federal rulings metal halide ballasts in low-watt options (150W-500W fixtures) must be pulse start and have a minimum ballast efficiency of 88%.²⁵⁴ Amendments made in 2014 require more stringent energy conservations standards with compliance required by February 10, 2017.²⁵⁵

DEFINITION OF BASELINE EQUIPMENT

The baseline condition is the existing bulb and fixture. If unknown assume, High Intensity Discharge (HID) Metal Halide lighting with probe start fixture and a standard ≤ 400 Watt lamp.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The measure life is assumed to be 15 years.²⁵⁶

DEEMED MEASURE COST

Actual costs should be used when available. If unknown, cost is assumed to be \$267.257

LOADSHAPE

Lighting BUS

²⁵³ Building a Brighter Future: Your Guide to EISA-Compliant Ballast and Lamp Solutions from Philips Lighting: http://1000bulbs.com/pdf/advance%20eisa%20brochure.pdf

²⁵⁴ Under EISA rulings, metal halide ballasts in low-watt options must be pulse start and have a minimum ballast efficiency of 88%. This ruling virtually eliminates the manufacture of probe start (ceramic) fixtures but some exemptions exist including significantly the 150w wet location fixtures (as rated per NEC 2002, section 410.4 (A)). These will be replaced by 150W. Department of Energy – 10 CFR Part 431 – Energy Conservation Program: Energy Conservation Standards for Metal Halide Lamp Fixtures; Final Rule 7746 Federal Register / Vol. 79, No. 27 / Monday, February 10, 2014 / Rules and Regulations https://www.federalregister.gov/articles/2014/02/10/2014-02356/energy-conservation-program-energy-conservation-standardsfor-metal-halide-lamp-fixtures#h-9
²⁵⁵ The revised 2014 efficiency standards for metal halides require that luminaires produced on or after February 10, 2017, must

not contain a probe-start metal halide ballast. Exceptions to this ruling include, metal halide luminaires with a regulated-lag ballast that utilize an electronic ballasts which operates at 480V and those which utilize a high-frequency (≥1000Hz) electronic ballast that utilize an electronic ballasts which operates at 480V and those which utilize a high-frequency (≥1000Hz) electronic ballast. Department of Energy − 10 CFR Part 431 − Energy Conservation Program: Energy Conservation Standards for Metal Halide Lamp Fixtures; Final Rule 7746 Federal Register / Vol. 79, No. 27 / Monday, February 10, 2014 / Rules and Regulations https://www.federalregister.gov/articles/2014/02/10/2014-02356/energy-conservation-program-energy-conservation-standardsformetal-halide-lamp-fixtures#h-9

266 GDS Associates, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, June 2007,

²⁵⁶ GDS Associates, Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, June 2007, http://library.ceel.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLights&HVACGDS_1Jun2007.pdf
²⁵⁷ Assuming cost of lamp and fixture combined per Itron, Inc. 2010-2012 WO017 Ex Ante Measure Cost Study – Final Report (Deemed Measures), May 27, 2014.

Ext Lighting BUS Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * WHF_e * ISR$$

Where:

Watts_{Base} = Input wattage of the existing system which depends on the baseline

fixture configuration (number and type of lamp). Value can be selected from the reference table at the end of the characterization or a custom

value can be used.

Wattsee = New Input wattage of EE fixture, which depends on new fixture

configuration. Value can be selected from the appropriate reference table at the end of the characterization, or a custom value can be used.

Hours = Average annual lighting hours of use as provided by the customer or

selected from the Lighting Reference Table in Section 2.6. If hours or

Building Type are unknown, use the C&I Average value.

WHF_e = Waste heat factor for energy to account for cooling energy savings

from efficient lighting is selected from the Reference Table in Section

2.8 for each Building Type.

If building is un-cooled, the value is 1.0.

ISR = In Service Rate is assumed to be 100%

Heating Penalty:

If electrically heated building:²⁵⁸

$$\Delta kWh_{heatpenalty} = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours*ISR*(-IF_{kWH})$$

Where:

 IF_{kWh} = Lighting-HVAC Interaction Factor for electric heating impacts; this

factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Reference Table in Section 2.8. If

unknown, use the C&I Average value.

SUMMER COINCIDENT DEMAND SAVINGS

²⁵⁸ Negative value because this is an increase in heating consumption due to the efficient lighting.

$$\Delta kW = \Delta kWh * CF$$

Where:

 ΔkWh = as calculated above.

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001899635 for indoor lighting = 0.0000056160 for exterior lighting = 0.0001379439 for <u>exterior</u> 24/7 lighting

NATURAL GAS SAVINGS 259

$$\Delta Therms = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours * ISR * (-IF_{therms})$$

Where:

IF_{Therms} = Lighting-HVAC Interaction Factor for gas heating impacts; this factor

represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Please select from the Reference Table in Section 2.8 for each Building Type.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

No O&M adjustments apply to this measure.260

REFERENCE TABLES²⁶¹

Lamp Watt _{EE}	Efficient Fixture Ballast	Efficient System Lumen	System Watt _{EE}	Lamp Watt _{Base}	Baselines Ballast ²⁶²	System Watts _{Base}	Baseline System Lumen
Pulse Start MH 150W	Pulse Start- CWA Ballast	10500	185	Probe Start MH 175W	standard C&C	210	9100
Pulse Start MH 175W	Pulse Start- CWA Ballast	11200	208	Probe Start MH 175W	standard C&C	210	9100
Pulse Start MH 200W	Pulse Start- CWA Ballast	16800	232	Probe Start MH250W	standard C&C	295	13500
Pulse Start MH 250W	Pulse Start- CWA Ballast	16625	290	Probe Start MH250W	standard C&C	295	13500

²⁵⁹ Negative value because this is an increase in heating consumption due to the efficient lighting

²⁶⁰ Given that probe start MH technology is becoming a technology of the past, it is assumed that upon failure they would have been replaced with pulse start technology. ²⁶¹ Per lamp/ballast.

²⁶² Standard Magnetic Core and Coil ballast systems are common for Metal Halide lamp wattages 175-400. See Panasonic "Metal Halide: Probe Start vs. Pulse Start."

Ameren Missouri

Appendix H - TRM - Vol. 2: C&I Measures

Pulse Start	Pulse Start-	21000	368	Probe Start	standard	458	24000			
MH 320W	CWA Ballast	21000	300	MH400W	C&C	430	24000			
Pulse Start	Pulse Start-	25200	400	Probe Start	standard	458	24000			
MH350W	CWA Ballast	23200	23200	23200	23200	23200 400	MH400W	C&C	436	24000
Pulse Start	Pulse Start-	20020	450	Probe Start	standard	450	24000			
MH 400W	CWA Ballast	29820	452	MH400W	C&C	458	24000			

MEASURE CODE:

2.6.10 Occupancy Lighting Sensor Controls

DESCRIPTION

Occupancy sensors are devices that reduce lighting levels by turning lights on or off in response to the presence (or absence) of people in a defined area. Associated energy savings depends on the Building Type, location area covered, type of lighting and activity, and occupancy pattern.²⁶³

This measure relates to the installation of interior occupancy sensors on new fixtures in an existing lighting system. Lighting control types covered by this measure include remote-mounted and fixture mounted. It does not cover automatic photo sensors, time clocks, and energy management systems. All sensors must be hard wired and control interior lighting.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

It is assumed that this measure characterization applies to only fixture-mounted occupancy sensors and remote mounted occupancy sensors.

DEFINITION OF BASELINE EQUIPMENT

The baseline efficiency case assumes lighting fixtures with no occupancy controls.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life for all lighting controls is assumed to be 10 years. ²⁶⁴

DEEMED MEASURE COST

When available, the actual cost of the measure shall be used. When not available, the following default values are provided:

Lighting control type	Cost ²⁶⁵
Full cost of fixture mounted occupancy sensor	\$45
Full cost of remote (ceiling) mounted occupancy sensor	\$105

LOADSHAPE

Lighting BUS Miscellaneous BUS Ext Lighting BUS

Algorithm

CALCULATION OF SAVINGS

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²⁶³ United States Department of the Interior. Greening the Department of Interior. http://www.doi.gov/archive/greening/energy/occupy.html

²⁶⁴ Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, June 2007.

 $^{^{265}\,\}mathrm{Based}$ on averaging typical prices quoted by online vendors.

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = kW_{Controlled} * Hours * ESF * WHF_{e}$

Where:

= Total lighting load connected to the control in kilowatts. Savings is kW_{Controlled}

per control. The total connected load per control should be collected from the customer, or use the default values presented below.

= The total annual operating hours of lighting for each type of Hours

building before occupancy sensors. This number should be collected from the customer. If no data is available, the deemed average number of operating hours by Building Type should be used as provided by Lighting Reference Table in Section 2.6. If Building

Type is unknown, use the C&I Average value.

ESF = Energy Savings factor (represents the percentage reduction to the

> operating Hours from the non-controlled baseline lighting system). Determined on a site-specific basis or using the default values below: = Waste heat factor for energy to account for cooling energy savings

from more efficient lighting is provided in the Lighting Reference

Table in Section 2.6.

Lighting Control Type Interior	Default kW controlled ²⁶⁶
Fixture-mounted occupancy sensor	0.138 (per fixture)
Remote (ceiling) mounted occupancy sensor	0.338 (per control)

Lighting Control Type	Energy Savings Factor ²⁶⁷
Fixture-mounted sensor	24%
Remote (ceiling) mounted occupancy sensor	24%
Network Connected controls	24%

Heating Penalty:

WHFe

If electrically heated building:268

 $\Delta kWh_{heatpenalty} = kW_{controlled} * Hours * ESF * (-IF_{kWH})$

Where:

²⁶⁶Efficiency Vermont Technical Reference Manual 12.31.2018, Page 47;

https://puc.vermont.gov/sites/psbnew/files/doc_library/Vermont%20TRM%20Savings%20Verification%202018%20Version_FIN_ AL.pdf

267 Lawrence Berkeley National Laboratory. A Meta-Analysis of Energy Savings from Lighting Controls in Commercial Buildings.

Page & Associates Inc. 2011.

http://eetd.lbl.gov/publications/meta-analysis-energy-savings-lighting-controls-commercial-buildings.

LBNL's meta study of energy savings from lighting controls in commercial buildings bases its savings analysis on over 240 actual field installations. The report found that savings are over-represented and do not filter for external factors such as building orientation, location, use, weather, blinds, commissioning, changes in behavior after controls are set, etc. As such, their value of 24% represented the best conservative estimate of occupancy controls energy savings achievable in the field today. ²⁶⁸ Negative value because this is an increase in heating consumption due to the efficient lighting.

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 IF_{kWh}

= Lighting-HVAC Interaction Factor for electric heating impacts; this factor represents the increased electric space heating requirements due to the reduction of waste heat rejected by the efficient lighting. Values are provided in the Lighting Reference Table 2.6.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 Δ kWh = As calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor.

= 0.0001899635 for indoor lighting = 0.0001379439 for Miscellaneous = 0.000056160 for exterior lighting

Natural Gas Energy Savings

If gas heated building (or unknown):

 $\Delta Therms = kW_{controlled} * Hours * ESF * (-IF_{therms})$

Where:

 $IF_{Therms} \\$

= Lighting-HVAC Integration Factor for gas heating impacts; this factor represents the increased gas space heating requirements due to the reduction of waste heat rejected by the efficient lighting and is provided in the Lighting Reference Table in Section 2.6 by Building Type.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.6.11 Street Lighting

DESCRIPTION

This measure characterizes the savings associated with LED street lighting conversions where a LED fixture replaces a high-intensity discharge (HID) outdoor lighting system, including metal halide, high pressure sodium, and mercury vapor. LED street lights provide considerable benefits compared to HID lights, including:

- Improved nighttime visibility and safety through better color rendering, more uniform light distribution and elimination of dark areas between poles.
- Reduced direct and reflected uplight which are the primary causes of urban sky glow.
- 40-80% energy savings (dependent on incumbent lighting source).
- 50-75% street lighting maintenance savings.²⁶⁹

This measure includes LED fixture housings including cobrahead and post-top and is applicable only where utility tariffs support LED street lighting conversions.

This measure was developed to be applicable for a one-to-one RF opportunity only.²⁷⁰

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment must be an LED fixture that meets the United Illuminating Rate Schedule, alongside all other luminary performance requirements, based on site characteristics²⁷¹ and all local, state and federal codes.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is the existing lighting system – a metal halide, high pressure sodium, or mercury vapor outdoor lamp, ballast, and fixture.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The measure life is assumed to be 12.5 years.²⁷²

DEEMED MEASURE COST

²⁶⁹ See NEEP "LED Street Lighting Assessment and Strategies for the Northeast and Mid-Atlantic," January 2015, and the Municipal Solid State Street Lighting Consortium for more information http://www1.eere.energy.gov/buildings/ssl/consortium.html
²⁷⁰ Many light fixtures were placed in service 20-50 years ago and may no longer service their intended purpose. It is important to

Many light intuities were placed in service 20-30 years ago and may no tonget service their linetacet purpose. It is important to conduct a comprehensive assessment of lighting needs with a lighting professional when considering a LED street lighting project. LED street lighting can result in removal of lighting altogether as LED lights provide better CRI and lighting levels than existing HID lighting types. While this measure only characterizes a one-to-one replacement value, it is recommended that this measure be updated following a Missouri assessment to see where LED street lighting has resulted in the removal of street lighting to ensure additional savings calculations are captured. Recommend using Street and Parking Facility Lighting Retrofit Financial Analysis Tool developed by DOE Municipal Solid-State Street Lighting Consortium and the Federal Energy Management Program.

271 See DOE Municipal Solid-State Street Lighting Consortium "Model Specifications for LED Roadway Luminaires v.2.0," July 2014.

²⁷² The measure lifetime is calculated using 4,000 annual hours of use from Ameren Missouri "Light Emitting Diode (LED) Street and Area Lighting Report," July 2013 and a typical LED streetlight lifetime of 50,000 hours from Massachusetts Department of Energy Resources "LED Streetlights: What is Your Plan? (webinar)," September 11, 2013.

Actual measure installation cost should be used, including material and labor.²⁷³ If the actual cost of the LED unit is unknown, use the default values for typical LED streetlight retrofits provided below.274

Light output						
Low (<50W) Med (50W-100W) High (>100W)						
Fixture Type	min	max	min	max	min	max
Decorative/Post Top	\$350.00	\$615.00	\$550.00	\$950.00	\$750.00	\$1,450.00
Cobrahead	\$99.00	\$225.00	\$179.00	\$451.00	\$310.00	\$720.00

LOADSHAPE

Ext Lighting BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS²⁷⁵

$$\Delta kWh = \frac{Watts_{Base} - Watts_{EE}}{1000} * Hours$$

Where:

WattsBase = Actual wattage if known, if unknown assume the following

nominal wattage based on technology²⁷⁶

Metal Halide = 554W

High Pressure Sodium = 157W

Mercury Vapor = 228W

= Actual wattage²⁷⁷ Wattsee

= Annual operating hours Hours

 $=4,000 \text{ hours}^{278}$

SUMMER COINCIDENT PEAK DEMAND SAVINGS

No summer peak savings should be claimed for street lighting, as street lights are not expected to be operational during system peak loads.

Labor. Should include the removal of the old fixture and installation of the new fixture. Assume the typical prevailing wage as per the Annual Wage Order No. 23 published by the Missouri Department of Labor.

274 LED unit costs from New York State Energy Research and Development Authority "Street Lighting in New York State: Opportunities and Challenges," Revised January 2015.

275 There is no ISR input Savines are not unit. ²⁷³ Labor should include the removal of the old fixture and installation of the new fixture. Assume the typical prevailing wage as per

There is no ISR input. Savings are per unit.

²⁷⁶ Baseline wattages are a weighted average of products evaluated in Ameren Missouri "Light Emitting Diode (LED) Street and Area Lighting Report," July 2013. See "Street Lighting Baseline Wattages.xlsx."

²⁷⁷ It is important to ensure that retrofit opportunities base efficient wattage on a lumen per watt equivalence.

²⁷⁸ Ameren Missouri "Light Emitting Diode (LED) Street and Area Lighting Report," July 2013.

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

Annual O&M savings are estimated at \$50/LED streetlight.²⁷⁹

MEASURE CODE:

 $^{^{279}}$ New York State Energy Research and Development Authority "Street Lighting in New York State: Opportunities and Challenges," Revised January 2015.

2.7 Miscellaneous

2.7.1 Laptop Computer

DESCRIPTION

This measure estimates savings for a laptop (or notebook) computer with that has been certified by ENERGY STAR® (ES) Version 6.0.

This measure was developed to be applicable to the following program type: TOS. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient product is laptop meeting the requirements set forth by ENERGY STAR® Version 6.0

DEFINITION OF BASELINE EQUIPMENT

Non ENERGY STAR® qualified laptop.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The life of this measure is 4 years.²⁸⁰

DEEMED MEASURE COST²⁸¹

The incremental cost is \$5.

LOADSHAPE

Miscellaneous BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS²⁸²

Where:

Hours_{idle} = Annual hours the computer is on and idling. Custom input or based on usage pattern (see table below).

 $^{^{280}}$ Based on Energy $\operatorname{Star}^{\text{\tiny{\$}}}$ Office Equipment Calculator. See "Office Equipment Calculator.xlsx."

²⁸¹ Computer CASE Report, CA IOUs. <a href="http://www.energy.ca.gov/appliances/2013rulemaking/documents/proposals/12-AAER-2A Consumer Electronics/California IOUs Standards Proposal Computers UPDATED 2013-08-06 TN-71813. The small incremental cost is in alignment with Energy Star® reporting, which lists an incremental cost of \$0. 280 Based on the algorithms used by the Energy Star® Office Equipment Calculator. See "Office Equipment Calculator.xlsx."</p>

²⁸² Based on the algorithms used by the Energy Star® Office Equipment Calculator. See "Office Equipment Calculator.xlsx."

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P_{idle_base} = Power draw (kW) of baseline unit while idling. Based on computer

performance level (see table below).

 P_{idle_eff} = Power draw (kW) of efficient unit while idling. Based on computer

performance level (see table below).

Hours_{sleep} = Annual hours the computer is in sleep mode. Custom input or based on

usage pattern (see table below).

 $P_{\text{sleep_base}}$ = Power draw (kW) of baseline unit while in sleep mode. Based on

computer performance level (see table below).

P_{sleep_eff} = Power draw (kW) of efficient unit while in sleep mode. Based on

computer performance level (see table below).

Hours_{off} = Annual hours the computer is off. Custom input or based on usage

pattern (see table below).

P_{off_base} = Power draw (kW) of baseline unit while off. Based on computer

performance level (see table below).

P_{off_eff} = Power draw (kW) of efficient unit while off. Based on computer

performance level (see table below).

Table: Default Hours of Use²⁸³

Use Pattern	Hours_idle	Hours_sleep	Hours_off
Turned off at night, sleep enabled	803	1104	6854
Turned off at night, sleep disabled	1906	0	6854
Left on at night, sleep enabled	803	7957	0
Left on at night, sleep disabled	8760	0	0
Unknown	5853	439	2467

Table: Power Requirements^{284&285}

Performance Level ²⁸³	Baseline			Efficient		
	Pidle_base	Psleep_base	Poff_base	Pidle_eff	Psleep_eff	Poff_eff
Low	0.01104	0.00104	0.000563	0.0064	0.000787	0.000382
Medium	0.01482	0.00121	0.000606	0.00861	0.000889	0.000457
High	0.01724	0.00134	0.000619	0.01024	0.00122	0.000522

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 Δ kWh = Energy Savings as calculated above

²⁸³ Based on Energy Star[®] Office Equipment Calculator. See "Office Equipment Calculator.xlsx." "Unknown" based on data suggesting 36% of computers are shut off at night and 8% have sleep mode enabled.

suggesting 36% of computers are shut off at night and 8% have sleep mode enabled.

284 Based on Energy Star® Office Equipment Calculator. See "Office Equipment Calculator.xlsx."

²⁸⁵ "Low" refers to budget or low-end models, "Medium" refers to mid-grade models and "High" refers to high-end models. For more specific performance definitions, refer to Energy Star® 6.0 Requirements.

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CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor = 0.0001379439

NATURAL GAS SAVINGS

N/A

WATER AND OTHER NON-ENERGY IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.7.2 Computer Power Management Software

DESCRIPTION

Computer power management software is installed on a network of computers. This is software which monitors and records computer and monitor usage, as well as allows centralized control of computer power management settings.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment is defined by the requirements listed below:

- Allow centralized control and override of computer power management settings of workstations which include both a computer monitor and CPU (i.e. a desktop or laptop computer on a distributed network).
- Be able to control on/off/sleep states on both the CPU and monitor according to the network administrator-defined schedules and apply power management policies to network groups.
- Have capability to allow networked workstations to be remotely wakened from power-saving mode (e.g. for system maintenance or power/setting adjustments).
- Have capability to detect and monitor power management performance and generate energy savings reports.
- Have capability to produce system reports to confirm the inventory and performance of
 equipment on which the software is installed.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF BASELINE EQUIPMENT

Baseline is defined as a computer network without software enforcing the power management capabilities in existing computers and monitors.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is 4 years.²⁸⁶

DEEMED MEASURE COST

The deemed measure cost is \$29 per networked computer, including labor.²⁸⁷

LOADSHAPE

Miscellaneous BUS

 $^{^{286}}$ Consistent with the expected lifetimes of Energy $\mathrm{Star}^{\text{\tiny{IB}}}$ Office Equipment.

²⁸⁷ Work Paper WPSCNROE0003 Revision 1, Power Management Software for Networked Computers. Southern California Edison

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = kWh_{savings} * N$

Where:

kWh_{savings} = Annual energy savings per workstation

= 200 kWh²⁸⁸ for desktops, 50 kWh for laptops²⁸⁹

= If unknown, assume 161 kWh (based on 74% desktop and 26% laptop)²⁹⁰

= Number of desktop or laptop workstations controlled by the power Ν

management software

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Energy Savings as calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor CF

= 0.0001379439

NATURAL GAS SAVINGS

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

Assumed to be \$2/unit annually.291

MEASURE CODE:

 $^{^{288}}$ Based on average energy savings/computer from the following sources:

South California Edison, Work Paper WPSCNROE0003 (200k Wh)

Surveyor Network Energy Manager Evaluation Report, NEEA (68, 100, and 128kWh)

Regional Technical Forum http://ttf.nwcouncil.org/measures/measure.asp?id=95 (200 kWh)
EnergySTAR* Computer Power Management Savings Calculator (~190 kWh for a mix of laptop/desktop and assuming 30% are already turned off at night) http://www.energystar.gov/ia/products/power_mgt/LowCarbonITSavingsCale.xlsx?78c1-120e&78c1-120e Power Management for Networked Computers: A Review of Utility Incentive Programs J. Michael Walker, Beacon

Consultants Network Inc., 2009 ACEEE Summer Study on Energy Efficiency in Industry (330 kWh).

²⁸⁹ Power Management for Networked Computers: A Review of Utility Incentive Programs J. Michael Walker, Beacon Consultants

Network Inc., 2009 ACEEE Summer Study on Energy Efficiency in Industry.

290 Based on PY6 ComEd Computer Software Program data showing a split of 74% desktop to 26% laptop.

291 Based on Dimetrosky, S., Luedtke, J. S., & Seiden, K. (2005). Surveyor Network Energy Manager: Market Progress Evaluation Report, No. 2 (Northwest Energy Efficiency Alliance report #E05-136). Portland, OR: Quantec LLC and review of CLEARResult document providing Qualifying Software Providers for ComEd program and their licensing fees; "Qualifying Vendor Software Comparison.pdf."

2.7.3 Heat Pump Pool Heater

DESCRIPTION

This measure applies to the installation of a heat pump pool heater in place of a standard electric pool heater on an outdoor pool at a commercial location.

This measure was developed to be applicable to the following program type: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new heat pump pool heater meeting program requirements.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new, standard efficiency electric resistance pool heater.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years.²⁹²

DEEMED MEASURE COST

The incremental equipment cost difference between an electric resistance pool heater and a heat pump pool heater is \$1,000 per unit.²⁹³

LOADSHAPE

Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = Q_{PoolHeating} * (1/Eff_{Base} - 1/Eff_{EE})$

Where:

 $Q_{PoolHeating} \\$

= Required annual heat transfer to pool water (kWh), calculated as

follows:²⁹⁴

For an uncovered pool: [53.075 * (SQFT)] + 1631.1

For a pool that is regularly covered when not in use: [8.079 * (SQFT)] +

1295.4

Where SQFT is the total surface area of the pool.

 $^{^{292}}$ Measure life is for a high-efficiency pool heater, from 2017 Michigan Energy Measures Database.

²⁹³ Measure cost based on "The Definitive Guide to Heating Your Swimming Pool," AquaCal, July 2013. Electric resistance pool heaters can be purchased for less than \$2,000, and heat pump pool heaters cost between \$2,000 and \$4,000.

²⁹⁴ Based on the results of a swimming pool energy calculation tool found at http://noanderson.com/services/swimming-pool-energy-temperature-calculator/. Results use St. Louis weather-related assumptions and assume a pool season of May through October (per Energy Star® guidelines), with a water temperature of 80 degrees Fahrenheit.

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Eff_{Base} = Efficiency of electric resistance pool heater

= 100%

Eff_{EE} = Efficiency (COP) of heat pump pool heater

= Actual

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWh * CF$$

Where:

 Δ kWh = Calculated value above.

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001379439

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.7.4 Computer Server

DESCRIPTION

This measure estimates savings for a computer server with that has been certified by ENERGY STAR® (ES) Version 2.0.

This measure was developed to be applicable to the following program type: TOS. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient product is computer server meeting the requirements set forth by ENERGY STAR® Version 2.0.

DEFINITION OF BASELINE EQUIPMENT

Non ENERGY STAR® qualified computer server.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The life of this measure is 4 years.295

DEEMED MEASURE COST²⁹⁶

The incremental cost is \$9.80.

LOADSHAPE

Miscellaneous BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS²⁹⁷

Annual energy savings are based on the rated output of the server's power supply, according to the following table:

²⁹⁵ Consistent with Energy Star[®] computing equipment. It is important to note that lifetime doesn't necessarily reflect the expected functional lifetime of mechanical components, but rather the lifetime of operating system technology, which is generally assumed to become obsolete after a period of four years.

²⁹⁶ Computer CASE Report, CA IOUs. http://www.energy.ca.gov/appliances/2013rulemaking/documents/proposals/12-AAER-2A Consumer Electronics/California IOUs Standards Proposal Computers UPDATED 2013-08-06 TN-71813. The small incremental cost is in alignment with Energy Star® reporting, which lists an incremental cost of \$0 for all office equipment. ²⁹⁷ Based on current Energy Star® qualified product performance and assumptions drawn from the Energy Savings From Energy Star®-Qualified Servers report and Energy Star® Computer Specifications version 4.0. See "Computer Server Savings.xlsx" for additional details and methodology.

Power Supply Rated Output (W)	Baseline Annual Energy Consumption (kWh)	Efficient Annual Energy Consumption (kWh)	Annual Energy Savings (kWh)
Up to 500	1,221	742	479
501-1000	3,024	1,837	1,187
1001-1500	5,883	3,575	2,308
1501-2000	9,152	5,561	3,591
2001-2500	8,667	5,266	3,401
2501-3000	19,633	11,929	7,704

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Energy Savings as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001379439

NATURAL GAS SAVINGS

N/A

WATER AND OTHER NON-ENERGY IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.8 Motors

2.8.1 Motors

DESCRIPTION

This measure applies to the one-for-one replacement of an old, working or failed/near failure 1-350 horsepower, constant speed, uniformly loaded HVAC fan or pumping motor with a new motor of the same rated horsepower that meets or exceeds National Electrical Manufacturers Association (NEMA) Premium efficiency levels.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new motor that meets or exceeds NEMA Premium efficiency levels.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment efficiency is the efficiency of the existing motor, or if unknown, the federal minimum required efficiency is assumed.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years.²⁹⁸

DEEMED MEASURE COST

Actual incremental costs should be used if available. If actual costs are unknown, use default installed cost from table below.²⁹⁹

Motor Size (HP)	Installed Cost
1	\$730
1.5	\$725
2	\$800
3	\$840
5	\$860
7.5	\$1,165
10	\$1,298
15	\$2,242
20	\$2,522
25	\$2,873
30	\$3,095
40	\$3,716
50	\$4,073
60	\$5,128

²⁹⁸ California Database for Energy Efficiency Resources (DEER) 2014 Estimated Useful Life (EUL) Table Update.

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²⁹⁹ Installed costs from 2015-2016 Demand-Side Management Plan, Xcel Energy.

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Motor Size (HP)	Installed Cost
75	\$5,888
100	\$7,392
125	\$9,076
150	\$9,401
200	\$11,250
250	\$13,958
300	\$17,744
350	\$25,653

LOADSHAPE

Motors BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = HP^* LF * 0.746 * (1/\eta_{Bmotor} - 1/\eta_{EEmotor})* Hours$$

Where:

HP = Nominal horsepower (HP) of new motor

= Actual

LF = Load Factor; Motor Load at Fan/Pump Design CFM

 $=75\%^{300}$

0.746 = Conversion factor from HP to kWh

 η_{Bmotor} = Actual efficiency of existing motor, or if unknown, use federal baseline

nominal/nameplate motor efficiency as shown in table below.

 $\eta_{EEmotor}$ = Efficient motor nominal/nameplate motor efficiency

= Actual

Hours = Annual hours of operation for motor; see table below for HVAC

motors

³⁰⁰ Motor efficiency curves typically result in motors being most efficient at approximately 75% of the rated load. Determining Electric Motor Load and Efficiency, US DOE Motor Challenge, a program of the US Department of Energy, https://energy.gov/sites/prod/files/2014/04/f15/10097517.pdf.

Open Drip Proof (ODP) and Totally Enclosed Fan Cooled (TEFC)301

	Open	Drip Proof (O of Poles	DP) #	Totally End	closed Fan-Coo # of Poles	oled (TEFC)
Motor Size	6	4	2	6	4	2
(HP)		Speed (RPM)			Speed (RPM)	
	1200	1800	3600	1200	1800	3600
1	82.50%	85.50%	77.00%	82.50%	85.50%	77.00%
1.5	86.50%	86.50%	84.00%	87.50%	86.50%	84.00%
2	87.50%	86.50%	85.50%	88.50%	86.50%	85.50%
3	88.50%	89.50%	85.50%	89.50%	89.50%	86.50%
5	89.50%	89.50%	86.50%	89.50%	89.50%	88.50%
7.5	90.20%	91.00%	88.50%	91.00%	91.70%	89.50%
10	91.70%	91.70%	89.50%	91.00%	91.70%	90.20%
15	91.70%	93.00%	90.20%	91.70%	92.40%	91.00%
20	92.40%	93.00%	91.00%	91.70%	93.00%	91.00%
25	93.00%	93.60%	91.70%	93.00%	93.60%	91.70%
30	93.60%	94.10%	91.70%	93.00%	93.60%	91.70%
40	94.10%	94.10%	92.40%	94.10%	94.10%	92.40%
50	94.10%	94.50%	93.00%	94.10%	94.50%	93.00%
60	94.50%	95.00%	93.60%	94.50%	95.00%	93.60%
75	94.50%	95.00%	93.60%	94.50%	95.40%	93.60%
100	95.00%	95.40%	93.60%	95.00%	95.40%	94.10%
125	95.00%	95.40%	94.10%	95.00%	95.40%	95.00%
150	95.40%	95.80%	94.10%	95.80%	95.80%	95.00%
200	95.40%	95.80%	95.00%	95.80%	96.20%	95.40%
250	95.40%	95.80%	95.00%	95.80%	96.20%	95.80%
300	95.40%	95.80%	95.40%	95.80%	96.20%	95.80%
350	95.40%	95.80%	95.40%	95.80%	96.20%	95.80%
					•	

 $^{^{301}}$ For 1-200 HP motors, baseline efficiency is from NEMA MG 1 Table 12-12. For motors over 200 hp, baseline efficiency is from NEMA MG 1 Table 12-11.

Annual Hours of Use for HVAC Motors³⁰²

Building Type	Hot Water Pump Hours	Chilled Water Pump Hours	Fan Motor Run Hours
Large Office	5,233	6,385	6,753
Medium Office	3,437	5,921	6,968
Small Office	3,715	3,774	6,626
Warehouse	4,587	1,292	6,263
Stand-alone Retail	4,040	2,713	6,679
Strip Mall	3,908	2,548	6,687
Primary School	4,754	5,160	5,906
Secondary School	5,594	5,279	6,702
Supermarket	4,868	4,255	6,900
Quick Service Restaurant	4,231	3,378	7,679
Full Service Restaurant	4,595	4,897	7,664
Hospital	8,760	8,717	8,760
Outpatient Health Care	8,760	8,689	8,760
Small Hotel - Building	3,533	7,976	8,760
Large Hotel - Building	5,538	8,308	8,760
Midrise Apartment - Building	5,197	4,347	8,728
Nonresidential Average	4,411	3,539	6,773

SUMMER COINCIDENT PEAK DEMAND SAVINGS303

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Energy Savings as calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001379439

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

³⁰² Hours per year are estimated using the eQuest models as the total number of hours the heating or cooling system is operating for each Building Type. "Heating and Cooling Run Hours" are estimated as the total number of hours fans are operating for heating, cooling and ventilation for each Building Type. This may over claim certain applications (e.g. pumps) and so where possible actual hours should be used for these applications.

³⁰³ Since savings will be constant and without fluctuation over the period of operation, demand savings are simply the energy

³⁰³ Since savings will be constant and without fluctuation over the period of operation, demand savings are simply the energy savings divided by the hours of operation. Demand savings are expected to coincide with peak demand period definitions, consistent with assumptions in VFD measures on HVAC pumps and fans.

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.8.2 Pool Pump

DESCRIPTION

This measure applies to the installation of a variable frequency drive (VFD) on an existing single-speed pool pump at a commercial location. VFDs save energy by reducing the speed of the pool pump motor to match the pool's required flow rate. Additionally, VFD's soft-starting extends motor life by reducing wear.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new VFD meeting program requirements.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is an existing, single-speed pool pump without a VFD or other motor control device.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 10 years.304

DEEMED MEASURE COST

Actual costs (equipment and labor) should be used if available. If actual costs are unknown, assume equipment costs of \$200/motor horsepower and labor cost of \$46.305

LOADSHAPE

Motors BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = 1,747 * HP$

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³⁰⁴ EUL set to 10 years based on 2021 comparison with other TRM values; Database for Energy Efficient Resources (2014). http://www.deeresources.com/.

³⁰⁵ Costs from 2017 Michigan Energy Measures Database.

Where:

= Average annual energy savings per pool pump motor horsepower (kWh/HP) $^{306}\,$ 1,747

= Pool pump motor horsepower HP

= Custom input, actual horsepower rating of the pump motor.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

kWh = Electric energy savings, as calculated above.

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001379439

NATURAL GAS ENERGY SAVINGS

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

 306 Energy savings based on monitoring performed at commercial pool facilities, from "Commercial Variable Speed Pool Pump Market Characterization and Metering Study," Southern California Edison, February 2015.

2.8.3 Pool Pump Timer

DESCRIPTION

This measure applies to the installation of a pump timer on an existing single-speed pool pump at a commercial location. Many times, it is not necessary to run a pool's circulation pump 24 hours a day.

This measure was developed to be applicable to the following program type: RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new pump timer meeting program requirements.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is an existing, single-speed pool pump without a VFD or other motor control device.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 10 years.

DEEMED MEASURE COST

Actual costs (equipment and labor) should be used if available. If actual costs are unknown, assume equipment costs of \$100.307

LOADSHAPE

Motors BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = HRS * HP * .746$

Where:

HRS = Hours Timer will shut off pump annually

= Actual.

HP = Pool pump motor horsepower

= Custom input, actual horsepower rating of the pump motor.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

³⁰⁷ Costs from Ameren Missouri MEEIA 2016-18 TRM.

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 $\Delta kW = \Delta kWh * CF$

Where:

kWh

= Electric energy savings, as calculated above. = Summer peak coincidence demand (kW) to annual energy (kWh) factor CF

= 0.0001379439

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

2.8.4 Pump Optimization

DESCRIPTION

Pump improvements can be done to optimize the design and control of centrifugal water pumping systems, including water solutions with freeze protection up to 15% concentration by volume. Other fluid and gas pumps cannot use this measure calculation. The measurement of energy and demand savings for commercial and industrial applications will vary with the type of pumping technology, operating hours, efficiency, and existing and proposed controls. Depending on the specific application slowing the pump, trimming or replacing the impeller may be suitable options for improving pumping efficiency. Pumps up to 40 HP are allowed to use this energy savings calculation. Larger motors should use a custom calculation (which may result in larger savings than this measure would claim).

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is proven to be an optimized centrifugal pumping system meeting the applicable program efficiency requirements:

- Pump balancing valves no more than 15% throttled; and
- Balancing valves on at least one load 100% open.

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline equipment is assumed to be the existing pumping system including existing controls and sequence of operations.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 10 years.³⁰⁸

DEEMED MEASURE COST

The incremental capital cost for this measure can vary considerably depending upon the strategy employed to achieve the required efficiency levels and should be determined on a site-specific basis.

LOADSHAPE

Process BUS

Algorithm

CALCULATION OF SAVINGS

³⁰⁸ Martin, N. et al., Emerging Energy-Efficient Industrial Technologies: New York State Edition, American Council for an Energy Efficient Economy (ACEEE), March 2001 (as stated in the OH State TRM, page 269).

ELECTRIC ENERGY SAVINGS

$$\Delta kWh = (HP_{motor} * 0.746 * LF / \eta_{motor}) * HOURS * ESF$$

Where:

 $HP_{motor} \\$ = Installed nameplate motor horsepower

= Actual

0.746 = Conversion factor from horsepower to kW (kW/hp)

 $LF \ / \ \eta_{motor}$ = Combined as a single factor since efficiency is a function of load

LF = Load Factor; Ratio of the peak running load to the nameplate rating of

= Motor efficiency at pump operating conditions η_{motor}

HOURS = Annual operating hours of the pump

=Actual

ESF = Energy Savings Factor; assume a value of 15%.310

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

CF = Summer Coincident Peak Factor for measure

 $= 0.0001379439^{311}$

NATURAL GAS ENERGY SAVINGS

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

^{309 &}quot;Measured Loading of Energy Efficient Motors - the Missing Link in Engineering Estimates of Savings," ACEEE 1994 Summer Study Conference, Asilomar, CA.

³¹⁰ Published estimates of typical pumping efficiency improvements range from 5 to 40%. For analysis purposes, assume 15%. United States Industrial Electric Motor Systems Market Opportunities Assessment December 2002, Table E-7, Page 18, https://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/mtrmkt.pdf.

311 Based on Ameren Missouri 2016 Process Loadshape.

2.8.5 Variable Frequency Drives for Pumps and Fans on Hydronic HVAC Systems

DESCRIPTION

This measure applies to VFDs installed on HVAC chilled water distribution pumps, hot water distribution pumps, condenser water pumps and cooling tower fans. Back-up pumps/fans do not qualify for this measure. There is a separate measure for HVAC supply and return fans. The VFD will modulate the speed of the motor when it does not need to run at full load. Since the power of the motor is proportional to the cube of the speed for these types of applications, significant energy savings will result.

This measure was developed to be applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The VFD is applied to a pump or fan motor that does not have a VFD. The hydronic system that the VFD is applied to must have a variable or reduced load. Installation is to include the necessary control points and parameters (example: differential pressure, differential temperature, return water temperature) as determined by a qualified engineer.

DEFINITION OF BASELINE EQUIPMENT

The time of sale baseline is a new motor installed without a VFD or other methods of control. Retrofit baseline is an existing motor operating as is.

Installations of new equipment with VFDs which are required by regional code adoption should not claim savings.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life for HVAC application is 15 years.312

DEEMED MEASURE COST

Customer-provided costs will be used when available. Default measure costs are listed below for 1 to 75 HP motors.³¹³ The average of the values below is \$179/HP.

HP	Cost
1-9 HP	\$1,874
10-19 HP	\$2,967
20-29 HP	\$4,060
30-39 HP	\$5,154
40-49 HP	\$6,247
50-59 HP	\$7,340
60-69 HP	\$8,433

 $^{^{\}rm 312}$ Consistent with Ameren Missouri program assumptions.

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³¹³ Average costs observed by other Midwestern states energy efficiency programs – specific data reflects results from Iowa program costs.

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70-75 HP	\$9,526
>75 HP	\$179/HP

LOADSHAPE

Cooling BUS Heating BUS HVAC BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = BHP / EFFi * Hours * ESF$

Where:

BHP = System Brake Horsepower

= Nominal motor HP * Motor load factor)

Motors are assumed to have a load factor of 65% for calculating kW if actual values cannot be determined.³¹⁴ Custom load factor may be

applied if known.

EFFi = Motor efficiency, installed. Actual motor efficiency shall be used to

calculate kW. If not known, a default value of 93% is an appropriate

assumption.

Hours = Default hours are provided for HVAC applications which vary by

HVAC application and Building Type.³¹⁵ When available, actual hours

should be used.

ESF = Energy savings factor varies by VFD application. Units are kW/HP.

³¹⁴ Del Balso, Ryan J. "Investigation into the Reliability of Energy Efficiency/Demand Side Management Savings Estimates for Variable Frequency Drives in Commercial Applications," University of Colorado, Department of Civil, Environmental and Architectural Engineering, 2013.

³¹⁵ Hours per year are estimated using the eQuest models as the total number of hours the heating or cooling system is operating for each Building Type. "Heating and Cooling Run Hours" are estimated as the total number of hours fans are operating for heating, cooling and ventilation for each Building Type. This may over claim certain applications (e.g. pumps) and so where possible actual hours should be used for these applications.

Annual Hours of Use for VFD Pumps and Fans

Building Type	Heating Run Hours	Cooling Run Hours
Large Office	5233	6385
Medium Office	3437	5921
Small Office	3715	3774
Warehouse	4587	1292
Stand-alone Retail	4040	2713
Strip Mall	3908	2548
Primary School	4754	5160
Secondary School	5594	5279
Supermarket	4868	4255
Quick Service Restaurant	4231	3378
Full Service Restaurant	4595	4897
Hospital	8760	8717
Outpatient Health Care	8760	8689
Small Hotel - Building	3533	7976
Large Hotel - Building	5538	8308
Midrise Apartment - Building	5197	4347
Nonresidential Average	4411	3539

ESF for VFD Pumps and Fans

Application	ESF ³¹⁶
Hot Water Pump	0.3577
Cooling Water Pump	0.3389
Cooling Tower Fan	0.126^{317}

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 $\Delta kWh \\$ = Energy Savings as calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.000910684 Cooling Water Pumps = 0.000443983 Hot Water Pumps = 0.000443983 Cooling Tower Fans

FOSSIL FUEL IMPACT DESCRIPTIONS AND CALCULATION

316 Developed from datasets produced from the Northeast Energy Efficiency Partnerships Variable Speed Drive Loadshape Project.
 See supporting workbook "VSD HVAC Pump Savings.xlsx" for derivation.
 317 Based on the methodology described in the Illinois Statewide TRM for Energy Efficiency, 7th Edition (2019).

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If fossil fuel impacts are expected, a custom analysis should be used to support them.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.8.6 Variable Frequency Drives for HVAC Supply and Return Fans

DESCRIPTION

This measure applies to VFDs installed on HVAC supply fans and return fan. Back-up fans do not qualify for this measure. There is a separate measure for HVAC Pumps. The VFD will modulate the speed of the motor when it does not need to run at full load. Since the power of the motor is proportional to the cube of the speed for these types of applications, significant energy savings will result.

This measure is applicable to the following program types: TOS and RF. If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The VFD is applied to an HVAC fan motor that does not have a VFD. The air distribution system must have a variable or reduced load, and installation is to include the necessary control point as determined by a qualified engineer (example: differential pressure, temperature, or volume). Savings are based on the application of VFDs to a range of baseline system conditions, including no control, inlet guide vanes, outlet guide vanes, relief dampers, and throttling valves.

DEFINITION OF BASELINE EQUIPMENT

The TOS baseline is a new motor installed without a VFD or other methods of control. The RF baseline is an existing motor operating as is. RF baselines may or may not include guide vanes, throttling valves, or other methods of control.

Installations of new equipment with VFDs which are required by regional code adoption should not claim savings.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life for HVAC application is 15 years.³¹⁸

DEEMED MEASURE COST

Customer provided costs will be used when available. Default measure costs are listed below for up to 100 hp motors.³¹⁹ The average of the values below is \$168/HP.

HP	Cost
1-9 HP	\$1,874
10-19 HP	\$2,967
20-29 HP	\$4,060
30-39 HP	\$5,154
40-49 HP	\$6,247
50-59 HP	\$7,340
60-69 HP	\$8,433
70-79 HP	\$9,526
80-89 HP	\$10,620

³¹⁸ Consistent with Ameren Missouri program assumptions.

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³¹⁹ Average costs observed by energy efficiency programs in Iowa.

90-100 HP	\$11,713
>100 HP	\$168/HP

LOADSHAPE

HVAC BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS320

 $\Delta kWh_{fan} = kWh_{Base} - kWh_{Retrofit}$

 $\Delta kWh_{total} = \Delta kWh_{fan}*(1 + IE_{energy})$

$$kWh_{Base} = 0.746*HP*\frac{LF}{\eta_{moto}})*RHRS_{base} \sum\nolimits_{0.0\%}^{100\%} \left(\%FF*PLR_{Retrofit}\right)$$

$$kWh_{Retrofit} = 0.746*HP* \frac{\mathit{LF}}{\eta_{moto}})*RHRS_{base} \sum\nolimits_{30\%}^{100\%} \left(\%FF*PLR_{Retrofit}\right)$$

Where:

 ΔkWh_{fan} = Fan-only annual energy savings ΔkWh_{total} = Total project annual energy savings

 kWh_{Base} = Baseline annual energy consumption (kWh/yr) $kWh_{Retrofit}$ = Retrofit annual energy consumption (kWh/yr)

0.746 = Conversion factor for HP to kWh HP = Nominal horsepower of controlled motor

= Load Factor; Motor Load at Fan Design CFM (Default = 65%)³²¹ LF

= Installed nominal/nameplate motor efficiency ηmotor

> = Actual. If unknown, default can be assumed as a NEMA Premium Efficiency, ODP, 4-pole/1800 RPM fan motor, with efficiency indicated in

the table below.

 $RHRS_{Base}$ = Annual operating hours for fan motor based on Building Type.

%FF = Percent of time at flow fraction

 $PLR_{Base} \\$ = Part load ratio for a given flow fraction range based on the baseline flow

control type (see table below)

= Part load ratio for a given flow fraction range based on the retrofit flow $PLR_{Retrofit} \\$

control type (see table below)

³²⁰ Methodology developed and tested in Del Balso, Ryan Joseph. "Investigation into the Reliability of Energy Efficiency/Demand Side Management Savings Estimates for Variable Frequency Drives in Commercial Applications." A project report submitted to the Faculty of the Graduate School of the University of Colorado, 2013.

³²¹ Lawrence Berkeley National Laboratory, and Resource Dynamics Corporation. (2008). "Improving Motor and Drive System Performance; A Sourcebook for Industry," U.S. Department of Energy, Office of Energy Efficiency and Renewable Energy, Golden, CO: National Renewable Energy Laboratory.

Eenergy

= HVAC interactive effects factor for energy (default = 15.7%)³²²

³²² Del Balso, Ryan Joseph. "Investigation into the Reliability of Energy Efficiency/Demand Side Management Savings Estimates for Variable Frequency Drives in Commercial Applications." A project report submitted to the Faculty of the Graduate School of the University of Colorado, 2013.

NEMA Premium Efficiency Motors Default Efficiencies³²³

	Open Drip Proof (ODP)			Totally E	Totally Enclosed Fan-Cooled (TEFC)			
	# of Poles				# of Poles			
Size HP	6	4	2	6	4	2		
SIZC III	Speed (RPM)				Speed (RPM)			
	1200	1800 Default	3600	1200	1800	3600		
1	0.825	0.855	0.770	0.825	0.855	0.770		
1.5	0.865	0.865	0.840	0.875	0.865	0.840		
2	0.875	0.865	0.855	0.885	0.865	0.855		
3	0.885	0.895	0.855	0.895	0.895	0.865		
5	0.895	0.895	0.865	0.895	0.895	0.885		
7.5	0.902	0.910	0.885	0.910	0.917	0.895		
10	0.917	0.917	0.895	0.910	0.917	0.902		
15	0.917	0.930	0.902	0.917	0.924	0.910		
20	0.924	0.930	0.910	0.917	0.930	0.910		
25	0.930	0.936	0.917	0.930	0.936	0.917		
30	0.936	0.941	0.917	0.930	0.936	0.917		
40	0.941	0.941	0.924	0.941	0.941	0.924		
50	0.941	0.945	0.930	0.941	0.945	0.930		
60	0.945	0.950	0.936	0.945	0.950	0.936		
75	0.945	0.950	0.936	0.945	0.954	0.936		
100	0.950	0.954	0.936	0.950	0.954	0.941		
125	0.950	0.954	0.941	0.950	0.954	0.950		
150	0.954	0.958	0.941	0.958	0.958	0.950		
200	0.954	0.958	0.950	0.958	0.962	0.954		
250	0.954	0.958	0.950	0.958	0.962	0.958		
300	0.954	0.958	0.954	0.958	0.962	0.958		
350	0.954	0.958	0.954	0.958	0.962	0.958		
400	0.958	0.958	0.958	0.958	0.962	0.958		
450	0.962	0.962	0.958	0.958	0.962	0.958		
500	0.962	0.962	0.958	0.958	0.962	0.958		

³²³ Douglass, J. (2005). Induction Motor Efficiency Standards. Washington State University and the Northwest Energy Efficiency Alliance, Extension Energy Program, Olympia, WA. Retrieved October 17, 2013, from http://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/motor_efficiency_standards.pdf.

Default hours are provided for HVAC applications which vary by Building Type. 324 When available, actual hours should be used.

Building Type	Total Fan Run Hours
Large Office	6753
Medium Office	6968
Small Office	6626
Warehouse	6263
Stand-alone Retail	6679
Strip Mall	6687
Primary School	5906
Secondary School	6702
Supermarket	6900
Quick Service Restaurant	7679
Full Service Restaurant	7664
Hospital	8760
Outpatient Health Care	8760
Small Hotel - Building	8760
Large Hotel - Building	8760
Midrise Apartment - Building	8728
Nonresidential Average	6773

Flow Fraction (% of design cfm)	Percent of Time at Flow Fraction
0% to 10%	0.0%
10% to 20%	1.0%
20% to 30%	5.5%
30% to 40%	15.5%
40% to 50%	22.0%
50% to 60%	25.0%
60% to 70%	19.0%
70% to 80%	8.5%
80% to 90%	3.0%
90% to 100%	0.5%

³²⁴ Hours per year are estimated using the modeling results and represent the total number of hours the fans are operating for heating, cooling and ventilation for each Building Type.

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Control Type	Flow Fraction									
control 1 ypc	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%
No Control or Bypass Damper	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Discharge Dampers	0.46	0.55	0.63	0.70	0.77	0.83	0.88	0.93	0.97	1.00
Outlet Damper, BI & Airfoil Fans	0.53	0.53	0.57	0.64	0.72	0.80	0.89	0.96	1.02	1.05
Inlet Damper Box	0.56	0.60	0.62	0.64	0.66	0.69	0.74	0.81	0.92	1.07
Inlet Guide Vane, BI & Airfoil Fans	0.53	0.56	0.57	0.59	0.60	0.62	0.67	0.74	0.85	1.00
Inlet Vane Dampers	0.38	0.40	0.42	0.44	0.48	0.53	0.60	0.70	0.83	0.99
Outlet Damper, FC Fans	0.22	0.26	0.30	0.37	0.45	0.54	0.65	0.77	0.91	1.06
Eddy Current Drives	0.17	0.20	0.25	0.32	0.41	0.51	0.63	0.76	0.90	1.04
Inlet Guide Vane, FC Fans	0.21	0.22	0.23	0.26	0.31	0.39	0.49	0.63	0.81	1.04
VFD with duct static pressure controls	0.09	0.10	0.11	0.15	0.20	0.29	0.41	0.57	0.76	1.01
VFD with low/no duct static pressure	0.05	0.06	0.09	0.12	0.18	0.27	0.39	0.55	0.75	1.00

Provided below are the resultant values based upon the defaults provided above:

Control Type	$\overline{\Sigma_{0\%}^{100\%}(\%FF} \times PLR_{Base})$
No Control or Bypass Damper	1.00
Discharge Dampers	0.80
Outlet Damper, BI & Airfoil Fans	0.78
Inlet Damper Box	0.69
Inlet Guide Vane, BI & Airfoil Fans	0.63
Inlet Vane Dampers	0.53
Outlet Damper, FC Fans	0.53
Eddy Current Drives	0.49
Inlet Guide Vane, FC Fans	0.39
VFD with duct static pressure controls	0.30
VFD with low/no duct static pressure	0.27

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kW h_{total} *CF$

Where:

 $\begin{array}{ll} \Delta kWh_{total} & = As \ calculated \ above. \\ CF & = 0.000443983 \end{array}$

NATURAL GAS ENERGY SAVINGS

If fossil fuel impacts are expected, a custom analysis should be used to support them.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

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DEEMED O&M COST ADJUSTMENT CALCULATI	ON	
N/A		
Measure Code:		

Revision 4.0<u>5.0</u>

Ameren Missouri

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2.9 Refrigeration

2.9.1 Commercial Solid and Glass Door Refrigerators & Freezers

DESCRIPTION

This measure applies to ENERGY STAR® vertical closed and horizontal closed refrigerators or freezers installed in a commercial kitchen. ENERGY STAR® commercial refrigerators and freezers are more energy efficient because they are designed with components such as ECM evaporator and condenser fan motors, hot gas anti-sweat heaters, or high-efficiency compressors, which will significantly reduce energy consumption.

This measure was developed to be applicable to the following program type: TOS.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new ENERGY STAR® certified vertical closed or horizontal closed, solid or glass door refrigerator or freezer meeting energy consumptions requirements as determined by door type (solid or glass) and refrigerated volume (V).

ENERGY STAR® Requirements (Version 3.0, Effective October 1, 2014)

Volume (ft³)	Maximum Daily Energy Consumption (kWh/day)				
	Refrigerator	Freezer			
Vertical Closed					
Solid Door					
0 < V < 15	$\leq 0.02V + 1.60$	\leq 0.25V + 1.55			
$15 \le V < 30$	\leq 0.09V + 0.55	\leq 0.20V + 2.30			
$30 \le V < 50$	\leq 0.01V + 2.95	\leq 0.25V + 0.80			
$V \ge 50$	$\leq 0.06V + 0.45$	\leq 0.14V + 6.30			
Glass Door					
0 < V < 15	\leq 0.10V + 1.07	\leq 0.56V + 1.61			
$15 \le V < 30$	\leq 0.15V + 0.32	\leq 0.30V + 5.50			
$30 \le V < 50$	$\leq 0.06V + 3.02$	$\leq 0.55V - 2.00$			
V ≥ 50	$\leq 0.08V + 2.02$	\leq 0.32V + 9.49			
Horizontal Closed					
Solid or Glass Doors					
All Volumes	$\leq 0.06V + 0.60$	\leq 0.10V + 0.20			

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new vertical closed or horizontal closed, solid or glass door refrigerator or freezer that is not ENERGY $STAR^{*}$ certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

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The expected measure life is assumed to be 12 years.325

DEEMED MEASURE COST

The incremental capital cost for this measure varies by size as shown in the table below:

Measure	Incremental Cost
Commercial Glass Door Freezers less than 15 ft ³	\$220
Commercial Glass Door Freezers 15 to 30 ft ³	\$950
Commercial Glass Door Freezers 30 to 50 ft ³	\$1,307
Commercial Glass Door Freezers more than 50 ft ³	\$2,300
Commercial Glass Door Refrigerators less than 15 ft ³	\$250
Commercial Glass Door Refrigerators 15 to 30 ft ³	\$500
Commercial Glass Door Refrigerators 30 to 50 ft ³	\$1,307
Commercial Glass Door Refrigerators more than 50 ft ³	\$2,300
Commercial Solid Door Freezers/Refrigerators less than 15 ft ³	\$150
Commercial Solid Door Freezers/Refrigerators 15 to 30 ft ³	\$400
Commercial Solid Door Freezers/Refrigerators 30 to 50 ft ³	\$550
Commercial Solid Door Freezers/Refrigerators more than 50 ft ³	\$700
Horizontal Closed - Solid or Glass Door Refrigerator (all volumes)	\$525
Horizontal Closed - Solid or Glass Door Freezer (all volumes	\$595

LOADSHAPE

Refrigeration BUS

Algorithm

CALCULATION OF SAVINGS

ELECTRIC ENERGY SAVINGS

Custom calculation below.326

 $\Delta kWh = (kWh_{Base} - kWh_{ESTAR}) * Days$

Where:

 kWh_{Base}

= Maximum daily energy consumption (kWh/day) of baseline

refrigerator or freezer

= Calculated as shown in the table below using the actual refrigerated volume (V)

 $^{^{325}}$ Measure life from ENERGY STAR® Commercial Kitchen Equipment Savings Calculator which cites reference as "FSTC research on available models, 2009."

https://www.energystar.gov/sites/default/files/asset/document/commercial_kitchen_equipment_calculator%2003-15-2016.xlsx.

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kWh_{ESTAR} = Maximum daily energy consumption (kWh/day) of ENERGY STAR®

= Custom or if unknown, calculated as shown in the table below using

the actual refrigerated volume (V)

= Refrigerated volume (ft³) calculated in accordance with the Department

of Energy test procedure in 10 CFR §431.64

= Actual installed

= Days of refrigerator or freezer operation per year Days

= Custom, or if unknown assume 365.25 days per year

Equipment Type	kWhBase ³²⁷
Solid Door Refrigerator	0.10V + 2.04
Glass Door Refrigerator	0.12V + 3.34
Solid Door Freezer	0.40V + 1.38
Glass Door Freezer	0.75V + 4.10

Volume (ft³)	Maximum Daily Energy Consumption (kWh/day)				
	Refrigerator	Freezer			
Vertical Closed					
Solid Door					
0 < V < 15	\leq 0.02V + 1.60	≤ 0.25V + 1.55			
15 ≤ V < 30	\leq 0.09V + 0.55	≤ 0.20V + 2.30			
30 ≤ V < 50	≤ 0.01V + 2.95	≤ 0.25V + 0.80			
V ≥ 50	≤ 0.06V + 0.45	$\leq 0.14V + 6.30$			
Glass Door					
0 < V < 15	≤ 0.10V + 1.07	≤ 0.56V + 1.61			
15 ≤ V < 30	\leq 0.15V + 0.32	\leq 0.30V + 5.50			
30 ≤ V < 50	≤ 0.06V + 3.02	$\leq 0.55V - 2.00$			
V ≥ 50	≤ 0.08V + 2.02	≤ 0.32V + 9.49			
Horizontal Closed					
Solid or Glass Doors					
All Volumes	≤ 0.06V + 0.60	≤ 0.10V + 0.20			

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWh * CF$$

Where:

 $\Delta k W h \\$ = Electric energy savings, calculated above

CF

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001357383^{328}$

^{327 32510} CFR §431.66 - Energy Conservation Standards for Commercial Refrigerators, Freezers and Refrigerator-Freezers. 328 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Refrigeration. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

Ameren	

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NATURAL GAS ENERGY SAVINGS

N/A

PEAK GAS SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

MEASURE CODE:

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2.9.2 Refrigerated Beverage Vending Machine

DESCRIPTION

This measure applies to new ENERGY STAR®, Class A or Class B refrigerated vending machines. ENERGY STAR® vending machines incorporate more efficient compressors, fan motors, and lighting systems as well as a low power mode option that allows the machine to be placed in low-energy lighting and/or low-energy refrigeration states during times of inactivity.

This measure was developed to be applicable to the following program type: TOS.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a new or rebuilt ENERGY STAR $^{\text{®}}$, Class A or Class B 329 refrigerated vending machine meeting energy consumptions requirements as determined by equipment type (Class A or Class B).

ENERGY STAR® Requirements (Version 3.1, Effective March 1, 2013)

Equipment Type	Maximum Daily Energy Consumption (kWh/day)
Class A	$\leq 0.0523V + 2.432$
Class B	$\leq 0.0657V + 2.844$

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a new or rebuilt, Class A or Class B refrigerated vending machine that is not ENERGY $STAR^{\otimes}$ certified.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years. 330

DEEMED MEASURE COST

The incremental cost of this measure is \$140.331

LOADSHAPE

Refrigeration BUS

Algorithm

CALCULATION OF SAVINGS

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³²⁹ Class A means a refrigerated bottled or canned beverage vending machine that is fully cooled, and is not a combination vending machine. Class B means any refrigerated bottled or canned beverage vending machine not considered to be Class A, and is not a combination vending machine. See 10 CFR §431.292 "Definitions concerning refrigerated bottled or canned beverage vending machines."

³³⁰ Average of measure lives recognized by Ameren Missouri (10 years) and KCPL (14 years). Also consistent with Energy Star® commercial refrigerator lifetime.

³³¹ Consistent with Ameren Missouri MEEIA 2016-18 and KCPL TRM assumptions.

ELECTRIC ENERGY SAVINGS

Custom calculation below.

$$\Delta kWh = (kWh_{Base} - kWh_{ESTAR}) * Days$$

Where:

 kWh_{Base} = Maximum daily energy consumption (kWh/day) of baseline

vending machine

= Calculated as shown in the table below using the actual refrigerated

volume (V)

 kWh_{ESTAR} = Maximum daily energy consumption (kWh/day) of ENERGY

STAR® vending machine

= Custom or if unknown, calculated as shown in the table below

using the actual refrigerated volume (V)

V = Refrigerated volume³³² (ft³)

= Actual installed

= Days of vending machine operation per year Days

= 365.25 days per year

Equipment Type	kWhBase 333
Class A	0.055V + 2.56
Class B	0.073V + 3.16

Equipment Type	kWhEE ³³⁴
Class A	≤ 0.0523V + 2.432
Class B	< 0.0657V + 2.844

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

= Electric energy savings, calculated above ΔkWh

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001357383^{335}$

MEASURE CODE:

³³² V is measured by the American National Standards Institute (ANSI)/Association of Home Appliance Manufacturers (AHAM) HRF-1-2004, ``Energy, Performance and Capacity of Household Refrigerators, Refrigerator-Freezers and Freezers.'' Measurement All Capacity of Household Refrigerators and Freezers and Freof refrigerated volume must be in accordance with the methodology specified in Section 5.2, Total Refrigerated Volume (excluding subsections 5.2.2.2 through 5.2.2.4), of ANSI/AHAM HRF-1-2004.

^{333 33010} CFR §431.296 - Energy Conservation Standards for Refrigerated Bottled or Canned Beverage Vending Machines

^{333 2016} CFR 931.296 - Energy Conservation Statistics of the Conference of Cambridge Version 3.1 requirements for maximum daily energy consumption.

335 2016 Ameren Missouri Coincident Peak Demand Factor for Commercial Refrigeration. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf.'

2.9.3 Door Heater Controls for Cooler or Freezer

DESCRIPTION

This measure applies to door heater controls installed on commercial coolers or freezers. There are two main categories of commercially available control strategies that achieve "on-off" control of door heaters based on either (1) the relative humidity of the air in the store or (2) the "conductivity" of the door (which drops when condensation appears). In the first strategy, the system activates door heaters when the relative humidity in a store rises above a specific set point and turns them off when the relative humidity falls below that set point. In the second strategy, the sensor activates the door heaters when the door conductivity falls below a certain set point and turns them off when the conductivity rises above that set point. Savings result from a reduction in electric energy use due to heaters not running continuously and from reduced cooling loads when heaters are off. The assumptions included within this measure assume that door heater controls which are properly designed and commissioned will achieve approximately equivalent savings, regardless of control strategy.

This measure applies to the following program type: RF.

DEFINITION OF EFFICIENT EQUIPMENT

To qualify for this measure, the installed equipment must be a door heater control installed on a commercial glass door cooler or freezer.

DEFINITION OF BASELINE EQUIPMENT

The baseline equipment is a door heater without controls, installed on a commercial glass door cooler or freezer.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 12 years. 336

DEEMED MEASURE COST

Actual incremental costs should be used if available. The incremental capital cost \$151 per door.³³⁷

LOADSHAPE

Refrigeration BUS

Algorithm

CALCULATION OF SAVINGS

336 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, "Effective/Remaining Useful Life Values," California Public Utilities Commission, December 16, 2008.

³³⁷ Ameren Missouri Technical Resource Manual – Effective January 1, 2018.

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ELECTRIC ENERGY SAVINGS

 $\Delta kWh = kW_{Base} * DOORS * (\%ON_{Base} - \%ON_{Control}) * Hours$

Where:

 $kW_{\text{Base}} \\$ = Per door electric energy consumption of door heater without

= Assume 0.130 kW per door³³⁸

DOORS = Number of doors controlled with door heater controls

= Actual or if unknown, use 1 (a per door savings)

 $\%ON_{Base}$ = Effective run time of uncontrolled door heater

= Actual or if unknown, use 90.7%³³⁹

%ON_{Control} = Effective run time with anti-sweat door heater controls

= Actual or if unknown, use 45.6% 339330

Hours = Annual hours of cooler or freezer operation

= Assume 8,766 hours per year

BF = Cooling Bonus factor for reduction in waste heat inside of the

refrigerated space.

= 1.3 for a refrigerator (medium/high temp), 1.5 for freezers (low

temp)340

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh)

factor.

 $= 0.0001357383^{341}$

Savings calculated with default values as defined above.

Door Heater Control Application	ΔkWh/door	ΔkW/door
Refrigerator	668.1	0.0907
Freezer	770.9	0.1046

³³⁸ The Cadmus Group, Commercial Refrigeration Loadshape Project Final Report, Northeast Energy Efficiency Partnerships, Regional Evaluation, Measurement, and Verification Forum, Lexington, MA 2015. Page 75, Table 42.

339 The Cadmus Group, Commercial Refrigeration Loadshape Project Final Report, Northeast Energy Efficiency Partnerships,

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Regional Evaluation, Measurement, and Verification Forum, Lexington, MA 2015. Page 67, Table 37.

340 The Cadmus Group, Commercial Refrigeration Loadshape Project Final Report, Northeast Energy Efficiency Partnerships,

Regional Evaluation, Measurement, and Verification Forum, Lexington, MA 2015. Page 78, Figure 54.

³⁴¹ Ameren Missouri Coincident Peak Demand Factor for Commercial Refrigeration. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf"

Ameren Missouri	Appendix H - TRM – Vol. 2: C&I Measures
NATURAL GAS ENERGY SAVINGS	
N/A	

MEASURE CODE:

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2.9.4 Electronically Commutated Motors (ECM) for Walk-in and Reach-in Coolers/Freezers

DESCRIPTION

This measure consists of replacement of an existing, uncontrolled, and continuously operating standard efficiency shaded-pole evaporator fan motor in refrigerated display cases or fan coil in walk-ins.

This measure achieves savings by installing a more efficient motor, thereby moving the same amount of air with less energy requirements. Additionally, less waste heat is produced, resulting in a decreased refrigeration load.

This measure was developed to be applicable to the following program type: RF.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

This measure applies to the replacement of an existing standard-efficiency shaded-pole evaporator fan motor in refrigerated display cases or fan coil in walk-ins. The replacement unit must be an electronically commutated motor (ECM). Savings assume that efficient motors operate continuously.

DEFINITION OF BASELINE EQUIPMENT

The baseline is the existing shaded-pole motor(s) with no fan control operating 8760 hours continuously in a refrigerated display case or fan coil unit of a walk-in cooling unit.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 15 years.³⁴²

DEEMED MEASURE COST

The measure cost is assumed to be \$177 per motor for a walk in cooler and walk in freezer, including the cost of the motor plus installation.³⁴³

LOADSHAPE

Miscellaneous BUS

Algorithm

CALCULATION OF SAVINGS

Savings are based on a measure created by Energy & Resource Solutions for the California Municipal Utilities Association and supported by PGE workpaper PGE3PREF126. Note that climate differences across all California climate zones resulted in negligible savings differences, which indicates that the average savings for the California study should apply equally as well to

³⁴² DEER database.

³⁴³ Difference in the fully installed cost (\$468) for ECM motor and controller, listed in Work Paper PGE3PREF126, "ECM for Walk-In Evaporator with Fan Controller," June 20, 2012, and the measure cost specified in the DEER database for controller (\$291).

Missouri. Savings found in the aforementioned source are presented in combination with savings from controllers, however for the purposes of this measure only those associated with the ECM upgrade are considered.

ELECTRIC ENERGY SAVINGS

 $\Delta kWh = Savings per motor * motors$

Where:

Savings per motor 344 = based on the motor rating of the ECM motor – see table below.

Motors = number of fan motors replaced

Evaporator Fan Motor Rating (of ECM)	Annual kWh Savings/motor
16W	408
1/15 - 1/20HP	1,064
1/5HP	1,409
1/3HP	1,994
1/2HP	2,558
3/4HP	2,782

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

Where:

 ΔkWh = Electric energy savings, as calculated above.

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

= 0.0001379439

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

³⁴⁴ See reference workbook "ECM Savings.xlsx" for derivation.

2.9.5 Strip Curtain for Walk-in Coolers and Freezers

DESCRIPTION

This commercial measure pertains to the installation of infiltration barriers (strip curtains) on walkin coolers or freezers. Strip curtains impede heat transfer from adjacent warm and humid spaces into walk-ins when the main door is opened, thereby reducing the cooling load. As a result, compressor run time and energy consumption are reduced. The engineering assumption is that the walk-in door is open for varying durations per day based on facility type, and the strip curtain covers the entire door frame. All assumptions are based on values that were determined by direct measurement and monitoring of over 100 walk-in units in the 2006-2008 evaluation for the CA Public Utility Commission.³⁴⁵

This measure was developed to be applicable to the following program type: RF.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

The efficient equipment is a strip curtain added to a walk-in cooler or freezer. The new strip curtain must cover the entire area of the doorway when the door is opened.

DEFINITION OF BASELINE EQUIPMENT

The baseline assumption is a walk-in cooler or freezer that previously had either no strip curtain installed or an old, ineffective strip curtain installed.

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 4 years.³⁴⁶

DEEMED MEASURE COST

The incremental capital cost for this measure is \$10.22/sq ft of door opening.347

LOADSHAPE

Refrigeration BUS

Algorithm

CALCULATION OF SAVINGS

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³⁴⁵ The scale factors have been determined with tracer gas measurements on over 100 walk-in refrigeration units during the California Public Utility Commission's evaluation of the 2006-2008 CA investor owned utility energy efficiency programs. The door-open and close times, and temperatures of the infiltrating and refrigerated airs are taken from short term monitoring of over 100 walk-in units. http://www.calmac.org/publications/ComFac_Evaluation_V1_Final_Report_02-18-2010.pdf.
³⁴⁶ DEER 2014 Effective Useful Life.

³⁴⁷ The reference for incremental cost is \$10.22 per square foot of door opening (includes material and labor). 2008 Database for Energy-Efficiency Resources (DEER), Version 2008.2.05, "Cost Values and Summary Documentation," California Public Utilities Commission, December 16, 2008.

ELECTRIC ENERGY SAVINGS348

 $\Delta kWh = \Delta kWh/SQFT * A$

Where:

 $\Delta kWh/SQFT = Average annual kWh savings per square foot of infiltration barrier.$ Based on application type, as indicated by the table below.349

= Doorway area. Use actual measurements, if unknown use the values in the table below.

Туре	Pre-Existing Curtains	Energy Savings ΔkWh/sq ft
Supermarket - Cooler	Yes	37
Supermarket - Cooler	No	108
Supermarket - Freezer	Yes	119
Supermarket - Freezer	No	349
Convenience Store - Cooler	Yes	5
Convenience Store - Cooler	No	20
Convenience Store - Freezer	Yes	8
Convenience Store - Freezer	No	27
Restaurant - Cooler	Yes	8
Restaurant - Cooler	No	30
Restaurant - Freezer	Yes	34
Restaurant - Freezer	No	119
Refrigerated Warehouse	Yes	254
Refrigerated Warehouse	No	729

Facility Type	Doorway Area (sq ft)
Supermarket - Cooler	35
Supermarket - Freezer	35
Convenience Store - Cooler	21
Convenience Store - Freezer	21
Restaurant - Cooler	21
Restaurant - Freezer	21
Refrigerated Warehouse	80

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWh * CF$

 $^{^{348}}$ The source algorithm from which the savings per square foot values are determined is based on Tamm's equation (an application of Bernoulli's equation) [Kalterveluste durch kuhlraumoffnungen. Tamm W,.Kaltetechnik-Klimatisierung 1966;18;142-144;] and the ASHRAE handbook [American Society of Heating, Refrigeration, and Air-Conditioning Engineers (ASHRAE). 2010. ASHRAE Handbook, Refrigeration: 13.4, 13.6].

349 See reference file "Strip Curtain Savings Calcs.docx" for details on derivation.

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Where:

 ΔkWh = Electric energy savings, calculated above

CF = Summer peak coincidence demand (kW) to annual energy (kWh) factor

 $= 0.0001357383^{350}$

NATURAL GAS ENERGY SAVINGS

N/A

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

^{350 2016} Ameren Missouri Coincident Peak Demand Factor for Commercial Refrigeration. See reference "Ameren Missouri 2016 Appendix E - End Use Shapes and Coincident Factors.pdf."

2.10 Shell

2.10.1 Windows

DESCRIPTION

Energy and demand saving are realized through the installation of windows that offer performance improvements over baseline windows. Savings may be realized from reducing air infiltration, improved insulating properties, and changes to solar heat gain through the glazed surfaces of the building.

This measure was developed to be applicable to the following program types: RF and NC.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to exceed the efficiency requirements defined by the program.

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline is assumed to meet the efficiency requirements set forth by local jurisdictions. In most cases, this will be some version of the IECC. For retrofit applications, the baseline condition is the existing condition and requires assessment of the existing window assemblies.

Local code shall be referenced to define baseline where applicable. As an example, the following is set forth by IECC 2012. An efficient window would have specifications not exceeding these values.

	Climate Zones 4 & 5
U-Factor	
Fixed Windows	0.38 Btu/ft ² .°F.h
Operable Windows	0.45 Btu/ft ² .°F.h
SHGC	0.40

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The expected measure life is assumed to be 20 years.351

DEEMED MEASURE COST

For retrofit projects, full installation costs should be used, including both material and labor costs to install the windows.

In all other scenarios, the incremental cost for this measure is assumed to be \$1.50 per square foot of window area. 352

LOADSHAPE

351 Consistent with window measure lives specified by Ameren Missouri and KCP&L.

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³⁵² Alliance to Save Energy Efficiency Windows Collaborative Report, December 2007. Consistent with other market reports.

Cooling BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS

Electric energy savings is calculated as the sum of energy saved when cooling the building and energy saved when heating the building.

$$\Delta kWh = \Delta kWhcooling + \Delta kWhheating$$

Heating and cooling savings are composed of three components: infiltration, conduction and solar gains. In instances where infiltration savings do not apply or are not eligible, it may be disregarded. If central cooling, the electric energy saved in annual cooling due to the added insulation is:

 $\Delta kWh_{cooling} = Infltration_{cooling} + Conduction_{cooling} + Solar_{cooling}$

 $\begin{aligned} & Infiltration_{Cooling} = (CFM_{PRE} - CFM_{POST})*60*EFLH_{cooling}*\Delta T_{AVG,cooling}*0.018*\\ & LM \ / \ (1000*\eta_{cooling}) \end{aligned}$

Where:

CFM_{PRE} = Infiltration at natural conditions as estimated by blower door testing

before window upgrade

= Actual

CFM_{POST} = Infiltration at natural conditions as estimated by blower door testing after

window upgrade

= Actual

60 = Converts Cubic Feet per Minute to Cubic Feet per Hour

 $EFLH_{cooling} \hspace{0.5cm} = Equivalent \hspace{0.1cm} Full \hspace{0.1cm} Load \hspace{0.1cm} Hours \hspace{0.1cm} for \hspace{0.1cm} Cooling \hspace{0.1cm} [hr] \hspace{0.1cm} are \hspace{0.1cm} provided \hspace{0.1cm} in \hspace{0.1cm} Section \hspace{0.1cm} 2.7,$

HVAC End Use

 $\Delta T_{AVG,cooling}$ = Average temperature difference [^{0}F] during cooling season between

outdoor air temperature and assumed 75°F indoor air temperature – see

table below

0.018 = Specific Heat Capacity of Air (Btu/ft 3 °F)

LM = Latent Multiplier to account for latent cooling demand 353

= 3.0 for St. Louis, MO

1,000 = Conversion from Btu to kBtu

= Seasonal energy efficiency ratio (SEER) of cooling system (kBtu/kWh)

 $\eta_{\text{cooling}} = \text{Actual}$

³⁵³ The Latent Multiplier is used to convert the sensible cooling savings calculated to a value representing sensible and latent cooling loads. The values are derived from the methodology outlined in Infiltration Factor Calculation Methodology by Bruce Harley, Senior Manager, Applied Building Science, CLEAResult 11/18/2015 and is based upon an 8760 analysis of sensible and total heat loads using hourly climate data.

Weather Basis (City based upon)	OA _{AVG,cooling} [°F] ³⁵⁴	ΔT _{AVG,cooling} [°F]
St Louis, MO	80.8	5.8

 $Conduction_{Cooling} = \left(U_{BASE} - U_{EFF}\right) * A_{window} * EFLH_{cooling} * \Delta T_{AVG,cooling} / \left(1000 * \eta_{cooling}\right)$

Where:

U_{BASE} = U-factor value of baseline window assembly (Btu/ft².°F.h)

= Dependent on Weather Basis and window type. See table below for IECC

2012 requirements.

U_{EFF} = U-factor value of the efficient window assembly (Btu/ft².°F.h)

= Actual.

 A_{window} = Area of insulated window (including visible frame and glass) (ft²)

Other variables as defined above.

$$Solar_{Cooling} = \left(SHGC_{BASE} - SHGC_{EFF}\right) * A_{window} * \Psi_{cooling} / \left(1000 * \eta_{cooling}\right)$$

Where:

SHGC_{BASE} = Solar Heat Gain Coefficient of the baseline window assembly

(fractional)

SHGC_{EFF} = Solar Heat Gain Coefficient of the efficient window assembly

(fractional)

= Incident solar radiation during the cooling season (Btu/ft²):355

 $\Psi_{\text{cooling}} = 40,996 \text{ for St. Louis, MO}$

Other variables as defined above.

If the building is heated with electric heat (resistance or heat pump), the electric energy saved in annual heating due to the window upgrade is:

 $\Delta kWh_{heating} = Infltration_{heating} + Conduction_{heating} - Solar_{heating}$

 $Infiltration_{heating} = \left(CFM_{PRE} - CFM_{POST}\right) * 60 * EFLH_{heating} * \Delta T_{AVG,heating} * 0.018 / (3,412 * \eta_{heating})$

Where:

EFLH_{heating} = Equivalent Full Load Hours for Heating [hr] are provided in Section 2.7, HVAC end use

³⁵⁴ National Solar Radiation Data Base -- 1991- 2005 Update: Typical Meteorological Year 3
http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html. Heating Season defined as September 17th through April 13th, cooling season defined as May 20 through August 15th. For cooling season, temperatures from 8AM to 8PM were used to establish average temperatures as this is when cooling systems are expected to be loaded.
355 See "Windows SHG.xlsx" for derivation.

 $\Delta T_{AVG,heating} = Average temperature difference [^0F] during heating season between$

outdoor air temperature and assumed 55°F heating base temperature

3,412 = Conversion from Btu to kWh.

 η_{heating} = Efficiency of heating system

= Actual. Note: electric resistance heating and heat pumps will have an efficiency greater than or equal to 100% Other variables as defined above.

Weather Basis	OAAVG,heating	ΔTAVG,heating
(City based upon)	[°F] ³⁵⁶	[°F]
St Louis, MO	43.2	11.8

Conduction_{heating} = (U_{BASE} - U_{EFF}) * A_{window} * EFLH_{heating} * Δ T_{AVG,heating}/ (3,412 * η _{heating})

Where:

Variables as defined above.

$$Solar_{Heating} = \left(SHGC_{BASE} - SHGC_{EFF}\right) * A_{window} * \Psi_{Heating} / \left(3{,}412 * \eta_{Heating}\right)$$

Where:

$$\Psi_{\text{heating}}$$
 = Incident solar radiation during the heading season (Btu/ft²)
= 66,592 for St. Louis, MO

Other variables as defined above.

SUMMER COINCIDENT PEAK DEMAND SAVINGS

$$\Delta kW = \Delta kWH_{cooling} * CF$$

Where:

 Δ kWH_{cooling} = Annual electricity savings for cooling, as calculated above

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

for Cooling = 0.000910684

NATURAL GAS SAVINGS

CF

If building uses a gas heating system, the savings resulting from the window assembly is calculated with the following formula.

 $\Delta Therms = Infltration_{gasheat} + Conduction_{gasheat} - Solar_{gasheat}$

³⁵⁶ National Solar Radiation Data Base — 1991- 2005 Update: Typical Meteorological Year 3
http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html. Heating Season defined as September 17th through April 13th, cooling season defined as May 20 through August 15th. For cooling season, temperatures from 8AM to 8PM were used to establish average temperatures as this is when cooling systems are expected to be loaded.

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 $Infiltration_{gasheat} = \left(CFM_{PRE} - CFM_{POST}\right) * 60 * EFLH_{heating} * \Delta T_{AVG,heating} * 0.018 / (100,000 * \eta_{heat})$

 $Conduction gasheat = \left(U_{BASE} - U_{EFF}\right) * A_{window} * EFLH_{heating} * \Delta T_{AVG,heating} \ / \ (100,000 * \eta_{heat})$

 $Solar_{gasheat} = \left(SHGC_{BASE} - SHGC_{EFF}\right) * A_{window} * \Psi_{Heating} \, / \, \left(100,\!000 * \eta_{heat}\right)$

Where:

 $\begin{array}{ll} 100,\!000 & = Conversion \ from \ BTUs \ to \ Therms \\ \eta_{heat} & = Efficiency \ of \ heating \ system \\ & = Actual \end{array}$

Other variables as defined above.

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A

2.10.2 Ceiling and Wall Insulation

DESCRIPTION

Energy and demand saving are realized through reductions in the building cooling and heating loads.

This measure was developed to be applicable to the following program types: RF and NC.

If applied to other program types, the measure savings should be verified.

DEFINITION OF EFFICIENT EQUIPMENT

In order for this characterization to apply, the efficient equipment is assumed to exceed the efficiency requirements defined by the program.

DEFINITION OF BASELINE EQUIPMENT

In order for this characterization to apply, the baseline is assumed to meet the efficiency requirements set forth by local jurisdictions. In most cases, this will be some version of IECC. For retrofit applications, the baseline condition is the existing condition and requires assessment of the existing insulation. It should be based on the entire wall assembly.

Local code shall be referenced to define baseline where applicable. As an example, the following is set forth by IECC 2012:

	ASHRAE/IECC Climate Zone 5 (A, B, C) Nonresidential		
	Assembly Maximum Insulation Min. R-Value		
Mass	U-0.078	R-11.4 ci	
Metal Building	U-0.052	R-13 + R-13 ci	
Metal Framed	U-0.064	R-13 + R-7.5 ci	
Wood Framed and Other	U-0.064	R-13 + R-3.8 ci or R-20	

	ASHRAE/IECC Climate Zone 6 (A, B, C) Nonresidential		
	Assembly Maximum	Insulation Min. R-Value	
Mass	U-0.078	R-13.1 ci	
Metal Building	U-0.052	R-13 + R-13 ci	
Metal Framed	U-0.064	R-13 + R-7.5 ci	
Wood Framed and Other	U-0.051	R-13 + R-7.5 ci or R-20 + R-3.8 ci	

Note: ci = continuous insulation

DEEMED LIFETIME OF EFFICIENT EQUIPMENT

The measure expected useful life (EUL) is assumed to be 20 years per DEER 2008. This is consistent with SDG&E's 9th Year Measure Retrofit Study (1996 & 1997 Residential Weatherization Programs), CPUC's Energy Efficiency Policy Manual v.2, and GDS's Measure Life Report Residential and Commercial/Industrial Lighting and HVAC Measures (June 2007).

DEEMED MEASURE COST

For retrofit projects, full installation costs should be used.

For new construction projects, costs should be limited to incremental material and labor costs associated with the portion of insulation that exceeds code requirements.

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LOADSHAPE

HVAC BUS

Algorithm

CALCULATION OF ENERGY SAVINGS

ELECTRIC ENERGY SAVINGS

Electric energy savings is calculated as the sum of energy saved when cooling the building and energy saved when heating the building:

$$\Delta kWh = \Delta kWh_{cooling} + \Delta kWh_{heating}$$

If central cooling, the electric energy saved in annual cooling due to the added insulation is

$$\Delta \text{kWh}_{\text{cooling}} = \frac{\left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) * Area * CRF * EFLH_{cooling} * \Delta T_{AVG,cooling}}{(1,000*\eta_{cooling})}$$

If the building is heated with electric heat (resistance or heat pump), the electric energy saved in annual heating due to the added insulation is:

$$\Delta kWh_{heating} = \frac{\left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) * Area * CRF * EFLH_{heating} * \Delta T_{AVG,heating}}{(3.412*\eta_{heating})}$$

Where:

 $R_{\text{existing}} = Assembly \text{ heat loss coefficient with existing insulation } [(hr-^0F-ft^2)/Btu]$ $R_{\text{new}} = Assembly \text{ heat loss coefficient with new insulation } [(hr-^0F-ft^2)/Btu]$

Area = Area of the surface in square feet.

CRF = Correction Factor. Adjustment to account for the effects the framing has

on the overall assembly R-value, when cavity insulation is used.

= 100% if Spray Foam or External Rigid Foam

= 50% if studs and cavity insulation³⁵⁷

EFLH_{cooling} = Equivalent Full Load Hours for Cooling [hr] are provided in Section 2.7,

HVAC End Use

 $\Delta T_{AVG,cooling} = Average temperature difference [^0F] during cooling season between$

outdoor air temperature and assumed 75°F indoor air temperature

1,000 = Conversion from Btu to kBtu

 $\eta_{cooling} \hspace{1.5cm} = Seasonal \hspace{0.1cm} energy \hspace{0.1cm} efficiency \hspace{0.1cm} ratio \hspace{0.1cm} (SEER) \hspace{0.1cm} of \hspace{0.1cm} cooling \hspace{0.1cm} system \hspace{0.1cm} (kBtu/kWh)$

= Actual

³⁵⁷ Consistent with the information listed in ASHRAE, 2001, Table 5-1 Wall Sections with Steel Studs Parallel Path Correction Factors and experimental findings by the Oak Ridge National Laboratory, "Couple Secrets about How Framing is Effecting the Thermal Performance of Wood and Steel-Framed Walls."

EFLH_{heating} = Equivalent Full Load Hours for Heating [hr] are provided in Section 2.7,

HVAC end use

 $\Delta T_{AVG,heating} = Average temperature difference [^0F] during heating season between$

outdoor air temperature and assumed 55°F heating base temperature

3,412 = Conversion from Btu to kWh. = Efficiency of heating system η heating

= Actual. Note: electric resistance heating and heat pumps will have an

efficiency greater than or equal to 100%

Weather Basis	OAAVG,cooling	ΔTAVG,cooling	OAAVG,heating	ΔTAVG,heating
(City based upon)	[°F] ³⁵⁸	[°F]	[°F] ³⁵⁹	[°F]
St Louis, MO	80.8	5.8	43.2	11.8

If the building is heated with a gas furnace, there will be some electric savings in heating the building attributed to extra insulation since the furnace fans will run less.

 $\Delta kWh_{heating} = \Delta Therms * Fe * 29.3$

Where:

ΔTherms = Gas savings calculated with equation below.

= Percentage of heating energy consumed by fans, assume 3.14%³⁶⁰ Fe

29.3 = Conversion from therms to kWh

SUMMER COINCIDENT PEAK DEMAND SAVINGS

 $\Delta kW = \Delta kWH_{cooling} * CF$

Where:

ΔkWH_{cooling} = Annual electricity savings for cooling, as calculated above.

= Summer peak coincidence demand (kW) to annual energy (kWh) factor

for Cooling = 0.0004439830

NATURAL GAS SAVINGS

³⁵⁸ National Solar Radiation Data Base -- 1991- 2005 Update: Typical Meteorological Year 3

http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html. Heating Season defined as September 17th through April 13th, cooling season defined as May 20 through August 15th. For cooling season, temperatures from 8AM to 8PM were used to establish average temperatures as this is when cooling systems are expected to be loaded. 359 National Solar Radiation Data Base -- 1991- 2005 Update: Typical Meteorological Year 3

http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html. Heating Season defined as September 17th through April 13th, cooling season defined as May 20 through August 15th. For cooling season, temperatures from 8AM to 8PM were used to establish average temperatures as this is when cooling systems are expected to be loaded.

³⁶⁰ Fe is not one of the AHRI certified ratings provided for furnaces, but can be reasonably estimated from a calculation based on the certified values for fuel energy (Ef in MMBtu/yr) and Eae (kWh/yr). An average of a 300 record sample (non-random) out of 1495 was 3.14% for residential units. This is, appropriately, ~50% greater than the Energy Star® version 3 criteria for 2% Fe. See "Programmable Thermostats Furnace Fan Analysis.xlsx" for reference. Assumed to be consistent with C&I applications.

If building uses a gas heating system, the savings resulting from the insulation is calculated with the following formula.

$$\Delta \text{Therms} \qquad \frac{=\left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) * Area * CRF * EFLH_{heating} * \Delta T_{AVG,heating}}{(100,000*\eta_{heat})}$$

Where:

 $\begin{array}{ll} R_{existing} & = Assembly \ heat \ loss \ coefficient \ with \ existing \ insulation \ [(hr^0F-ft^2)/Btu] \\ R_{new} & = Assembly \ heat \ loss \ coefficient \ with \ new \ insulation \ [(hr^0F-ft^2)/Btu] \\ Area & = Area \ of \ the \ surface \ in \ square \ feet. \ Assume \ 1000 \ sq \ ft \ for \ planning. \\ EFLH_{heating} & = Equivalent \ Full \ Load \ Hours \ for \ Heating \ are \ provided \ in \ Section \ 2.7, \end{array}$

HVAC end use

 $\Delta T_{AVG,heating}$ = Average difference [${}^{0}F$] during heating season (see above)

 $\begin{array}{ll} 100,\!000 & = Conversion \ from \ BTUs \ to \ Therms \\ \eta_{heat} & = Efficiency \ of \ heating \ system \end{array}$

= Actual

WATER IMPACT DESCRIPTIONS AND CALCULATION

N/A

DEEMED O&M COST ADJUSTMENT CALCULATION

N/A