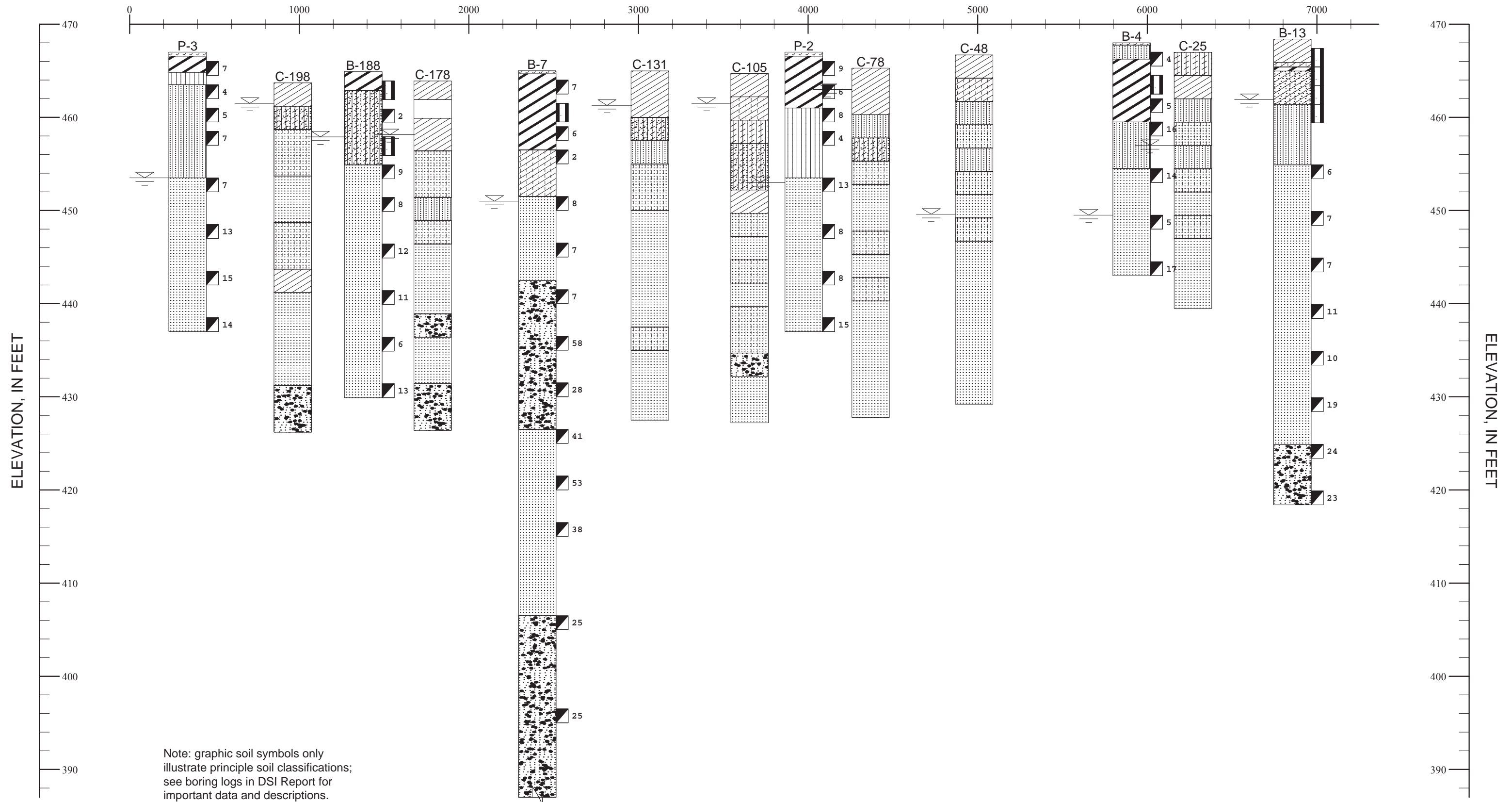


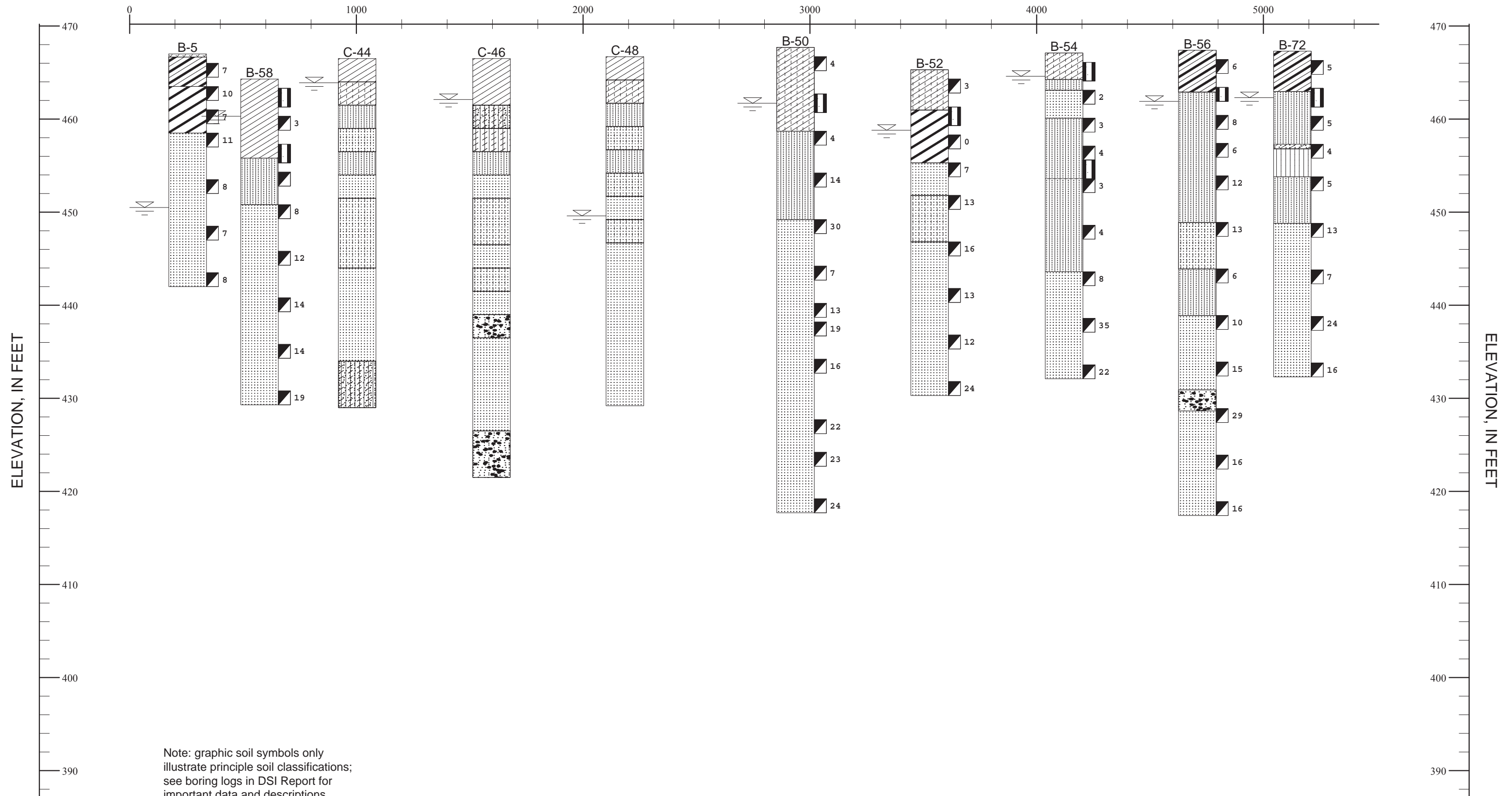
Figure 1



Note: graphic soil symbols only illustrate principle soil classifications; see boring logs in DSI Report for important data and descriptions.

- | | | | |
|----------------------------------|---|----------------------------------|--|
| Topsoil | Poorly-graded SAND (SP) | Poorly-graded SAND & GRAVEL (GP) | Clayey SAND or Sandy CLAY (SC) |
| High plastic CLAY (CH) | Low plastic CLAY (CL) | Interval not sampled | Depth of ground water observed during drilling |
| Inorganic, non-plastic SILT (ML) | Clayey Sandy SILT (ML) | Low plastic Silty CLAY (CL) | |
| Silty SAND or Sandy SILT (SM) | Poorly-graded SAND with traces of fines | Low plastic Clayey SILT (ML) | |

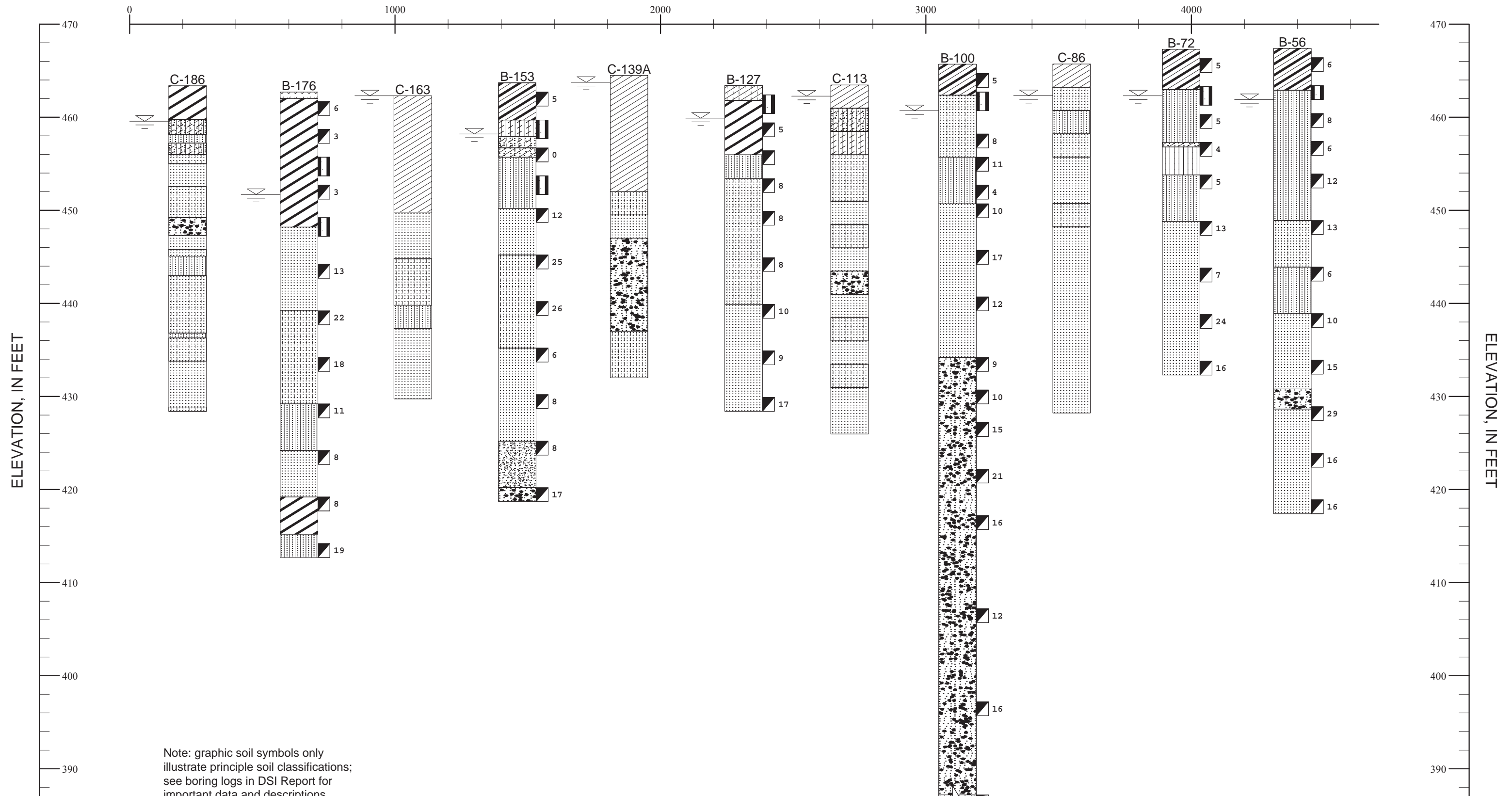
Ameren Missouri Labadie UWL
GENERAL SOIL PROFILE
A-A'



Note: graphic soil symbols only illustrate principle soil classifications; see boring logs in DSI Report for important data and descriptions.

- | | | | |
|-----------------------------|---|----------------------------------|--|
| Topsoil | Low plastic CLAY (CL) | Clayey Sandy SILT (ML) | Inorganic, non-plastic SILT (ML) |
| Medium to high plastic CLAY | Silty SAND or Sandy SILT (SM) | Low plastic Clayey SILT (ML) | Depth of ground water observed during drilling |
| High plastic CLAY (CH) | Low plastic Silty CLAY (CL) | Poorly-graded SAND & GRAVEL (GP) | |
| Poorly-graded SAND (SP) | Poorly-graded SAND with traces of fines | Clayey SAND or Sandy CLAY (SC) | |

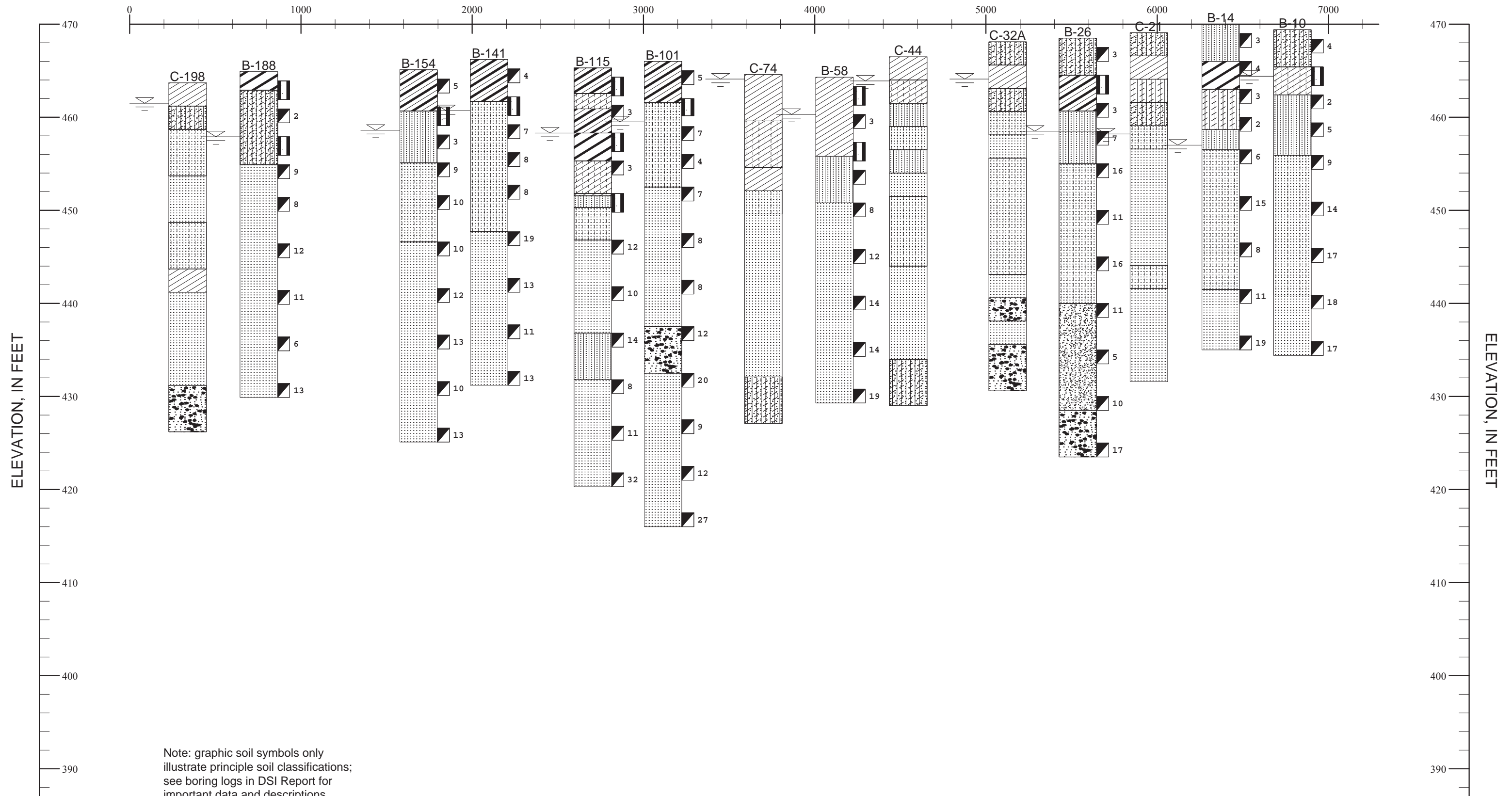
Ameren Missouri Labadie UWL
GENERAL SOIL PROFILE
B-B'



Note: graphic soil symbols only illustrate principle soil classifications; see boring logs in DSI Report for important data and descriptions.

- | | | | |
|---|----------------------------------|--------------------------------|--|
| High plastic CLAY (CH) | Poorly-graded SAND (SP) | Medium to high plastic CLAY | Well-graded SAND with no fines (SW) |
| Clayey Sandy SILT (ML) | Poorly-graded SAND & GRAVEL (GP) | Low plastic Clayey SILT (ML) | Low plastic Silty CLAY (CL) |
| Silty SAND or Sandy SILT (SM) | Topsoil | Clayey Silty SAND (SC-SM) | Inorganic, non-plastic SILT (ML) |
| Poorly-graded SAND with traces of fines | Low plastic CLAY (CL) | Clayey SAND or Sandy CLAY (SC) | Depth of ground water observed during drilling |

Ameren Missouri Labadie UWL
GENERAL SOIL PROFILE
C-C'

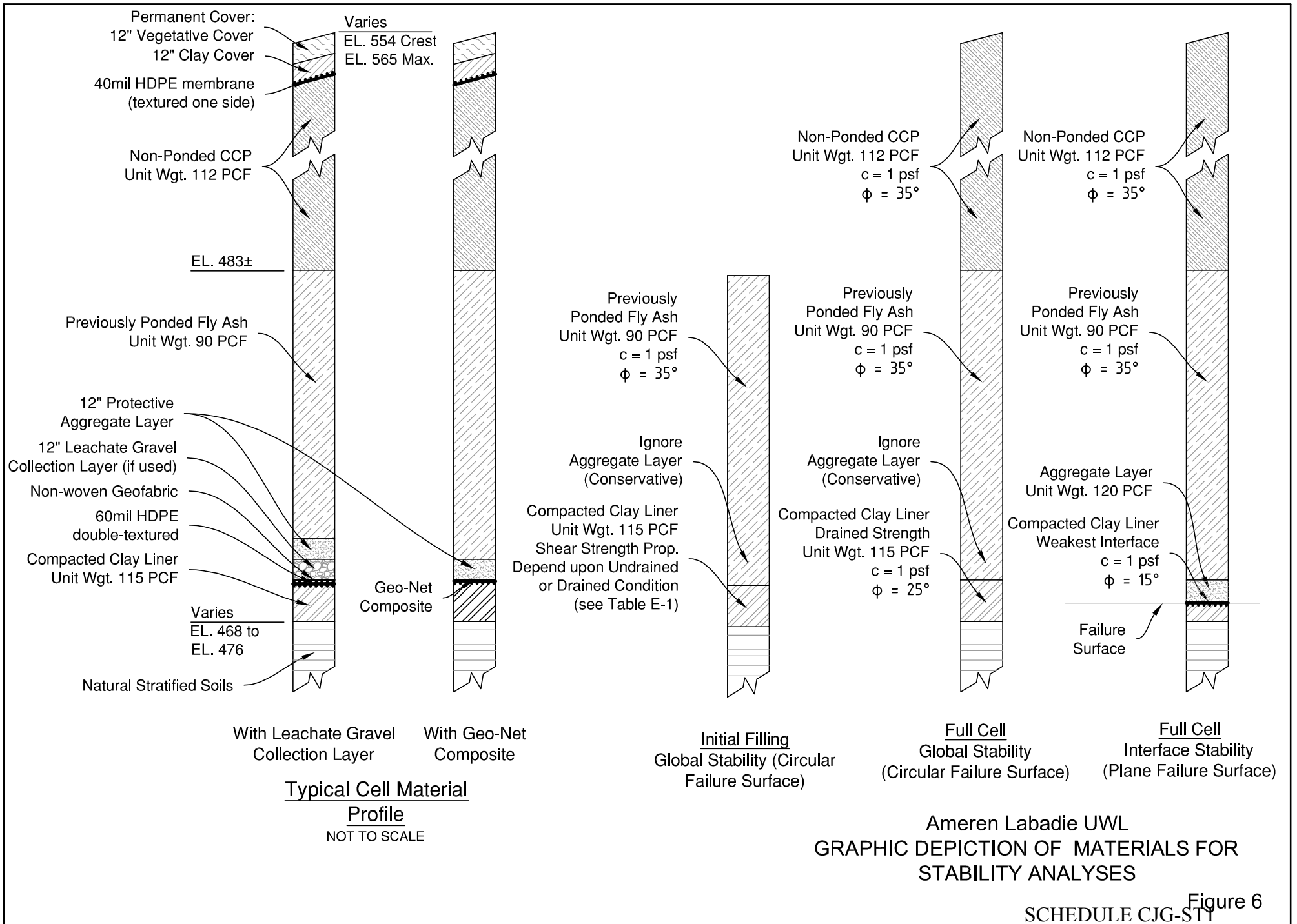


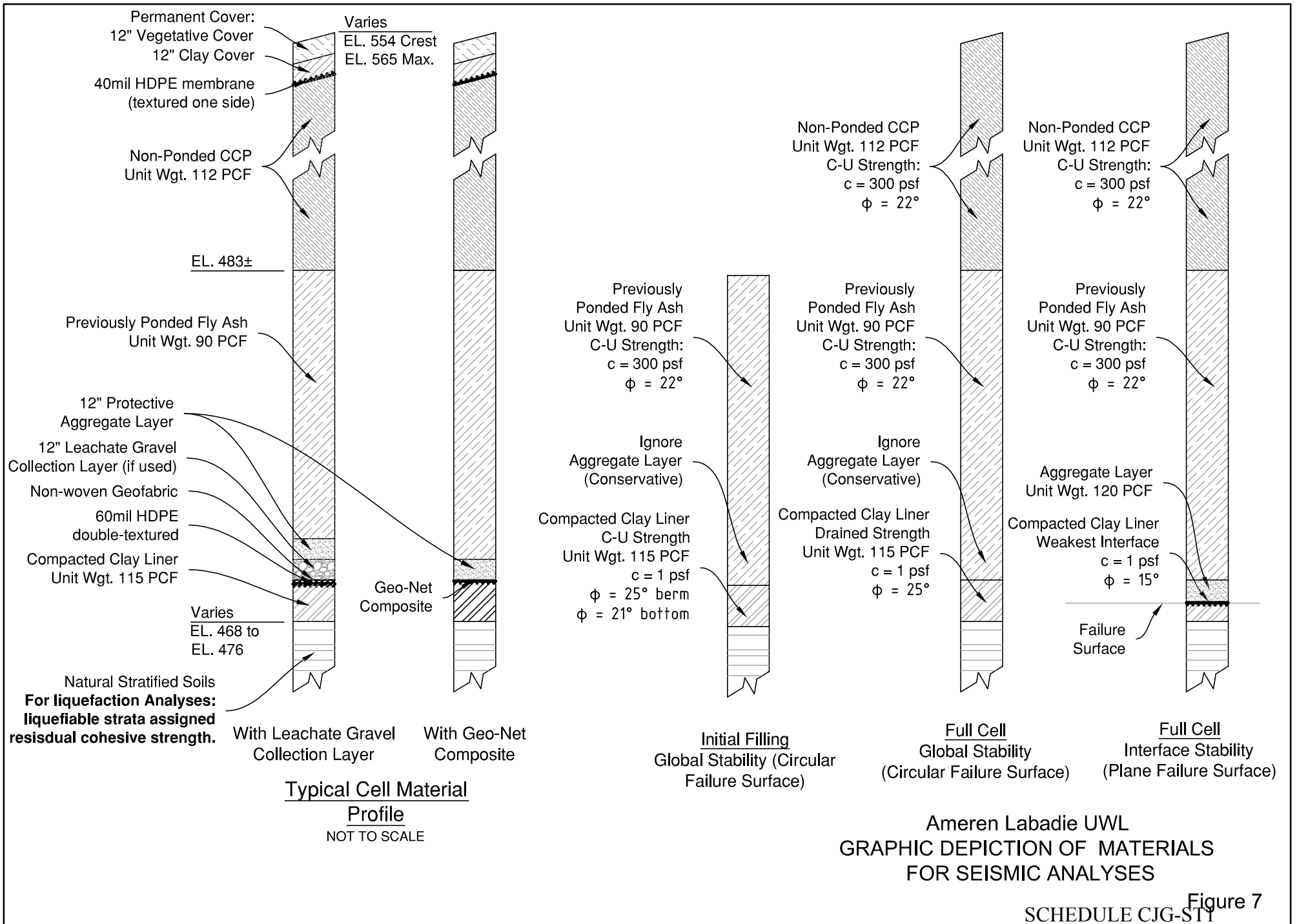
Note: graphic soil symbols only illustrate principle soil classifications; see boring logs in DSI Report for important data and descriptions.

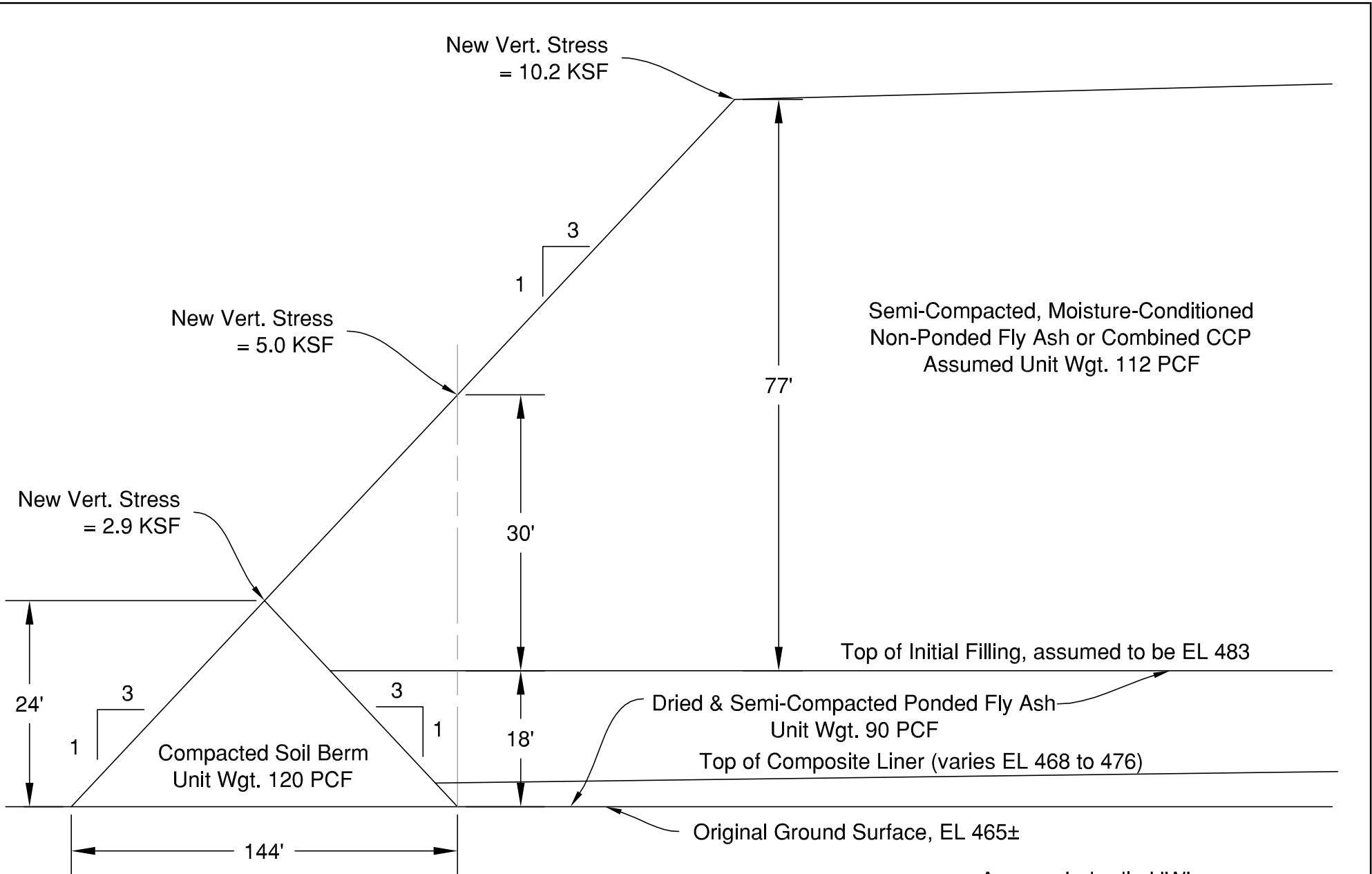
- | | | |
|---|----------------------------------|-------------------------------------|
| Low plastic CLAY (CL) | Poorly-graded SAND & GRAVEL (GP) | Low plastic Silty CLAY (CL) |
| Clayey Sandy SILT (ML) | High plastic CLAY (CH) | Clayey SAND or Sandy CLAY (SC) |
| Poorly-graded SAND with traces of fines | Medium to high plastic CLAY | Well-graded SAND with no fines (SW) |
| Poorly-graded SAND (SP) | Silty SAND or Sandy SILT (SM) | Low plastic Clayey SILT (ML) |

Depth of ground water observed during drilling

Ameren Missouri Labadie UWL
GENERAL SOIL PROFILE
D-D'

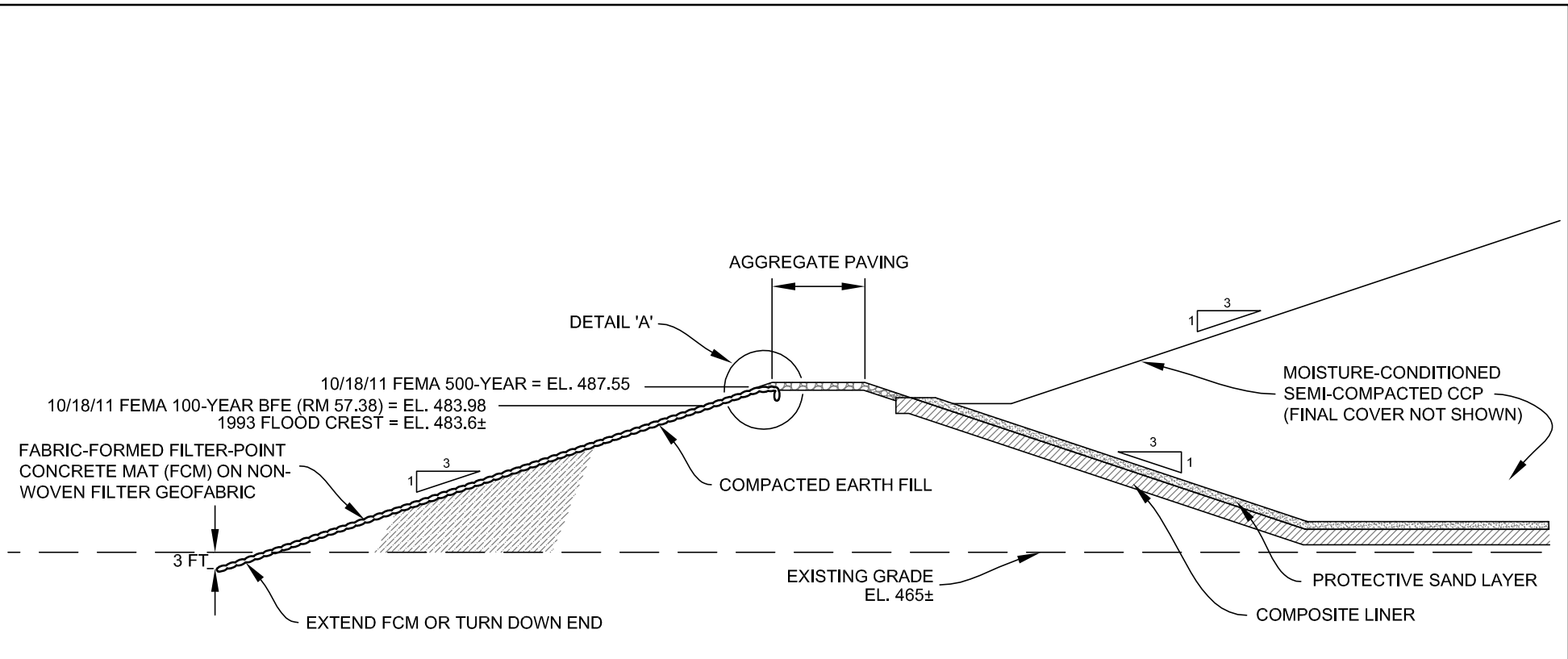




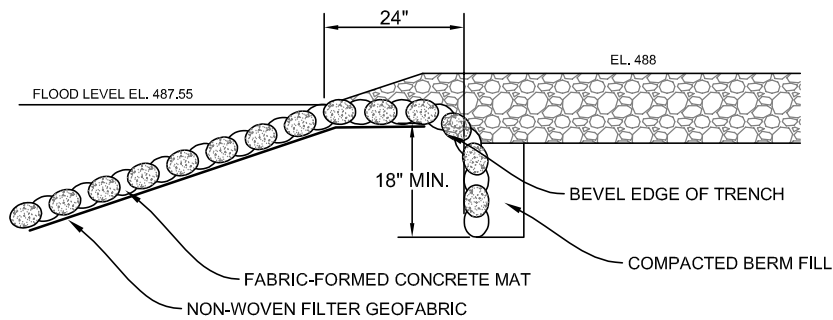


Ameren Labadie UWL
 MODEL FOR CALCULATION OF VERT. STRESSES
 FOR SETTLEMENT ANALYSES

Figure 8
 SCHEDULE C/JG-ST1

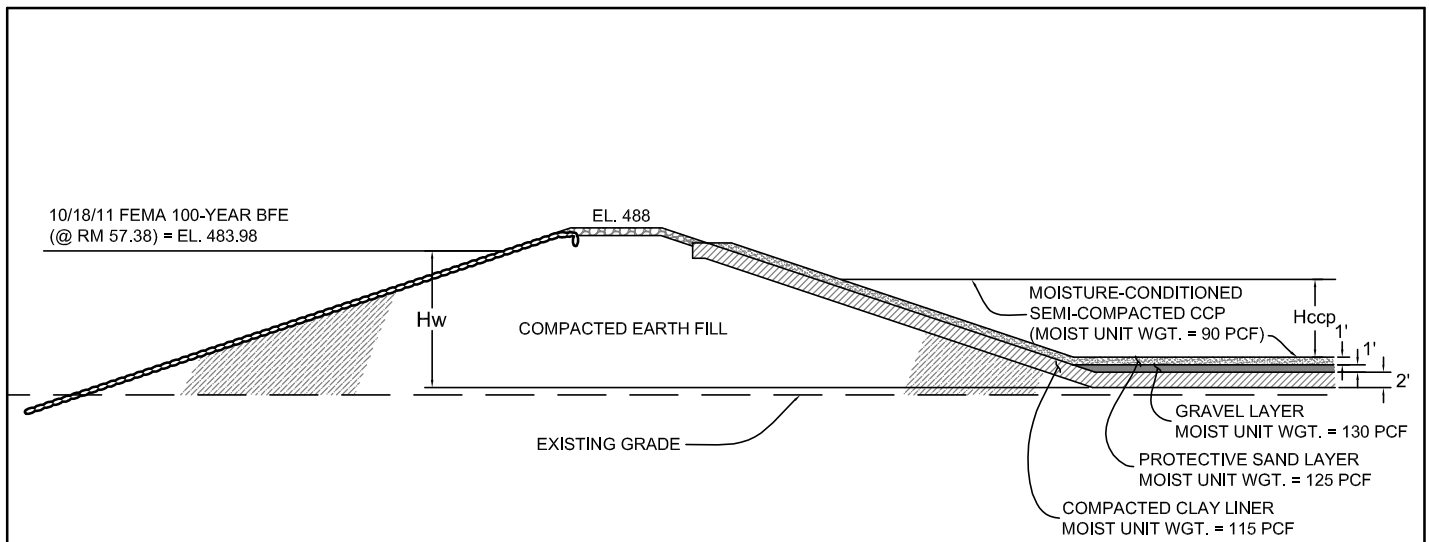


GENERAL CROSS-SECTION OF PERMANENT EXTERIOR BERM



DETAIL 'A' - FCM ANCHOR TRENCH

Ameren Missouri Labadie UWL
 PROPOSED CONCRETE EROSION
 PROTECTION FOR EXTERIOR BERMS



Factor of Safety Against Hydrostatic Uplift of Bottom Clay Liner (FS_{uplift}):

$$FS_{uplift} = (H_{ccp} \times 90 \text{ PCF} + 1' \times 125 \text{ PCF} + 1' \times 130 \text{ PCF} + 2' \times 115 \text{ PCF}) / (H_w \times 62.4 \text{ PCF})$$

with a 12" thick protective sand layer, 12" thick gravel leachate collection layer, and a 24" thick compacted clay liner, where:

H_w = difference in height from flood level to bottom of clay liner (based upon the assumption that the subgrade of the clay liner is permeable)

H_{ccp} = height of CCP above sand layer (with CCP moist unit weight = 93 PCF)

The required height of the CCP for a FS_{uplift} of 1.1 and with a gravel collection layer:

$$\text{Required } H_{ccp} = [(H_w \times 62.4 \text{ PCF} \times 1.1) - 485 \text{ PSF}] / 90 \text{ PCF}$$

Example: for 100-year flood at el. 484 and bottom of clay liner at el. 466,

$H_w = 484 - 466 = 18$ feet, and required $H_{ccp} = 8.3$ feet for $FS_{uplift} = 1.1$, or a vertical difference of 5.7 feet between the 100-year flood level and the top of the CCP fill.

If a geonet is substituted for the 12" thick gravel collection layer, and the geonet is considered to be weightless, then:

$$FS_{uplift} = (H_{ccp} \times 93 \text{ PCF} + 1' \times 125 \text{ PCF} + 2' \times 115 \text{ PCF}) / (H_w \times 62.4 \text{ PCF})$$

and the required height of the CCP is:

$$\text{Required } H_{ccp} = [(H_w \times 62.4 \text{ PCF} \times 1.1) - 355 \text{ PSF}] / 90 \text{ PCF}$$

where H_{ccp} is the height of CCP above the protective sand layer. This equation applies to any point on the side slope of the berm where the geonet will be used, but only if the berm is constructed with permeable fill (sands and silts).

Ameren Missouri Labadie UWL
CALCULATION OF RESISTANCE
TO HYDROSTATIC UPLIFT ON CLAY LINER